Appendix F-1

Geotechnical Desk Study - Part 1

States of Jersey Jersey Future Hospital: Geotechnical Desk Study

JFH-ARP-ZZ-XX-RP-G-0001

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This report takes into account the particular instructions and requirements of our client.

It is not intended for and should not be relied upon by any third party and no responsibility is undertaken to any third party.

Job number 237035

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1 Introduction

Ove Arup and Partners Ltd (Arup) have been appointed by the States of Jersey to undertake a detailed geotechnical desk study and present recommendations for ground investigation. The purpose of the geotechnical desk study is to support a planning application for the redevelopment and construction of new hospital buildings on part of the existing site and some adjacent buildings including provision of new/modified basement at Jersey General Hospital. The redevelopment at Westaway Court is also looked at during this report.

The proposals are to comprehensively redevelop both the Jersey General Hospital and Westaway Court sites to provide modernised health facilities.

The locations of the existing and proposed footprints of Jersey General Hospital and Westaway Court are shown on **Figure 1**.

Since the last issue of the Jersey Future Hospitals Geotechnical Desk Study the ground and groundwater conditions section has been updated to include additional information from a ground investigation undertaken for the adjacent Patriotic Street MSCP (undertaken in 1983). Ground investigation data from three other sites within 60m to the southwest of the Jersey Future Hospitals site (undertaken between 2007 and 2014) have also been considered. These additional records provide further information relating to the site stratigraphy and useful additional detail concerning groundwater strikes and groundwater monitoring which is of particular importance for assessment of basement design options and optimum construction sequencing.

2 Report Objective

The purpose of this detailed geotechnical desk study report is to gather and present all available relevant geotechnical information to inform the proposed redevelopment of the Jersey General Hospital and Westaway Court sites. A detailed review of all available information has been undertaken, including:-

- The latest development proposals
- Engineering records and drawings; including existing buildings, foundations and basement layouts
- Geology and hydrogeology
- Encountered ground conditions and existing ground investigation
- Hydrology
- Historical maps and aerial photographs
- Referenced historical documents
- Environmental issues, features and constraints

Identified features and constraints are highlighted on **Figure 11**, and identified ground risks are summarised in the Ground Risk Register in **Appendix F**. A preliminary assessment of the main geotechnical considerations for the sites is presented to help inform design development decisions. Recommendations are presented for additional ground investigations to better understand the ground risks, stratigraphy and groundwater conditions and to allow characteristic parameters for geotechnical designs to be derived.

3 Proposed Development

The hospital development proposals are currently being developed by Hassells. Available artistic illustration of demolition / construction schematic extracts from Hassell's report [28] for the General Hospital site and indicative drawing of currently considered options of redevelopment [29] for Westaway Court are provided in **Appendix J.** Indicative proposed footprints are provided on **Figure 2** and **Figure 3**.

A list of all relevant records and engineering drawings reviewed as part of the preparation of this report is presented in **Appendix A**, and available construction drawings provided in **Appendix E**.

3.1 Jersey General Hospital

The existing building layouts based upon the Ordnance Survey mapping and the proposed redevelopment footprints are indicated on **Figure 2.** Key proposed redevelopments of the existing General Hospital site and adjacent land is understood to currently comprise the following:

- Granite Block C and the Granite Gatehouse Grade I listed buildings are the only buildings to remain.
- Existing hospital buildings D, E and H and existing Stafford Hotel, Sutherland Court and Revere Hotel are to be demolished to allow for construction of the basement and new building. It is understood that demolition is proposed will be sequenced across the site.
- Existing hospital buildings A, B, F and G are outside of the development footprint and currently are not proposed for demolition works. Careful consideration will be required for removal and reinstatement of connections and building links between the existing hospital buildings to be demolished (between block E and Block F), those outside of the proposed hospital footprint that are to be retained and between block E and H to be demolished and block C to be retained

At the time of writing, the proposed New Build Hospital development layout (presented on **Figure 3**) can be summarised as follows:

- The New Build Hospital will comprise a large rectangular building spanning between Kensington Place in the north and Gloucester Street in the south. A smaller building is proposed in the west. The New Build Hospital is proposed to be some 8 storeys high. Two new access roads are proposed either side parallel with the lengths of the new rectangular building and parallel with existing Newgate Street.
- The construction of a large 'L'shaped basement is proposed to extend from Gloucester Street in the south to Kensington Place in the north, beneath the footprint of the new building. The western end of the basement north of Patriotic Street Multi Story Car Park is proposed to house one of the lift cores and service yard access. The basement is

anticipated to be constructed within at least a 10m perimeter of the proposed new building footprint boundary, see **Figure 3**.

- A new access link between Patriotic Street Multi Storey Car Park and the north-western part of the new hospital building is proposed at the western end of the scheme area.
- During the demolition and construction phase of the development a three storey temporary clinic block is to be constructed.

Further to the proposed development at the Jersey General Hospital there's a potential for an additional storey to be added to the existing Patriotic Street Multi-Storey Car Park situated south-west of the existing hospital buildings.

The Patriotic Street MSCP has had two preliminary feasibility reports prepared which consider the possibility of construction of an extra storey [26], [27]. Photographs and relevant images of the MSCP and the existing hospital buildings are presented in **Appendix B-1**.

The proposals at the Jersey General Hospital are currently being developed.

3.2 Westaway Court

The existing building layouts based upon the Ordnance Survey mapping and indicative development proposal footprints are provided on **Figure 3** and the latest hospital proposals provided in **Appendix J.**

At the time of writing proposals for Westaway Court comprised the following:

- Demolition of Blocks A, B, C and D and replacement with new building. Buildings to be primarily accommodation blocks for medical professionals who work in the Hospital. The tallest building is a 9 storey tower block (with a square footprint) and a 4 storey 'L-shaped' building around the southern and eastern sides of the tower block. Currently the two buildings aren't proposed to be linked and a small car park/courtyard space is proposed between the two buildings.
- Building to consist of up to four storeys above ground.
- Typical clinical zones have been identified by level on 1:500 scale drawings.
- Plant areas/plant rooms and locations are still under review
- The proposed building will require an interim state to accommodate an alternative internal layout

4 The Site

4.1 Site Location and Description

4.1.1 Jersey General Hospital

The Jersey General Hospital site is situated off Gloucester Street, to the northwest of the town centre of St Helier, and approximately 250m from the seashore of St Aubin's Bay. The site location for Jersey General Hospital is shown on **Figure 1**.

The existing Jersey General Hospital building layout is shown on **Figure 2**. Photographs taken during a recent site walkover undertaken by an Arup Structural Engineer on Thursday 18th August 2016 are included in **Appendix B-1**. The locations these photographs were taken are indicated on **Figure 4**.

The site is approximately 'z-shaped' measuring approximately 200m by 150m. The surface of the site appears relatively flat however it generally slopes from north to south. Based on Ordnance Survey levels (as indicated on **Figure 11**) the elevation at the northern corner of the site is 12.8mOD whereas the southern corner is at 7.6mOD. An approximate difference in ground elevation across the site of 5.2m. There is also a change in elevation over the length of the proposed new development (refer to **Figure 2**). From Gloucester Street to Kensington Place the site rises up by 3.3m. Careful consideration of this elevation change should be taken into account as part of the design.

The site is bounded to the northeast by 'The Parade', to the southeast by 'Gloucester Street', to the southwest by 'Newgate Street' and to the northwest by 'Kensington Place'.

The site is an active hospital with a congested building layout, with buildings constructed during the 1800's, 1960's and 1980's, see **Figure 2**. Some of the junctions between buildings are stepped, one example of this is a step down from the court yard in the south-western part of the site adjacent to Block E and adjacent to Block H.

Site walkover Photographs 15 to 18 show parking is mainly confined to the basements in the western and southern parts of the site. The known extent of the basements are indicated on **Figure 6**. There is peripheral parking in the southern part of the site in front of Granite Block C, see Photo 22.

The Jersey Planning Department report the 1860 Granite General Hospital building and Granite Gatehouse within the southern part of the site to be Grade I listed buildings [3], the 'Statement of Significance' is as follows:

"An important example of a substantial mid-19th century hospital typical of the period retaining most historic features, with outstanding masonry work. The entrance lodge is an unusual building of high quality, retaining fine feature in a muscular hybrid classical/neo-Norman style. Together a fine ensemble."

The history of the site is discussed further in the Site History section below.

4.1.2 Westaway Court

Westaway Court site is situated approximately 100m north of the Jersey General Hospital site on the north side of Parade Gardens and west of St Helier town centre. The site is bounded by Savile Street along the north-eastern boundary, Elizabeth Place along the north-western boundary and Parade Gardens to the south. The site location for Westaway Court is also shown on **Figure 1**.

There are two existing buildings on the Westaway Court site. The first is a square 9 storey tower block at the north of the site and the second is an 'L-shaped' 4 storey building to the south of the tower block, see photo 4 in **Appendix B-2**. There is a large car park adjacent to Savile Street which has an access road along the north-western edge of the site to an internal car park/courtyard area in the space between the two buildings. Site walkover photographs taken on Thursday 18th August 2016 by an Arup Structural Engineer are indicated in **Appendix B-2** and locations are indicated on **Figure 5**.

The buildings on the site are currently used as accommodation for medical professionals who work in the Jersey General Hospital.

4.2 Site History

The history of the Jersey General Hospital and the Westaway Court sites have been reviewed using historical plans, aerial photos obtained from Jersey Archives and supplemented with published information and historical documents on the hospital site [3] [7] [8] [13] [14] dating between 1741 and 2016.

The approximate proposed hospital building footprints are annotated on historical plan extracts and aerial photographs provided in **Appendix C**.

4.2.1 Jersey General Hospital

A report on the history of the Jersey General Hospital, after its centenary year in 1963 [13], details how the hospital first came to fruition in the 18th century. A summary of the key findings of this report is provided below as follows.

In 1741 a Mrs Bartlett "bequeathed to the public 50,000 francs of which 10,000 was to erect a poor house and 40,000 for its upkeep'[13]. The poor house was initially planned to be built in St. Aubin which, at that time, was the commercial capital of the Island. Eventually the States of Jersey decided on a site in St. Helier and in 1765 the foundation of the poor house was laid. A chronological history of Jersey General & Acute Hospital document shows that a building 'for the destitute, aged and orphans".

The Jersey Planning portal [3] indicates the first foundation stone laid for the first 'poor house' building in 1765 and the building (referred to as C18) was completed in 1768.

By 1772 the poor house is reported to have opened [14] for the destitute, aged and orphans. Designed to house 250 there were usually 350 accommodated.

Earliest historical plan dated 1781, shows the rectangular 'poor house' building (Block C) in place within the site.

The Centenary document and chronological history document both indicate the original building was burnt down in 1783.

In 1793 the hospital is reported to have reopened [14].

Richmond Map dated 1795 shows the Granite Block building footprint and an entrance track to the south-eastern side of the building. Beyond the south-eastern boundary buildings are shown to be present off the present day Parade Road, with open undeveloped areas to the north-east, north and south-west. A surface water feature flows in a westerly direction towards the southern corner of the site at which point it changes direction to flow in a south-westerly direction where it discharges at St Aubin's Bay.

Map dated 1800 shows the same hospital building footprint, within a more defined rectangular site boundary. Garden areas are shown to the east and west of the building. The surface water feature is no longer shown. No mapping features are shown within the far south-western part of the proposed new hospital footprint.

The 1834 map shows that the infrastructure surrounding the site was established, comprising Gloucester Street, Parade Place, and George Street (the present day Kensington Place). The Granite Block hospital building footprint remains unchanged. Some 'step-like' features are annotated at the southern side of the building, possibly access to the basement (refer to basement layout provided on **Figure 6**). Gardens are marked out to the rear of the Granite Block within the central western part of the proposed development footprint. No buildings are annotated within the western part of the proposed footprint off George Street. A rectangular building marked 'Prison' is annotated within the south-western part of the site.

The Godfray Map of 1849 shows the Granite Block within the same footprint. The prison building remains present to the south-west of the site. A building is present within the location of the present day location of Patriotic Street MSCP. A row of development has been constructed within the south-western part of the site off George Street (present day Kensington Place).

The hospital is reported on the planning portal [3] to have been destroyed by fire in July 1859. The new hospital building is reported to have begun construction on the same foundation stone in 1860. The official opening ceremony of the hospital building took place on 10th March 1863. It is also reported that the hospital was designed by architect Thomas Gallichan and built by Messer Le Gros & Le Cras. The entrance lodge was added in 1877 [3].

A photograph taken around 1879 [7] from the high ground near Westmount Road, near Overdale Hospital, west of the site, shows the western side of the hospital building and the chimney in place. The prison building is shown to the right-hand side of the chimney (in the locale of the present day Patriotic Street MSCP.

Plans dated 1900 and 1907 show the infrastructure of St Helier is further established. George Street is renamed Kensington Place. Newgate Street is

annotated along the western boundary of the site. The prison buildings remain present within the south-western part of the site. No significant changes to the site and the surrounding area.

The Centenary document [13] also details several changes to the hospital in the early 20th century. In 1908 the Hospital Committee were involved in a legal case between themselves and a Mr Mirehouse who had complained about the conditions and the way the Hospital was run concerning the spread of certain diseases. After this case considerable improvements were made to the internal conditions of the hospital.

Following on from this the Centenary document [13] explains how the Hospital had electricity installed for the first time in 1923. In 1924 the General Hospital was recognised as a training hospital for nurses.

It also details how in 1930 a separate building was to be constructed to house the poor, aged and infirm meaning that the original building now purely dealt with medical cases.

In 1940 the Hospital was occupied by German Armed Forces.

Aerial photos taken in 1943 and 1944 show no significant changes. Historical documents indicated that the Hospital was occupied by German forces between the years of 1940-1945 [13] [14]. Jersey was liberated in 1945.

Peter Crill House was constructed in 1949 and opened in 1950 (initial nurses home at the time). Subsequently overclad / refurbished.

In 1962 the 1960's Wing opened housing Accident & Emergency, 2 theatres and private wing.

Ordnance survey plan dated 1968 shows the prison buildings in the western part of the site are shown as one building, annotated 'H M Prison'.

Aerial photo dated 1974 shows Block B had been constructed by this time. The prison buildings had been demolished and hospital buildings extended within the western part of the site. With the exception of the Granite Block C, other buildings on the site appear of a different layout compared to the present day.

The Chronological historical document indicates the Gwyneth Huelin Block (out patients) (Block E) was opened in 1979 (Phase 1) and the Engineering block (Block G) housing the boiler and oil tanks was opened in 1980 (Phase 1A) [14].

From review of the chronological history document and a Jersey group of Hospitals document it is clear that Block F, containing a pharmacy, mortuary and kitchens, was opened in 1983 (Phase 1B) [14] [15]. Construction of Blocks E, F and G was part of a multi-phase process that began in 1969 as indicated in the Jersey group of Hospitals document [15].

In 1983 Pathology, Pharmacy, Mortuary and Kitchens opened (Phase 1B).

The Granite bell tower from the original (demolished) hospital chapel was relocated alongside the lodge in 1984 [3].

Between 1984 and the present day modifications have occurred to the hospital building.

In 1987, in-patient seven story block opened (Phase 2).

In 1994 Peter Crill House opened (formerly the Nurses Home).

In 2015, a long-term temporary theatre was constructed within the narrow car park to the front of the Granite Block.

Summary

In summary the Jersey General Hospital site has been continuously developed since 1765 with more large scale construction developments occurring in the late 20th century. The constant development of the Jersey General Hospital site increases the likelihood that made ground will be encountered beneath the site.

4.2.2 Westaway Court

Earliest historical plan dated 1781 shows no mapped features within the site. Meadows' are mapped to the north-east of the site on within the outskirts of St Helier.

Richmond Map dated 1795 shows the Westaway site within the south-western corner of a field parcel to the north of 'rough pasture' land. Elizabeth Place is shown in place as a track / road to the west of the site. A small rectangular building is shown within the far south-western corner of the field parcel. '

Map dated 1800 shows the site within the south-western corner of an area of land annotated 'Prairies' (meadows). No buildings or features are annotated within the site or immediate vicinity of the site. The present day Elizabeth Place is annotated 'Le Rouge Bevillen' to the west of the site. The cemetery is annotated in the present day location within the eastern side of Parade Gardens.

The 1834 map shows that the infrastructure surrounding the site was becoming established. Within the site boundary, a rectangular building is present along much of the western boundary with gardens across the central and southern parts of the site. No mapped features are shown across the northern part of the site, which lies within the southern part of a larger field parcel. Immediately south of the site 'The Parade' (public open space / gardens) perimeter is lined with trees and layout established. The bounding road to the west is annotated 'Elizabeth Place'.

The Godfray Map of 1849 shows no significant change to the site. Further development has occurred to the surround site area.

Plans dated 1900 and 1907 show no significant changes to the site and the surrounding area. The infrastructure of St Helier is further established.

Ordnance survey plan dated 1968 and aerial photos show a north-west to southeast orientated building present within the site. No further significant change.

Construction drawings dated 1993 for Block D (linking Blocks A and C) are provided in **Appendix E**. As built drawings are not currently available.

No further significant changes have occurred up to the present day.

Summary

Historical mapping has shown that the Westaway Court site was green-field (meadows) up until 1843 when the first mapped building was constructed on the Westaway Court site. Construction drawings for Block C (1974) and Block D (1993) give an indication of the construction date for the current existing buildings.

4.3 Geology

The BGS hold no digital mapping for the Channel Islands. The geology of Jersey has been studied from 1:25,000 scale geological map. An extract of the map is provided within **Figure 7**.

Geological information has been reviewed from the following sources:

- Jersey Channel Islands Sheet 2 at 1:25,000 scale Geological map [9]
- Jersey Channel Islands geological memoir [10]

4.3.1 Made Ground

Jersey General Hospital

Made ground is anticipated to be present on the site relating to the construction platform to the historic and existing buildings and activities at the site. The site is surfaced with hard standings or buildings, as shown on the site walkover photos provided in **Appendix B-1**.

Westaway Court

Made ground is anticipated to be present on the Westaway Court site related to the construction and demolition of historic and the existing buildings on site. The site surface is covered with hard standings, masonry and tarmac as shown in the site walkover photos in **Appendix B-2**.

4.3.2 Superficial deposits

Jersey General Hospital

The geological map shows the site to be over Blown Sands superficial deposits typically comprising a structureless quartz-feldspar with low shell content due to aeolian deposition. The underlying Alluvium can comprise organic silts and muds with peat layers up to 2m thick, and often lenses and layers of coarser grained material, especially towards the base.

Westaway Court

The Westaway Court site is underlain by the same Alluvium superficial deposits which lie underneath the Blown Sand deposits found under the Jersey General Hospital site. Comprising of silts, muds and peat layers up to 2m thick. Coarser grained material especially towards the base.

4.3.3 Bedrock

Jersey General Hospital

The solid geology beneath the site comprises the Jersey Shale Formation (JSh) across much of the site, comprising mudstone, sandstone and grit. The St John's Road Andesite (JA) of the St Saviour's Andesitic Formation is shown to outcrop beneath the superficial deposits across the far north-western corner of the site.

The St John's Road Andesite forms the eastern outer limb of the north-east to south-west trending fold called the St Helier syncline, in the volcanic rocks. The dip of the eastern limb is indicated to be approximately 80° to the west [10].

The geological map extract provided in **Figure 7** shows three boreholes within the central and eastern parts of the site, within the Jersey Shale Formation. These could be the locations of the 1973 boreholes discussed in Section 5.1 below; however this is not confirmed.

Westaway Court

The Jersey Shale Formation (JSh) lies beneath the Westaway Court site.

4.3.4 Geological Paper dated 1989 on construction of basements in St Helier

There is a geological paper written by Littlejohn G.S et al. that details the difficulties of constructing basements within the St Helier blown sand deposits from a development at the TSB building in 1989 [30].

The TSB building lies approximately 500m east of the Jersey General Hospital Site but is also underlain by the same blown sand deposits with a high phreatic surface. This provides difficulty for constructing underground structures as the ground conditions are very unstable and prone to running sand conditions, as mentioned from the anecdotal evidence at the Jersey General Hospital site and the observed concrete infill / underpinning observed by a Rothwell engineer, at the corner of the Granite Block.

The paper details several methods for controlling groundwater for basement construction including:

- Secant piled walls
- Sheet pile cofferdams
- Jet grouting
- Ground freezing
- Grouting

Dewatering

The paper details how the TSB development used a grout curtain to cut off the outside driving head of water from the base of the excavation. This was combined with dewatering to reduce the groundwater level by 2.5m under the basement footprint [30]. This technique was successful for the TSB small scale project however potentially a more substantial method of controlling groundwater and unstable ground conditions is anticipated to be required for the larger scale Jersey General Hospital basement development. Given its proposed extend indicated on **Figure 3**.

The most likely of these options to be suggested for the Jersey General Hospital basement developments are currently secant pile walls. Further investigation into the potential for running sand needs to be undertaken to better inform future development options.

5 Ground and Groundwater Conditions

Factual records from 11No. historical ground investigations have been reviewed for the Jersey General Hospital and Westaway Court sites dated between 1973 and 2014. The records from which are provided in **Appendix D-1** and listed below.

The P02 issue of this desk study incorporates additional ground investigation information from the Patriotic Street MSCP, dating from 1983 (including 7 No. boreholes) and records from three other sites along Kensington Place and the Esplanade dating between 2007 and 2014 (including 12 No. boreholes). Details are presented in Table 1A.

The additional data have been reviewed and incorporated with the other available information.

The Patriotic Street boreholes are immediately adjacent to the site and of particular relevance. The soil and rock descriptions are considered relatively indicative in comparison to the other ground investigation information available. (BH1R, BH2 and BH4 include only limited descriptions regarding superficial deposit and made ground composition, and BH3, BH5, BH6 and BH7 have only allow very high level identification of strata). However, the GI also includes very useful information in relation to groundwater conditions, which is summarised in Section 5.1.1.

See **Appendix D** for further details.

Table 1A: Historical ground investigation records – Jersey General Hospital

GI Ref.	BH/TP Ref.	Depth (m)	Distance from site (m)	Comments				
	ON-SITE							
Foundations Engineering	BH1	10.8	Associated with Block E construction. Within proposed JFH site	Boreholes 1 & 2 located on				
Ltd, Jersey General Hospital, Phase I	BH2	11.0		Newgate Street. Borehole 3				
(6 th /12 th March 1973)	вн3	12.3	footprint.	located on central access road.				
Geotechnical Engineering Ltd, Jersey	BH1	15.2	Associated with Block F	Indicative borehole locations have been gained from the				
General Hospital, Phase IB	ВН2	15.0	construction. Within JGH site footprint.	Patriotic Street MSCP section plans. These locations have been indicatively marked on Figure 8.				
(12 th /14 th July 1979)	ВН3	13.5	-					
Geomarine Ltd, Main	BH1	12.7	Located within site footprint. Block C car	Boreholes associated with the construction of temporary				
Theatres Upgrade SI, Jersey General Hospital	TP1	0.5						
(7 th /8 th March 2014)	TP2	1.2	park.	theatre facilities.				
OFF-SITE								
Amplus Ltd, 33 Gloucester Street, Raliegh House (4th/5th February 2000)	BH1	10.1	~100m S.E	The Amplus reports don't provide locations of boreholes. Locations				

GI Ref.	BH/TP Ref.	Depth (m)	Distance from site (m)	Comments	
	BHP1	10.5		estimated from associated drawings.	
Amplus Ltd, 15-16 The Parade	BHP2	9.9	~50m S.W		
(11 th September 2006)	ВНР3	9.7			
Gloucester Street surface	BH1	8.0		No logs available. Indicative	
water sewer outfall	BH2	7.5	~10m	log summaries provided on	
drawing	BH3	8.0	S.E	the Gloucester Street surface	
(Drawing dated: 12 th January 1982)	BH4	9.0	(Gloucester Street)	water sewer outfall drawing in Appendix N.	
	BH1R	13.4		Boreholes associated with the	
	BH2	11.3		construction of the Patriotic	
Patriotic Street MSCP	BH4	10.8	~10m S.W	Street MSCP.	
(Records dated: 1983)	BH3	11.2		Lack of detailed logs did not	
(Records dated, 1965)	BH5	11.1	(Patriotic Street MSCP)	allow for differentiation	
	BH6	15.8		between strata within the	
	BH7	15.2		superficial deposits.	
Amplus Ltd	BH4300	10.3	~40m		
Kensington Gate Car Park	BH4301	10.5	S.W	Boreholes associated with the	
(8 th /12 th January 2007)	BH4302	11.0	(Kensington Place)		
Geomarine Ltd	BH4303	6.8		construction of Kensington	
Kensington Place	BH4304	7.4	~60m	Gate Car Park.	
(16 th /21 st July 2009)	BH4305	7.3	S.W		
	BH4306	6.4	(Kensington Place)		
	BH4307	8.4			
Amplus Ltd	BH4802	7.0	~60m	Boreholes located on the site	
66-72 Esplanade	BH4803	11.6	S.W	adjacent to the Patriotic Street MSCP.	
(21st March/2nd April	BH4804	7.5	S. w (Esplanade)		
2014)	BH4805	11.7	(Espianauc)		

 Table 1B: Historical ground investigation records – Westaway Court

GI Ref.	BH/TP Ref.	Depth (m)	Distance from site (m)	Comments
		W	estaway Court	
Westaway Court,	BH1	15.0	Westaway Court (see Figure 8) ~200m N.E of the JFH site	Boreholes associated with the construction of a link building forming the 'L-shaped' building.
Matthew F Warner & Associates Ltd	TP3	2.7		
(4 th /6 th January 1994)	TP4	2.5		

The approximate locations of all exploratory holes, at both sites, are shown on **Figure 8**.

5.1 Ground Conditions (Jersey General Hospital)

The ground investigation data from the investigation presented above in **Table 1A** have been reviewed and summarise in **Table 2** (provide towards the back of this report).

Since the previous issue of this Geotechnical Desk Study **Table 2** has been updated to include detailed ground investigation data from the Patriotic Street MSCP GI and 3No individual ground investigations located approximately 60m to the southwest of the Jersey General Hospital site. **Table 2** is now presented within the tables section towards the back of this report.

Ground Conditions Conclusions

A summary of the ground conditions encountered at the Jersey General Hospital site is provided in **Table 3** below.

Table 3: Summary of encountered ground conditions, Jersey General Hospital

Stratum	Description	Recorded Thicknesses (m)			
Made Ground	Fill with inclusions of brick, tiles, concrete and gravel	0.1m to 3.8m			
Blown Sand	Fine to coarse sand, with occasional silts, fine sand and gravel	0.0m to 5.5m			
Alluvium	Interbedded layers: - Cohesive: firm to stiff CLAY / SILT - Granular: medium dense silty SAND / sandy GRAVEL	3.0m to 8.3m			
Head	Encountered at the Kensington Place ground investigation (Geomarine, 2009). Composition similar to that of the alluvium. Not anticipated to be encountered beneath the JGH site. See Figure 8 for the Geomarine 2009 GI locations.				
Bedrock	Jersey Shale Formation: Southern and eastern parts of site. - Highly weathered to moderately weathered fine grained mudstones and siltstones / slightly metamorphosed mudstone Evidence of mudstones containing pyrite crystals and veins. John's Road Andesite Formation: Western corner of site Dolerite - 'Amygdaloidal lava' (Basalt)	0.3m to 4.5m proven Rockhead between 9.0m bgl and 12.2m bgl			

Refer to the geological sections 2-2 and 9-9 in **Appendix H** for an indicative representation of the anticipated ground conditions beneath the Jersey General Hospital site, and in relation to the proposed basement development.

Made Ground

Made ground encountered up to a maximum extent of 2.8m bgl. The made ground strata generally comprised fill with inclusions of brick, tile, concrete and gravel.

No visual or olfactory evidence of contamination was recorded at any of the exploratory hole locations.

Blown Sand

Blown sand deposits were encountered universally across all ground investigation locations underlying made ground and to a maximum recorded depth of 6.5m bgl. The blown sand deposits were generally light in colour and comprised fine to medium grained sands with occasional bands of silts and gravels. SPTs were carried out during the ground investigations at the Jersey General Hospital site identified that the Blown Sand superficial deposits returned N values of between 5 and 20, representative of a loose to medium dense granular material. For a visual representation of the blown sand materials refer to the construction photographs from the temporary theatres block provided in **Appendix B-3**.

Alluvium

The alluvial deposits comprised a mixture of interbedded cohesive materials (clays, silts) and granular materials (sands, gravels). The alluvial deposits are relatively extensive and extend down to bedrock (9.0-12.2m bgl). SPTs within the alluvium returned N values of between 8 and 41 consistent with a medium dense to very dense granular material or firm to stiff cohesive material.

Head

Head deposits were encountered underlying reworked blown sand made ground at the Kensington Place site during the 2009 ground investigation, see **Figure 8**. The head deposits were of a very similar description to the alluvial deposits stated above. However, the ground investigation records presented visual and olfactory evidence of hydrocarbon contamination. Consultation with the States of Jersey during the undertaking of the Environmental Statement has revealed that this evidence was a result of a past leakage/spillage and has since been remediated.

Bedrock

Bedrock surface was encountered between 9.0m bgl and 12.2m bgl across all previously undertaken ground investigations. Both the Jersey Shale Formation (meta-siltstones and mudstones) and the St Johns Andesite Formation (volcanic rock) were encountered often described as meta-siltstone / lightly metamorphosed mudstone / dolerite. Upper weathered bedrock was recovered as 'grey rock fragments in grey clay matrix' from 8.97-9.05mbgl in BH1 (2000) and 'highly weathered rock fragments in a silty CLAY' from 10.8 to 11mbgl. SPT N values of between 45 and 50 were recorded within the weathered surface of bedrock, indicating very dense or stiff materials. Pyrite veins and crystals were noted within the mudstones encountered during the 1979 Phase IB ground investigation.

Summary

The ground conditions encountered across the historical ground investigation undertaken to date presents consistent findings. Made ground is anticipated to be encountered extensively across the GJH site to a potential depth of 2.8m bgl. Loose to medium dense blown sand was consistently recorded to be present underlying the made ground, to recorded depths of between 2 and 6.5m bgl. The

blown sand was found to be relatively loose, and anecdotal evidence suggests that running sand may be a potential issue during further works if adequate controls are not incorporated into the development proposals to prevent ground loss. The blown sand was underlain by alluvial deposits comprising clay, silt, sand and gravel. The alluvial deposits are relatively extensive and overlie the bedrock with recorded depths of between 9.0-12.2m bgl. The ground investigations encountered both Jersey Shale formation and St Johns Andesite Formation beneath the site. The Jersey Shale formation was predominantly encountered in the southern and eastern sections of the site whereas the St Johns Andesite was encountered predominantly in the western corner of the site.

The previously undertaken ground investigations allow for a preliminary characteristic ground model to be idealised for design purposes, based on a reasonable 'worst case scenario' e.g. with the loose blown sands assumed to be at maximum recorded extent across the site. See the geological section drawings in **Appendix H** for the preliminary ground model. Once the proposed site specific ground investigation has been completed, the ground model can be refined further which may allow for more efficient design solutions.

5.1.1 Groundwater Conditions (Jersey General Hospital)

Table 4 below provides the recorded groundwater levels from historical ground investigation reports from the Jersey General Hospital site.

Table 4: Historical recorded groundwater levels, Jersey General Hospital

Ground Investigation	BH Ref.	Groundwater Observations
		ON-SITE
Foundations Engineering Ltd Phase I	BH1 (9.8mD)	GW strike at 1.3mD (8.5m bgl) within silty sand deposits. Subsequent GW monitoring recorded GW level at 1.5mD (8.3m bgl) within silty sand deposits. Note 2
(6th/12th March 1973)	BH2 (8.5mD)	GW strike at 1.5mD (7.0m bgl) within silty sand deposits. Subsequent GW monitoring recorded GW level at 1.8m D (6.7m bgl) within silty sand deposits. Note 2
	BH3 (10.6mD)	No GW information. Note 2
Geotechnical Engineering Ltd Phase IB	BH1 (10.3mD)	GW strike at 6.2mD (4.0m bgl) within orange brown silty sand deposits. Subsequent GW monitoring recorded GW level at 8.5mD (1.7m bgl) within fine white sand deposits.
(12th/14th July 1979)	BH2 (11.6mD)	GW strike at 7.6mD (4.0m bgl) within fine sandy clayey silt deposits.
	BH3 (10.0mD)	GW strike at 2.0mD (8.0m bgl) within brown silty sand and gravel deposits.
Geomarine Ltd (7 th /8 th March 2014)	BH1 (13.0mD) ^{Note3}	GW strike at 4.05m bgl, rose to ground level after 30 minutes (indicative of artesian conditions)
		OFF-SITE
Amplus Ltd (4 th /5 th February 2000)	BH1 (9.9mD) ^{Note4}	GW strike at 2.95m bgl, rose to 2.82m bgl in 15 minutes
Amplus Ltd (11th September 2006)	BHP1 (9.7mD) Note4 BHP2 (9.6mD) Note4 BHP3 (9.7mD) Note4	No groundwater encountered.
Gloucester Street Surface sewer drawing	BH1 (15.0mD) ^{Note1}	GW level at 2.8m bgl within sand deposits Note 1
(Drawing dated: 12 th January 1982)	BH2 (14.4mD) ^{Note1}	GW level at 2.0m bgl within sand deposits Note 1
	BH3 (13.0mD) ^{Note1}	GW level at 2.1m bgl within sandy gravel deposits Note 1
	BH4 (13.2mD) ^{Note1}	GW level at 1.8m bgl within gravelly sand deposits Note 1
Patriotic Street MSCP (Records dated: 1983)	BH1R (8.4mD)	Primary GW strike at 2.0mD (6.4m bgl) within gravel deposits. Secondary GW strike at -2.4mD (10.8m bgl) within clayey silt deposits and at head of bedrock. Subsequent GW monitoring recorded GW level at 5.0mD (3.4m bgl) within silt deposits.
	BH2 (8.8mD)	GW strike at 2.0mD (6.8m bgl) within gravelly silt deposits. GW monitoring level at 6.2mD (2.6m bgl) within silt deposits.
	BH3 (9.6mD)	GW strike at 3.0mD (6.6m bgl) within superficial deposits. GW monitoring level at 6.6mD (3.0m bgl) within superficial deposits.

Ground Investigation	BH Ref.	Groundwater Observations			
	BH4	GW strike at 2.3mD (6.9m bgl) within silt deposits. GW monitoring			
	(9.2mD)	level at 6.2mD (3.0m bgl) within silty sand deposits.			
	BH5	Primary GW strike at 1.9mD (6.9m bgl) within superficial deposits.			
	(8.8mD)	Secondary GW strike at 1.1mD (9.9m bgl) within superficial deposits.			
		Primary GW strike at 1.9mD (6.0m bgl) within superficial deposits.			
	BH6	Secondary GW strike at ² 2.2mD (10.1m bgl) within superficial deposits.			
	(7.9 mD)	Subsequent GW monitoring recorded GW level at 5.7mD (2.2m bgl)			
		within superficial deposits.			
		Primary GW strike at 2.0mD (6.2m bgl) within superficial deposits.			
	BH7	Secondary GW strike at ² 2.5mD (10.7m bgl) within superficial deposits			
	(8.2mD)	and at head of bedrock. Subsequent GW monitoring recorded GW level			
		at 5.0mD (3.2m bgl) within superficial deposits.			
Amplus Ltd	BH4300	No GW strikes recorded on log, GW depth measured as shallow as			
Kensington Gate Car Park		2.83m bgl			
(8 th /12 th January 2007)		No GW strikes recorded on log, GW depth measured as shallow as 2.0m			
		bgl			
	BH4302	No GW strikes recorded on log, GW depth measured as shallow as			
		1.46m bgl			
Geomarine Ltd	BH4303	-			
Kensington Place	BH4304				
(16 th /21 st July 2009)	BH4305	No GW strikes recorded on logs.			
	BH4306				
	BH4307				
Amplus Ltd	BH4802	No GW strikes recorded on log, GW depth measured at 3.75m bgl			
66-72 Esplanade	BH4803	No GW strikes recorded on log, GW depth measured at 1.95m bgl			
(21st March/2nd April	BH4804	No GW strikes recorded on log, GW depth measured at 4.57m bgl			
2014)	BH4805	No GW strikes recorded on log, GW depth measured at 5.47m bgl			

Note 1 - Groundwater levels gathered from States of Jersey Resources Board Gloucester Street surface water outfall drawing and accompanying note states 'The information above is the best available, however its accuracy cannot be guaranteed'. Additionally the drawing doesn't state whether the groundwater level was recorded from a groundwater strike or from subsequent groundwater monitoring.

Note 2 - Water was added to the boreholes to assist in shelling and this may possibly have disguised any slight seepages.

Note 3 - Elevations provided from Geomarine Ltd records are arbitrary values.

Note 4 – Elevation data for boreholes unavailable in records. Indicative elevations gained from GPS Geoplaner website [16].

Groundwater Conclusions

The ground investigation at the Patriotic Street MSCP in 1983 presents relatively consistent groundwater information. Primary groundwater strikes were consistently recorded between 3.0mD and 1.9mD (all between 6.0m bgl and 6.9m bgl). A secondary groundwater strike was often recorded between 1.1mD and 2.5mD (all between 9.9m bgl and 10.8m bgl). The secondary groundwater strikes were often just above the level of the bedrock within the alluvial deposits. Groundwater monitoring was installed at a selection of the Patriotic Street MSCP boreholes. Where present groundwater monitoring installations recorded a groundwater level between 6.6mD and 5.0mD (all between 2.2m bgl and 3.4m bgl) which is significantly shallower than the strike levels recorded.

The ground investigation at the Patriotic Street MSCP in 1983 also presented an interpretation of the 1973 JGH Phase I and 1979 JGH Phase IB (shown as Phase II in **Appendix D**) ground investigations. The interpretation presented detailed groundwater information that had previously not been available for review. The 1973 Phase I ground investigation recorded GW strikes of 1.3mD and 1.5mD at BH1 and BH2 respectively. Groundwater monitoring at these two locations indicated a slight rise to 1.5mD (BH1) and 1.8mD (BH2) which is considerably less than what was reported during the 1983 ground investigation. Furthermore, the 1979 Phase IB ground investigation indicated GW strikes between 7.6mD and 2.0mD.

As discussed above, there is a high level of variation in groundwater strike depths. The inconsistency in groundwater levels may be a result of tidal variation as the site is approximately 200m from the sea shore. The potential for tidally induced groundwater movement is proposed to be investigated as part of the future ground investigation.

Artesian Conditions

Groundwater at BH1 (2014) was struck at 4.05m bgl (within the alluvium deposits. A subsequent rise in groundwater level to the surface after 30 minutes is indicative of potentially artesian conditions. It is recommended groundwater monitoring is undertaken as part of an additional ground investigation in order to better understand the groundwater conditions beneath the site.

Summary

The inconsistency in groundwater observations between the ground investigations does not allow for a definitive groundwater level to be determined. However, the information gathered to date does allow for a preliminary ('reasonable worst case') ground and groundwater model to be formed. See sections '2-2' and '9-9' in **Appendix H** for a visual representation of the groundwater strikes beneath the site. The proposed ground investigation will gather further information regarding the groundwater conditions beneath the JGH site. Once the ground investigation has been completed, it may be possible to define the groundwater level beneath the site and any possible tidal variations. The groundwater information will be useful during the detailed design stage of the Jersey General Hospital development.

5.2 Ground Conditions (Westaway Court)

Table 5 below provides details on the encountered ground conditions at Westaway Court site.

Table 5: Encountered ground conditions, Westaway Court

Westaway Cou	urt, Matthew F Warn	er & Associates Ltd	(4 th /6 th January 1994)		
BH Ref. (Note 6)	Made Ground	Blown Sand	Alluvium	Bedrock	Total Depth
BH1 (13.3mOD)		Gravelly SAND with silt 0 – 3.0m	SILT, SAND and some CLAY 3.0 – 14.3m	Strong Igneous Rock 14.3 – 15.0m	15.0m
TP3 (13.1mOD)		Topsoil, Brown fine SAND 0 – 2.6m	SILT with some organics 2.6 – 2.7m		2.7m
TP4 (13.4mOD)	Brick, stone gravels. Slightly organic 0 – 1.4m	Off-white SAND 1.4 – 2.5m			2.5m

Note 6 – Elevation data for BH unavailable in records. Indicative elevation gained from GPS GeoPlaner website [16].

Table 6 below presents a summary of the data gathered from the aforementioned exploratory holes.

Table 6: Summary of encountered ground conditions, Westaway Court

Stratum	Description	Thickness
Made	Fill with inclusion of brick, concrete and gravel	0.0 to 1.4m
Ground		
Blown	Fine to coarse sand, with occasional silts, fine sand and gravel	1.1m to 3.0m
Sand		
Alluvium	SILT, SAND and some CLAY	11.3m
Bedrock	Strong Igneous Rock	0.7m proven
		Rockhead at 14.3mbgl

5.2.1 Groundwater Conditions (Westaway Court)

Groundwater was struck at 13.6mbgl within silts and sands underlying silty clays. The borehole record details fast inflow once groundwater was struck resulting in a rise to 7.5mbgl. A standpipe was installed to 5.0m bgl and subsequent groundwater monitoring recorded the groundwater level at 2.0mbgl.

6 Radon

Information for Radon on Jersey and the site area have been gathered from the Review of radon in the States of Jersey report for the environmental scrutiny panel [18], discussion with States of Jersey Department of the Environment, Environmental Protection and review of BRE211 [33].

Radon is a natural radioactive gas, which has no taste, smell or colour. It is produced by the radioactive decay of uranium and thorium, present in all soils and rocks in small quantities. There are a number of different isotopes of radon but the most important is radon-222 [18].

The geology on the Island of Jersey is similar to that found in areas of the South-West of England where the most recent mapping of Radon potential shows a high proportion of homes with a 30% or greater chance of a radon level that exceeds the Action Level [18].

Reports provided to the States of Jersey suggest that the granites in Jersey are similar to those in the South-West of England but older. The granites are also highly fractured which gives rise to pathways for the release of the gas to the surface which could give higher radon concentrations in buildings [18].

A three phase test of radon on the island of Jersey was carried out between 1987 and 1992. The first phase tested 30 homes across the island begun in 1987. The measurements were taken over 3 months and the results of the test revealed that 10% of the homes had radon levels in excess of the 200 Bq m⁻³ Action Level [18].

The second phase of testing focused on the homes that were close to the homes with higher measurements from the initial test and two underground workspaces were tested. These measurements were taken over a longer 9 month period and the results indicated 36% above the precautionary radon level of 200 Bq m⁻³ [18].

The third phase focused on testing of homes in St Helier. 24 homes and 5 schools were tested in 1992 with all of these dwellings testing below the Action Level of 200 Bq m^{-3} [18].

This last phase of the test is the most significant as it focuses on St Helier which is the town where the proposed sites are located. However, the States of Jersey state that 'all new houses built in Jersey must now be protected against radon' [3]. Therefore, full radon protective measures are required for the construction of the Jersey General Hospital new buildings.

Radon protective measures may comprise of gas tight membranes below all slabs and sealing of incoming services. A cost allowance should be made for gas protective measures including ground sumps. Regulatory communication in 2014 on Radon is provided in **Appendix L**. Regulatory requirements are to be confirmed [19].

7 Unexploded Ordnance (UXO)

There is no available published UXO mapping for Jersey General Hospital and Westaway Court.

Historical searches of Jersey and WWII suggest that Jersey was bombed by German aircrafts in June 1940 [2]. However it is widely known that no significant bombing took place on the island, rather occupation by the Germans. From further review of historical documents [13] [14], there is evidence that the Channel Islands were occupied by the Germans forces post 1940. This considerably lowers the risk of potential bombing by German aircraft and the risk of subsequent bombing from Allied aircraft is highly unlikely due to the islands British population majority. Their occupation ended in 1945 when Jersey was liberated.

Review of published historical sources at Jersey Archives has not revealed any evidence of bombing or identified UXOs at the two sites.

No evidence of building damages or surface depressions that could be associated with bombing was identified during the review of the aerial photos for the two sites (included in **Appendix C-2**). However, it must be noted that a limited number of aerial photos were available and no adjacent frames were available to allow a 3D view with a stereoscope.

The ground conditions at the two sites do not lend themselves to the risk of buried UXO (e.g. no soft ground).

Jersey General Hospital site has been continuously developed since the late 1700's, with substantial development within the entire site occurred in the second part of last century.

In light of the above, the risk of UXO at both sites is considered to be low.

8 Hydrogeology

Hydrogeological data has been gathered from the review of a Hydrogeological Map of Jersey from 1991 on the BGS website [17]. No digital data for Jersey is available and therefore the review of the hydrogeology is rom a scanned map. An extract of this map is presented as **Figure 9**. The drift and solid data from the map has been analysed and is presented below:

8.1 Drift (Superficial Deposits)

The majority of the Jersey General Hospital site is underlain by a blown sand aquifer, see **Figure 9**. It forms as a shallow productive aquifer yielding between 1.9-6.3 l/s. Average daily abstraction is around 1500m³/d but an additional 600m³/d is available before imposing any stress on the saline interface.

Beneath the blown sand deposits and under the Westaway Court site is an Alluvium based aquifer. It is generally 8-10m thick with gravels occurring in the lower 3m of the sequence. The hydraulic conductivity of the silty alluvium is generally of the order of 10⁻³m/d whereas the gravel section has a much higher hydraulic conductivity of 10-20m/d.

8.2 Solid (Bedrock)

The Jersey General Hospital site lies on the boundary between the Volcanic Group and the Jersey Shale formation, with the Westaway site above the Jersey Shale formation see **Figure 9**.

The Volcanic Group is a thick rhyolite and andesite volcaniclastic sequence deformed by a number of fold structures, minor faults and locally developed cleavage. Sustainable borehole yields range from 0.1-0.6 l/s however higher sustainable yields have been achieved meaning the average value for borehole specific capacity is 1.2 l/s/m. Hydraulic conductivity in the Volcanic group ranges from 0.2m/d to 13m/d.

The Jersey Shale Formation consists of highly indurated very fine to medium-grained sandstone units with subordinate mudstones and conglomerates, metamorphosed to low green-schist facies. Secondary permeability is available is the uppermost 40m derived from faults and fractures. Mean sustainable yield of boreholes is 0.6 l/s with the mean borehole specific capacity is only 0.6 l/s/m. The hydraulic conductivity is of the order of 1-10m/d.

The interaction between the Drift and Solid formation under and around the two site areas can be seen on the extract from the Hydrogeological map of Jersey [17] **Figure 9**.

8.3 Data Extracts

The Hydrogeological Map of Jersey (1991) also provides useful data on pH, total dissolved solids and annual rainfall. This data is presented in this section, however

further ground investigation will provide more relevant data for pH and the total dissolved solids in the immediate site vicinity.

pН

The pH ranges from 4.5 to 8.0 across the whole of the Island however within the vicinity of the site the pH range is between 7.0 and 7.5, therefore neutral to slightly alkali.

Total Dissolved Solids (TDS)

The area of the Island which has the highest level of TDS is the south-eastern tip with 1300-1600 mg/l; this is associated with marine intrusion and sea water contamination in this area. However the TDS on site is considerably lower with levels ranging from 500-700 mg/l.

Average Annual Rainfall

The average annual rainfall in St Helier ranges from 800mm towards the southern end of the town and 875mm in the northern boundaries of the town near St Saviour. Focussing on the site area, the average rainfall ranges from 825-850mm for both the Jersey General Hospital site and Westaway Court site.

9 Hydrology

9.1 Surface Water Features

From review of aerial photography and the Jersey Water Stream Nitrate map [35] has revealed the following hydrological features relating to the Jersey General Hospital and Westaway Court sites.

St Aubins Bay is located approximately 200m to the southwest of the Jersey General Hospital site.

The confluence between the Grands Vaux and Vallee des Vaux streams is located approximately 1.1km to the northeast of the Jersey General Hospital site. The Jersey Water Stream Nitrate map [35] shows the streams ending at the confluence location. This suggests that the streams are then culverted beneath St Helier before discharging out into St Aubins Bay. See the sub-surface water features section below for greater detail on the below ground water features.

No other surface water features are present within proximity to either the Jersey General Hospital site or the Westaway Court site.

9.2 Sub-Surface Water Features

9.2.1 Jersey General Hospital

Information regarding all available data on current sub-surface water features has been gathered from States of Jersey DfI (Department for Infrastructure - formerly known as Transport and Technical Services T&TS) drawing showing the Jersey General Hospital Site which can be found in **Appendix G**. For details of the existing drainage features, reference should be made to the separate drainage drawing SK100 which is currently being prepared by Arup civils at the time of writing.

The drawing provides the routes of foul sewers, storm sewers, old brick sewers and the route of the town brook (Le Faux Bie). Presented below is a summary of the data gathered from the drawing:

Le Faux Bie (Town Brook)

Originally the 'Le Faux Bie' stream ran through the area of St Helier where the Jersey General Hospital site is located. At some point during the development of this sector of the town the stream was culverted. The known route of this culvert is shown in **Figure 10**. The culvert comes towards Gloucester Street in a north-westerly direction before turning ~90° to flow along the line of Gloucester Street in a south-westerly direction. Amendments were made to the route of the culvert in 2004, also shown on Figure 10, to straighten the route. From manhole cover and invert levels it is estimated that the culvert is between 2.3 – 2.5m bgl around the area of the Jersey General Hospital site. Drawing E1-7 (**Appendix E**) shows a culvert plan beneath 6-14 Gloucester Street to the west and a selection of culvert sections along the length shown on the plan. The drawing was produced and

provided by Rothwell & Partners Ltd and has no drawing title however it is dated Feb 2006 it is referred to as Culvert details in this report [30]. The culvert is a brick arched structure, however a smaller oval shaped culvert is evident within the old culvert. Rothwell have provide photographs from an investigation showing that the space between the oval culvert and the original brick arch culvert has been infilled with concrete.

Foul Sewers

The foul sewer network runs almost around the whole site. Running underneath The Parade is a 530mm ø concrete foul sewer at an average depth of 4m bgl. This foul sewer then joins into a 1000mm ø glass reinforced plastic (GRP) sewer at the cross-roads between The Parade and Gloucester Street before then running under Gloucester Street in a south-westerly direction. The sewer remains 1000mm ø GRP before downsizing to a 600mm ø GRP pipe which flows under Gloucester Street until it meet the culverted brook which it discharges into. The average depth of the sewer below Gloucester Street is 2.6m bgl. A smaller foul sewer network runs along Newgate Street in a south-easterly direction towards Gloucester Street where it also discharges into the culverted brook. The sewer starts out at 150mm ø then up-sizes to 230mm ø before finally up-sizing to 300mm ø with an average depth of 1.75m bgl. The routes of all foul sewers mentioned can be seen on the drawing in **Appendix G**.

Surface Sewers

There is a lined 1525mm ø diameter surface water sewer that runs underneath Gloucester Street which has an average cover of 5480mm (5.48m). The routes of the surface water sewer network can be seen on the States of Jersey drawing in **Appendix G**, drawing dated 11/02/2015. A detailed plan and section drawing of the surface water outfall can be found in Appendix N along with 4 borehole records from along Gloucester Street, as mentioned in the ground conditions section above. The Gloucester Street surface sewer outfall drawing in **Appendix N** was provided by DfI on the 8/11/2016. Both drawings in **Appendix G** and **Appendix N** have been reviewed and the drawings show the same alignments of the surface water sewer beneath Gloucester Street.

Old Brick Sewers

There are brick sewer networks around the Jersey General Hospital site. To the south-west of the site a brick sewer starts on Newgate Street before turning under Patriotic Street. The brick sewer flows underneath Patriotic Street until it reaches the turning on to Patriotic Place where it joins another brick sewer and flows down Patriotic place. The brick sewer then eventually discharges into the culverted brook just before it reaches Gloucester Street. The average depth of this sewer, according to the source drawing is 2438mm (~2.44m).

Under Kensington Place a brick sewer network flows from north-east to south-west. The average depth of this network is between 4.1 - 4.2m and the network has a series of road gullies and other drainage running into it along its length.

A small brick sewer runs underneath Gloucester Street collecting water from road gullies and other drainage sources before eventually feeding into the culverted

brook. An average depth for this sewer is not presented on the current drawing and therefore the depth of this sewer is currently unknown.

The route of all the sewers and other sub-surface water features can be seen on the States of Jersey drawing in **Appendix G**.

9.2.2 Westaway Court

States of Jersey drawings provided in **Appendix G**, show storm and foul drainage with the site associated with the downpipes from the buildings. Refer to Arup site development and civils team report on the existing drainage [32].

10 Contamination and Ground Gases

Made ground is anticipated at both sites associated with historical and existing land use.

Proposed foundations solution, anticipated to be required by the regulatory authorities include the following:

- Foundation works risk assessment
- Ground gas assessment
- Soil risk assessment
- Groundwater risk assessment

Regulatory requirements should be further understood as part of the planning process. It is anticipated the regulator will apply ground related conditions to planning associated with satisfying regulatory and legislative requirements of the above.

Soil arisings will be generated from piling works, excavations for the new basement, foundation excavations, utility trenches and other excavations on the sites. It is unlikely that made ground could be reused as selected fill on account of historical land uses including demolition and current land use activities. However there is a potential that natural ground or possibly demolition rubble may be suitable for reuse, subject to appropriate testing and compliance with the regulators. Reuse might include piling mats etc or localised infill materials. Due to the limited space on the site and the active hospital, any sorting and screening to render materials suitable for reuse is anticipated to be undertaken off site, possibly at a local off site compound. A large volume of natural superficial deposits are anticipated to be generated as part of the basement construction works. Reuse of this volume of material may be explored at a suitable potential off site receptor. Suitability of reuse will need to be confirmed by appropriate geotechnical and geo-environmental risk assessments accordingly to its proposed end use and setting. There is a requirement for targeted ground investigation to determine the nature and composition of the ground to be excavated. It is anticipated the States of Jersey (SoJ) will require a material management plan for such materials, such as potential for re-use (such as piling mat), off-site disposal to landfill, remediation and / or treatment. For natural materials in particular, its anticipated diversion from landfill will be sought, particularly for natural materials, which is likely to attract both cost savings and carbon reduction efficiencies.

Jersey General Hospital Specific

The historical ground investigations identified no evidence of contamination. However, there is a potential for contamination sources associated with the historical and current use of the site (e.g. tanks, storage of chemicals, etc.).

Further consideration with regards to potential contamination will be addressed as part of the detailed ground investigation.

The Engineering block (Block G) contains two large oil tanks and four boilers within the block. Currently the development doesn't include Block G, as of the latest plans, however care must be taken during demolition as the demolition boundary currently runs along Block G's south-western edge. See **Figure 11** features and constraints plan.

The service road that runs along the north-western edge of Blocks E and F is currently being used as medical oxygen_storage, see site photos 6 and 7 in **Appendix B-1**, so this must be taken into account during any future ground investigation. Other medical gases are stored in a dedicated store adjacent to the existing site entrance gates.

Westaway Court

Historical mapping review of Westaway Court site indicates the site has been occupied by buildings since earliest plan date 1795. Made ground is anticipated to be encountered associated with demolition and construction works. The present day land use comprises residential hospital staff accommodation.

Based on available information, potential for contamination is anticipated to be low, however a potential risk remains. It is recommended that the chemical characterisation of the ground and groundwater conditions is undertaken as part of the scope of the ground investigation works.

11 Review of Existing Foundations

11.1 Jersey General Hospital

The approximate extents and locations of the existing piled foundations and basements have been determined by analysing all available record drawings, see **Appendix E**. Generally basements exist under the whole of Block B and Block C (Granite Block) with basements under parts of Block E and Block H.

11.1.1 Existing Foundations

Existing Buildings

A summary of foundation information available for the existing buildings on the site is provided in **Table 7** below and the existing building layout is shown on **Figure 2**.

Table 7: Existing Building Foundation Information – Jersey General Hospital

Building	Foundation type	Foundation Drawings / Info	Drawing dates
Block A	Piled foundations	No foundation records	Proposed construction
(Phase 2)		available.	drawings dated 1983, 1984, 1985.
Block B	Pad foundations	No foundation records	Proposed construction
(1960s wing)		available.	drawings dated 1958 to 1960.
Block C (Granite	The Granite building was	No foundation records	Not available.
Block)	constructed in 1768, pad	available.	
	foundations are anticipated.	Basement under part of	
		building (see Figure 5).	
		Listed Building.	
Block D (Peter Crill	Assumed piled based on	Column layout drawings, see	2007 - 2016
House)	column layout, refer to	Appendix E1	
	Appendix E1		
Block E (Gwyneth	Piled foundations and	Drawings available dated	Proposed construction
Huelin Block Phase 1)	basement	1975/76, see Appendix E1	drawings dated 1973 to 1977
Block F	Piled foundations	Pile layout drawings dated	Proposed construction
(Lab Block – Phase		1980, see Appendix E1	drawings dated 1979 to
1B)			1980
Block G -	Assumed piled based on	Pile layout drawings dated	Proposed construction
Engineering Block	column layout, refer to	1978, see Appendix E1	drawings dated 1978
(Phase 1A)	Appendix E1		
Block H - Daycare	Piled Foundations and	General arrangement	2007
	basement.	drawings, see Appendix E1	

11.1.2 Review of construction drawings

All relevant available construction drawings have been reviewed and the findings are presented below. A list of construction drawings can be found in **Appendix A**

Key Supporting Documents, with the relevant construction drawings themselves found in **Appendix E**.

Block H - Daycare

From review of documents E1-1 to E1-4 the locations of piles and pile caps for southern section of Block E and Block H have been identified. Drawings E1-1 to E1-3 are for the construction of Block H. E1-1 shows the existing pile cap locations, also shown in E1-4, and shows the location of a new pile cap with 2No. 300¢ piles located adjacent to the large central pile cap shown on E1-4. This pile cap supports a 203 UC 71 which is used to support the western most wing of the Block H development [20][21][22][23].

Drawing E1-1 also shows the edge of a ground beam between Block H and the Granite block (Block C) [20].

Block E – Gwyneth Huelin Block

Documents E1-5 and E1-6 are pile layout drawings provided by Edwards & Blackie. They provide the pile locations for the Gwyneth Huelin Block (Block E) which finished construction and was opened in 1979. Drawing E1-6 states that the max pile capacity for the piles for this wing is 50 tonnes [25].

Block D - Peter Crill House

Unfortunately no pile layout drawings have been provided for this building, an indication of the pile locations have been assumed based upon the column layouts shown on drawings E1-1, E1-2 and E1-10. This may impact the construction of the new development as one of the proposal options is for Block D to be demolished along with Blocks E, H and parts of Block F. The existing piles may present obstructions to new piling and construction works.

11.1.3 Existing Basements

The extent of the existing known basements at the Jersey General Hospital site is shown on **Figure 6**. There is a known basement underneath Block C which is most likely the first basement constructed on site. There is a basement under Block B, the 1960's wing, but this area of the site isn't part of the initial development. Block C's basement was then most likely knocked through during the Phase 1 development, constructed in the 1980's, to form the basement under Block E. Connected to the Block E basement is a basement car parking area as seen in site photos 14, 15, 16 and 17 in **Appendix B-1**. There is also a small basement area under the north-western edge of Block E. The exact construction date of Block H is currently unknown but construction drawings from 2007 indicate the construction happened around this time. The basement extent also extends under Block H as indicated on **Figure 6**. The main areas of basement that will constrain the development are those under Blocks C, E and H as this is the main area where development is taking place as shown on **Figure 3**. This is discussed further in the engineering considerations section below.

There is also the possibility that basements exist under the hotel buildings that are along Kensington Place which are planned to be demolished along with Blocks D,

E and H as part of the development. Although from site walkover this is considered unlikely, this should not be totally ruled out as construction drawings for the properties off Kensington Place are not currently available to confirm otherwise.

11.2 Westaway Court

Limited record drawings are available for the Westaway Court site, however an Arup calculations and sketches document dated 1992, provides relevant information on the proposed piled foundations for the extension structure between the original existing Blocks A and C.

Table 8: Existing Building Foundation Information – Westaway Court

Building	Foundation type	Foundation Drawings /	Drawing dates
		Info	
Block D	Piled	Pile layout drawings dated	Proposed construction
		1993, see Appendix E2	drawings 1993
Block C	Piled	Pile layout drawings dated	Proposed construction
		1974, see Appendix E2	drawings dated 1974

The relevant information is presented below and extracts of the Arup calculations and drawings document are provided within **Appendix I**.

11.2.1 Existing Foundations

An Arup calculations and drawings document makes reference to the Westaway Court foundations, see **Appendix I**. A technical note was written by Colin Roberts who gathered the information from Bill Grose (London Geotechnical Group – Arup). Bill Grose's recollection was that the foundations were piled and comprise of 450mm ø to 600mm ø CFA piles bored into bedrock. There are concerns over the end-bearing of the piles and the capacities of each pile are 'limited to 500kN or 700kN'.

As part of the Westaway Court calculations and drawings document there is a preliminary pile layout sketch showing the pile locations and pile caps for the extension between the original Blocks A and C. The piles are 600mm ø CFA bored with a depth taken as 15m based on information from nearby sites. However the depths could be different, as the depths were subject to a past proposed site investigation. The pile caps are 600mm square and 500mm deep with 500mm deep by 300mm wide ground beams spanning between them.

12 Preliminary Geotechnical Considerations

12.1 General Considerations

Geological Summary

Historical ground investigations indicate made ground up to around 1.5m deep, Blown Sand (comprising fine and medium silty sand) up to 4m deep and Alluvium (comprising sand and gravel with laminated silt) up to 10m deep. The north-western of the site is underlain by John's Road Andesite Formation and the south-eastern part of the site is underlain by Jersey Shale Formation (comprising mudstone and siltstone). Groundwater strikes typically at 4mbgl, although one historic borehole struck groundwater at 4mbgl which then rose to surface. The potential for artesian groundwater conditions cannot be ruled out at this stage, and further investigation of this is recommended as part of the scope of ground investigation works.

Preliminary Assessment of Characteristic Parameters

A preliminary assessment of the characteristic parameters for design has been undertaken, based on limited ground investigation information available. The superficial materials, including made ground and blown sand have been assumed to be predominantly granular. The preliminary parameters presented in **Table 9** below have been derived using guidance from BS8002:1994 for granular soils. Parameters will need to be confirmed as part of the scope of the ground investigation works.

Table 9: Preliminary Assessment of Characteristic Soil Parameters

Stratigraphy	Characteristic parameters
Made ground	$\Phi = 35^{\circ}$
	$\gamma = 18 \text{ kN/m}^2$
	C' = 0
Blown Sand	$\Phi = 35^{\circ}$
	$\gamma = 18 \text{ kN/m}^2$
	C' = 0
Alluvium	$\Phi = 35^{\circ}$
	$\gamma = 19 \text{ kN/m}^2$
	C' = 0
Weathered John's Road Andesite	$\Phi = 35^{\circ}$
Formation	$\gamma = 22 \text{ kN/m}^2$
Weathered Jersey Shale Formation	C' = 5 kPa

Structural Assumptions & Assessment

A summary of the structural assumptions and assessment section from a technical note document issued 06/07/2016 is provided below [19]:

Typical column working loads are anticipated to be approximately 7500kN. Based on this and available geotechnical information it is assumed that 750mm diameter CFA piles will be used. A typical column is therefore likely to needed to be supported on a 4 pile group of around 18-20m in depth with a 7-9m deep rock socket. This means that there will be approximately 1 pile per 10-15m² [19].

It is known that some of the existing buildings on the site are piled and as such these will present a constraint to the foundation design of the new buildings such that new piles may not be able to be placed in the most advantageous positions with a subsequent requirement for a more complex substructure. There is the potential to consider re-use of the existing piles, but this would require detailed investigations after demolition of the buildings. Given the programme requirements, it may not be possible to assess this and incorporate into the new build design in any case [19].

The extent and depth of the new basement is still to be confirmed. However, it is assumed that an excavation of between 5-6m will be required typically where basement is required with lift pits locally around 1.5m-2m deeper. It is recommended that the basement retaining wall be kept a minimum of 10m away from existing site perimeter and structures, and ideally as far from the site perimeter as practical. This will minimise the risk of undermining or the effects on existing structures/highway [19].

It should be noted, however, that given the ground conditions, excavation, even in an open cut, could potentially be difficult due to the presence of running sands, as mentioned below, and shallow groundwater that may be confined and under pressure. These conditions would increase the need for enhanced temporary works and dewatering during construction and should be noted. It may also be necessary to install movement monitoring on surrounding buildings and highway during the basement excavation and construction [19].

The opportunity to re-use demolition materials as fill on the site could be investigated further presuming a suitable location for crushing/stockpiling is identified [19].

Running Sand

Anecdotal evidence indicates during the construction of the existing basement to the north-west of the Granite Block there was a loss of material described as 'running sand' from the corner of the Granite Block resulting in movement and cracks forming in the Granite Block. The Granite Block was underpinned with concrete. No further details are currently available on these works.

The risk of running sand is therefore high in this area of the site, marked on **Figure 11** features and constraints plan, but as well as this there are large known deposits of blown sand across the Jersey General Hospital site. Because of this and the fact that previous running sand has been encountered leads to an increased risk of running sand being found elsewhere across the Jersey General Hospital site, in particular associated with the existing Pathology functions, which are adjacent to the Granite Block.

Further ground investigation will confirm the extent of blown sand under the site and therefore inform regarding the most likely locations for other areas of running sand.

Patriotic Street Car Park Retaining wall

The western boundary corner of the Jersey General Hospital site is quite complex and will require thorough consideration before the appropriate development

solution is decided. Currently there is a difference in ground levels between the Patriotic Street multi-storey car park and the existing hotel buildings scheduled to be demolished. The hotel buildings are at a higher ground level and a retaining wall structure lies between the hotel buildings and the MSCP, with the MSCP at a lower ground level; see site photos 9, 11 and 12 in **Appendix B-1**. The retaining wall structure is currently being supported by the MSCP (from visual evidence) with a series of concrete props in the tapering gap between the two structures; see photo 9 in **Appendix B-1**.

The proposed development will have a service yard in an under-croft part of the new development, this area will have large trucks manoeuvring and driving in and out. The current retaining wall structure will most likely be inadequate for the trucks and new columns and piles will need to be built in the vicinity of the retaining wall to support the new structure. Because of this the retaining wall will most likely also be demolished during the demolition phase and a more appropriate structure will be built as part of the new development. This area may also be demolished to the level of the MSCP for the construction of a basement structure to hold plant facilities.

However due to the difference in ground levels in this part of the site and the presence of the existing hotel buildings, development in this corner of the site must be carefully considered as mentioned earlier.

Reuse of Existing Piles

The reuse of existing piles is considered to be potentially advantageous given the highly developed and compact layout of the current site buildings. The redevelopment of the site is anticipated to be undertaken in a phase approach.

Indicative existing pile locations based upon available proposed engineering drawing records showing either proposed pile locations or proposed column layout is provided on **Figure 11**. Review of this figure shows a dense pile layout across the proposed hospital footprint, including proposed basement. In addition, depths and diameters of existing piles are not available.

The potential feasibility of reuse of existing piles should be considered in greater detail when the redevelopment proposals are firmed up and more detailed overlays of the existing building footprints and proposed basement extents can be undertaken.

Potential Piling Issues

Issues associated with piling are likely to include the following:

- Selection of appropriate piling methods to control vibration and noise.
 - o Potential issue for existing sensitive clinical services and equipment at the hospital (assuming a phased approach)
 - Potential impact on site neighbours, adjacent utilities, foundations, structures, basements and adjacent buildings, in particular the existing Granite Block (which has been underpinned at the northwestern corner when the existing block was constructed).

• Potential obstructions, which may require the pile layout to be designed around existing foundations that cannot be easily removed

Basements

The known basement extents for the Jersey General Hospital are shown on **Figure 6**. The demolition of Blocks D and E will interact with the basement structures. Other buried obstructions are anticipated to exist which may present issues during demolition and construction; such as old foundations, utilities, tanks and storage facilities associated with hospital services and acquired buildings off Kensington Place.

Ground and Groundwater Conditions

Bedrock was encountered between 8.75m and 12m below ground level in the boreholes excavated within the southern and eastern parts of the site. No ground investigation information is known to be available in the north-eastern part of the site.

Groundwater was encountered at shallow depth in BH1 sunk in 2014. During drilling groundwater was struck at 4m and rose to the surface after 30 minutes. No groundwater observations are recorded in the three other boreholes excavated at the site. No groundwater installations are known to exist at the site.

Existing crane pad / base and associated piles within Gloucester Street Car Park:

The approximate location of existing base and associated piles are indicated on Figure 11. A piled crane base was constructed for a tower crane during the Day Surgery extension (Block H) project, indicated on **Figure 2**.

13 Recommendations for Further Investigation

13.1 Jersey General Hospital

General Site Area

The Jersey General Hospital site is an active health care facility that is densely packed with existing buildings constructed at differing periods of time. Review of the historical borehole records (discussed in Section 5) confirms the geology beneath the south-eastern and western parts of the site, however further investigation and testing of bedrock at depth will be required when the building proposals are firmed up.

The groundwater regime beneath the site requires further understanding. It is understood the site may be impacted by saline intrusion, however it is unknown whether the groundwater beneath the site is tidally induced. It is recommended this is investigated during intrusive investigations through installation of tidal inducer monitoring.

Further investigation should be undertaken to understand the possible extent of running sand across the Jersey General Hospital site. Records of running sand have been reported during the Phase 1 construction in the 1970's when running sand caused the western wing of the Granite block to be displaced resulting in cracks. This was remedied with concrete to underpin the structure however, due to the deep deposits of blown sand under the Jersey General Hospital site, investigation must be undertaken to determine if running sand exist anywhere else beneath the site. It is recommended that investigation techniques are discussed with the GI contractor to ensure the most suitable methods are used to investigate running sand.

It is anticipated that when the proposed building details such as dimensions and loads, etc are confirmed, and the demolition and construction programme is known, ground investigation, pile geometry and integrity testing of the existing piles may be undertaken. Only then can the potential reuse of the existing foundations be fully investigated.

The log of BH1 sunk in 1979 reported the Jersey Shale Formation, described as a dark grey lightly metamorphosed mudstone to include bands of pyrite crystals. The potential for expansive properties associated with the presence of pyrite should be further investigated as part of any ground investigations.

In addition there is a need for assessment of characteristic parameters for design, using SPTs in boreholes, index tests including PSDs, Atterbergs of any cohesive material encountered and descriptions from logs.

13.2 Westaway Court

Demolition and new build is proposed at Westaway Court. Review of available record drawings indicate the residential hospital staff accommodation Blocks A to D are piled.

It is envisaged that any new construction will required a piled foundation solution. Ground investigation is required to inform the foundation design, geotechnical and geo-environmental considerations.

13.3 Indicative scope of investigations

It is understood that the hospital will remain active throughout the demolition and construction phases of the project. Given the densely developed proposed new hospital footprint, there is limited space and opportunity to undertake GI.

A phased intrusive investigation approach is recommended as follows:

- **Phase 1**: undertake GI in accessible areas of the existing active hospital sites
- Phase 2: anticipated to be undertaken during the early phase of demolition at the Jersey General Hospital site. In particular, there is no ground investigation information available for the existing sites off Kensington Place. Although review of historical borehole records south-west of the site indicate ground conditions to be relatively consistent
- As a minimum ground investigation works are proposed to determine the following:
 - Ground and groundwater conditions, including allowance for tidal monitoring
 - o Geotechnical properties of the superficial deposits and the rock
 - Geo-environmental characterisation of the made ground and natural deposits anticipated to be excavated as part of the basement excavations
 - Buried concrete design

The ground investigation is specified in a separated document [34], issued on 20/12/2016 and is / has been tendered to two GI contractors.

The proposed ground investigation locations are annotated on **Figure 11** features and constraints.

Phase 1 ground investigation is proposed to include 5No. boreholes at Jersey General Hospital (possibly a 6th subject to land access arrangements) and 3No. boreholes at Westaway Court.

Phase 2 ground investigation proposes 4No. boreholes at Jersey General Hospital, in the locale of the existing hotel buildings off Kensington Place, across the northern part of the proposed new hospital building footprint.

Proposed boreholes are recommended to include excavation by methods of cable percussive with rotary coring follow-on, including groundwater and ground gas monitoring installations, with sampling and in-situ testing.

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Tables

Tables

Table 2 Previously Encountered Ground Conditions. Jeresey General Hospital

GI Ref.	BH ID	GL (mD)	Depth (m)	Made Ground (m bgl)		al Deposits	Bedrock (m bgl)	Additionl Observations	SPT
0.7 1.6.1	D11 1D	GL (III)	Depth (m)	Ground (in bg.)	Blown Sand (m bgl) ON-SITE	Alluvium / Head (m bgl)	Deutsch (m bgt)	- rudiusii obser rudons	U1 1
Foundations Engineering Ltd Note 1 Jersey General Hospital Phase I (6-12 March 1973)	ВН1	9.8	10.9	GL-0.4: Tarmac overlying compacted sandstone gravel	0.4-2.8: Medium dense light brown fine sand with pebbles 2.8-3.7: Loose light brown silty sand	3.7-4.5: Firm light brown sandy very silty clay clay 4.5-5.5: Medium dense brown silty clayey sand 5.5-6.1: Firm to stiff silty grey clay 6.1-7.6: Medium dense sandy gravel 7.6-8.1: Firm grey silty clay 8.1-8.5: Medium dense sand 8.5-9.0: Firm grey clayey laminated silt 9.0-10.2: Stiff grey slightly silty clay with fine gravel	10.2-10.9: Hard dark grey fractured and weathered fine grained mudstone		Blown Sand N = 5 to 20 Alluvium N = 22 to 24 Bedrock N = 45 to 50
	вн2	8.5	11.0	GL-0.8: Tarmac overlying roadbase material and crushed granite	0.8-3.9: Medium dense light brown silghly silty fine to medium sand	3.9-5.6: Soft to firm brown sandy silty clay 5.6-6.4: Soft to firm brown grey sandy silt 6.4-7.0: Medium dense light brown fine to medium sand 7.0-7.9: Firm green/brown/grey clay 7.9-8.5: Medium dense sandy gravel 8.5-9.4: Soft to firm grey clay 9.4-10.4: Stiff brown silty clay with traces of gravel	10.4-11.0:Hard grey slightly weathered dolerite broken with clay smears		
	ВН3	10.6	13.9	GL-1.4: Concrete ducting overlying brown sand with gravels and brick	1.4-2.7: Dense light brown silty fine to medium sand 2.7-4.1: Medium dense dark brown clayey silty sand with some organic matter	4.1-5.0: Firm brown yellow sandy clay 5.0-6.8: Medium dense brown grey silty sand 6.8-8.5: Firm to stiff light grey sandy silty clay 8.5-9.8: Medium dense sandy gravel 9.8-11.3: Firm grey very silty laminated clay 11.3-12.0: Stiff grey/green/brown clay 12.0-12.4: Dense gravel and cobbles	12.4-13.9: Dolerite Refer to Appendix O		
Geotechnical Engineering Ltd Jersey General Hospital Phase IB (12-14 July 1979)	вні	10.3	15.2	GL-1.0: Made ground with some brick and gravel	1.0-4.0: Medium dense becoming looser white fine sand 4.0-6.5: Medium dense orange brown silty fine sand with occasional band of gravels and silts.	6.5-8.0: Medium dense orange mottled grey fine sandy silt with iron stained patches 8.0-8.3: Medium dense grey green mottled orange silty fine sand and fine gravel 8.3-9.6: Dense grey silty fine sand and fine gravel 9.6-11.0: Firm grey laminated fine sandy silt with pale grey fine sand laminations, dark grey clayey silt bands and some black organic inclsuions. Occasional rounded fine gravel. 11.0-12.2: Completely weathered rock. Very stiff grey mottled yellow grey clayey sandy silt with strong iron stained fragments of meta-siltstones.	12.2-12.75: Highly weathered iron stained fragments of meta-siltstones 12.75-14.2: Completely weathered very weak pale grey fine grained gravel meta-siltstone fragments in a silty clay matrix 14.2-15.2: Moderately weathered very strong pale greenish grey lightly metamorphosed chloride rich mudstone with calcite crystals, occasional pyrite and numerous calcite veins.	Indication of pyrite within mudstone bedrock stratum (14.2- 15.2m bgl)	Made Ground N = 17 Blown Sand N = 5 to 17 Alluvium N = 8 to 41
	вн2	11.6	15.0	GL-1.2: Sand with some gravel and brick fragments 1.2-1.8: Yellow brown very silty fine sand with some poorly cemented patches 1.8-2.8: Pale yellow grey and brown mottled fine and medium sand (Reworked blown sand).	2.8-3.3: Loose pal yellow fine sand 3.3-4.5: Medium dense to loose yellow and brown medium and fine sand	4.5-8.5: Medium dense greenish grey in places mottled orange poorly laminated fine sandy silt with dark grey laminations and bands of clayey silt 8.5-10.2: Dense yellow silty fine sand and fine to medium sub-angular gravel. 10.2-11.15: Firm pale grey silty fine sand with grey fine sandy silt. Some sandy laminations and occasional organic patches. 11.15-12.2: Firm grey laminated very silty fine sandy clay with occasional gravel patches.	12.2-15.0: Strong moderately weathered grey to greenish grey meta-siltstone with iron stained discontinuties. Numerous calcite veins.		

CIRC	DII IE	CL (P)	Don't ()	Made Council (c. 1. 1)		al Deposits	Bodon de (m. bol)	A 44'6'1 Ob ''	CDVE
GI Ref.	BH ID	GL (mD)	Depth (m)	Made Ground (m bgl)	Blown Sand (m bgl)	Alluvium / Head (m bgl)	Bedrock (m bgl)	Additionl Observations	SPT
Geotechnical Engineering Ltd fersey General Hospital Phase IB (12-14 July 1979)	вн3	10.0	13.5	GL-1.25: Sand with some gravel	1.25-3.0: Medium dense pale yellow grey fine sand 3.0-3.2: Loose white fine and medium sand 3.2-4.8: Loose brown to grey fine to medium sand with occasional silty patches	4.8-7.8: Fine blue grey mottled yellow laminated fine sadny silt with some iron staining. Occasional bands of yellow silty fine sand 7.8-9.0: Dense to medium dense grey beccoming brown silty sand with medium iron stained gravels 9.0-10.4: Firm orange brown silty fine sand becoming blue grey clayey sandy silt with black organic inclusions 10.4-10.8: Stiff blue grey laminated very silty clay with occasional gravel 10.8-11.0: Highly weathered rock fragments in a silty clay		Indiaction of pyrite bands within meta-silistone bedrock (11.0-13.5m bgl)	
Geomarine Ltd ersey General Hospital Main Theatres Upgrade 7-8 March 2014)	ВН1	13.0 ^{Note2}	12.7	GL-0.1: Tarmac surfacing 0.1-0.3: Backfill 0.3-0.5: Fill comprising bricks and concrete	0.5-0.8: Orange coarse sand 0.8-1.45: Orange brown gravelly silt 1.45-2.4: Grey white fine sand	2.4-2.8: Grey brown laminated sandy silt 2.8-3.25: Grey mottled brown silty sand 3.25-3.55: Green grey sandy silt 3.55-8.75: Green grey laminated silt 8.75-10.2: Grey silty cobbly gravel. Gravel is medium to coarse sub-rounded, cobbles are rounded. Gravel is of mixed lithologies becoming Jersey Shale with depth	10.2-12.7: Grey blue rock, recovered as medium to coarse angular gravel.		Blown Sand N = 6 Alluvium N = 9 to 22 Bedrock N = 47
	TP1	13.0 ^{Note2}	0.5	GL-0.1: Tarmac surfacing 0.1-0.25: Backfill 0.25-0.5: Concrete footing GL-0.1: Tarmac surfacing	Not encountered. Not encountered.	Not encountered. Not encountered.	Not encountered. Not encountered.		- -
				0.1-0.95: Backfill 0.95-1.2: Concrete footing					
				0.93-1.2. Colletete footing	OFF-SITE				
Amplus Ltd	BH1	9.9 ^{Note3}	10.1	GL-0.8: Loose soil and rubble fill		4.0-6.25: Soft light blue grey to dark brown	9.05-10.1: Dark grey slightly	1	Blown Sand
33 Gloucester Street Raleigh House (4-5 February 2000)					fine to coarse sand with rounded fine to medium gravel	occasionally organic silt 6.25-6.9: Firm to stiff light blue grey gravelly clayey silt 6.9-7.8: Medium dense brown and grey sandy fine to medium gravel 7.8-8.3: Soft to firm dark blue grey slightly sandy clayey silt 8.3-8.9: Soft to firm dark grey silty clay with rare gravel 8.9-9.05: Grey rock fragments in a grey clay matrix	weathered fine grained igneous moderately weak to moderatley strong very closely jointed sub- vertical discontinuties, iron staining on planar surfaces		N = 20 to 24 Alluvium N = 5 to 24
Amplus Ltd 15-16 The Parade 111 September 2006)	P1	9.7 ^{Note3}	10.5	GL-0.5: No description	0.5-3.0: Loose medium dense light brown sand	3.0-7.0: Soft to firm brown and grey sandy clay/silt 7.0-9.0: Firm to stiff brown gravelly clay 9.0-10.5: Firm to stiff brown and grey slightly sandy clay	Not encountered.		
	P2	9.6 ^{Note3}	9.9	GL-0.5: No description	0.5-3.0: Loose medium dense light brown sand	3.0-7.0: Soft to firm brown and grey sandy clay/silt 7.0-8.5: Firm to stiff brown gravelly clay 8.5-9.9: Firm to stiff brown and grey slightly sandy clay	Not encountered.		
	P3	9.7 ^{Note3}	9.7	GL-0.5: No description	0.5-3.0: Loose medium dense light brown sand	3.0-7.0: Soft to firm brown and grey sandy clay/silt 7.0-8.0: Firm to stiff brown gravelly clay 8.0-9.7: Firm to stiff brown and grey slightly sandy clay	Not encountered.		

GI Ref.	BH ID	CI (P)	Don't ()	Made Council (1 1)	Superfici	al Deposits	D - d d - (b -1)	Additionl Observations	SPT
	BH ID	GL (mD)	Depth (m)	Made Ground (m bgl)	Blown Sand (m bgl)	Alluvium / Head (m bgl)	Bedrock (m bgl)	Additioni Observations	SPI
Gloucester Street Surface Water Sewer Drawing Note 5 (12 January 1982)	ВН1	15.0 ^{Note4}	8.0	GL-0.9: Asphalt surfacing over sand and gravel sub-base	fine medium sand	2.9-4.0: Firm to stiff mottled pale brown and orange brown silghtly clayey silt with traces of roots 4.0-6.7: Soft to firm grey silt 6.7-7.8: Firm pale brown mottled orange brown very silty clay 7.8-8.0: Firm pale brown slightly clayey silt	Not encountered.		
	ВН2	14.4 ^{Note4}	7.5	GL-1.0: Asphalt surfacing over sand and gravel sub-base	medium sand	2.8-4.5: Soft pale brown becoming grey silt 4.5-5.9: Soft to firm grey very silty clay with zones of brown silt 5.9-6.1: Grey slightly sandy silt 6.1-6.3: Fine medium gravel 6.3-7.5: Medium dense grey silty fine medium sand with some medium gravel	Not encountered.		
	ВН3	13.0 ^{Note4}	8.0	GL-1.2: Asphalt surfacing over sand and crushed rock fill	some pale brown medium sand	3.4-5.8: Soft to firm grey silt 5.8-6.9: Firm grey silt with a little fine medium gravel 6.9-8.0: Firm black laminated brown silt with a slightly organic odour	Not encountered.		
	ВН4	13.2 ^{Note4}	9.0	GL-0.9: Asphalt surfacing over sand and gravel fill	sand and medium coarse gravel	4.3-6.5: Soft grey and brown silt 6.5-7.6: Medium dense medium fine gravel with a little coarse sand 7.6-8.6: Firm grey silt with some dark grey zones and organic odour 8.6-9.0: Firm dark grey silt	Not encountered.		
Patriotic Street MSCP (Records dated: 1983)	BHIR	8.4	13.4	GL-0.5: No description		2.6-4.9: Silt 4.9-6.2: Clayey Silt 6.2-7.5: Gravel 7.5-9.5: Clayey Silt 9.5-10.0: Silt 10.0-10.8: Clayey Silt	10.8-13.4: Amygdaloidal lava with basalt boulders 'Boulders with gravel in a clay matrix'		
	BH2	8.8	11.3	GL-0.6: No description		2.2-6.3: Silt 6.3-7.0: Gravelly Silt 7.0-8.8: Sand and Gravel 8.8-10.2: Clayey Silt	10.2-11.3: Siltstone 'Moderately strong grey fine Silstone'		
	ВН3	9.6	11.2	GL-1.8: No description	1.8-10.2: Mixture of clays silts sands and gravels Refer to Appendix O		10.2-11.2: Amygdalodial lava 'Thinly bedded amygdaloidal modertaly strong lava'		
	BH4	9.2	10.8	GL-0.4: No description	0.4-3.4: Silty Sand	3.4-7.3: Silt 7.3-8.2: Sandy Silty Clay 8.2-8.8: Silty Gravelly Sand 8.8-9.7: Clayey Silt	9.7-10.8: Siltstone Thinly bedded dark green moderately strong Siltstone'		
	BH5	8.8	11.1	GL-0.9: No description		ys silts sands and gravels	10.8-11.1: Siltstone 'Very thinly bedded dark green moderatly strong Siltstone'		
	ВН6	7.9	15.8	GL-1.1: No description	Refer to A	ys silts sands and gravels **Appendix O** very dense silty sand.	Not encountered.		
	ВН7	8.2	15.2	GL-1.2: No description	1.2-10.7: Mixture of cla	ys silts sands and gravels Appendix O	10.7-15.2: Amygdaloidal lava (Basalt) 'Closely jointed white veined dark grey fine basic volcanic (Basalt)'		

CLD 6	DIT ID	CI (D)	D 41()	M 1 C 1/ 1 D	Superfici	al Deposits	D 1 1/ 1 D	1124 101 4	CDVE
GI Ref.	BH ID	GL (mD)	Depth (m)	Made Ground (m bgl)	Blown Sand (m bgl)	Alluvium / Head (m bgl)	Bedrock (m bgl)	Additionl Observations	SPT
Amplus Ltd Kensington Gate Car Park (8-12 January 2007)	BH4300	-	10.3	GL-0.2: Concrete overlying hardcore fill	0.2-2.0: Very loose to loose brown fine to medium sand and occasional gravels.	2.0-3.0: Soft to firm brown sandy silt 3.0-6.3: Soft to firm blue grey slightly sandy clay/silt 6.3-7.8: Dense blue ffrey very clayey fine to coarse gravel 7.8-8.3: Very dense brown clayey sandy fine to medium gravel 8.3-9.1: Soft to firm brown sandy silt	iron staining		Blown Sand N = 4 Alluvium N = 5 to 52
	BH4301	-	10.5	GL-0.1: Concrete 0.1-1.0: Layers of concrete and sand 1.0-3.8: Concrete	Not encountered.	3.8-6.8: Very soft to firm grey brown slightly sandy clay with little fine gravel 6.8-9.2: Firm to stiff orange brown sandy clay with a little fine to medium gravel	9.2-10.5: Moderately weak grey slightly weathered andesite, very closely jointed		
	BH4302	-	11.0	GL-0.1: Concrete	0.1-1.5: Loose light brown to medium sand	1.5-7.0: Very soft red brown sandy silt becoming firm with depth 7.0-8.5: Dense grey and brown clayey very sandy fine to coarse gravel with occasional cobbles 8.5-9.6: Firm to stiff brown sandy silt with occasional grey fine to medium gravel	9.6-11.0: Moderately strong light grey slightly weathered andesite with iron staining		
Geomarine Ltd Kensington Place (16-21 July 2009)	BH4303	-	6.8	GL-0.55: Brown very gravelly fine to medium grained sand. Slight hydrocarbon smell 0.55-1.0: Brown soily gravelly fine to medium grained sand with layers of pale brown white sand 1.0-1.4: Light brown gravelly fine to medium garined sand. Coatse cobbles present	Not encountered. Made ground believed to be reworked blown sand material, see made ground strata.	1.4-2.9: Grey sand clay. Strong hydrocarbon smell with coarse gravel. (Head Deposits) 2.9-4.4: Grey clay. Strong hydrocarbon smell. (Head Deposits) 4.4-5.9: Grey slightly sandy clay with rare gravel fragments. Hydrocarbon smell. (Head Deposits) 5.9-6.8: Tan slightly sandy gravelly clay. Gravel is fine to coarse. (Head Deposits)	Not encountered.	Evidence of hydrocarbon contamination. (1.4-6.8m bgl)	
	BH4304	-	6.8	GL-1.4: Dark brown very gravelly clayey fine grained sand. Frequent cobbles. Brick fragments and rootlets present	Not encountered. Made ground believed to be reworked blown sand material, see made ground strata.	1.4-2.9: Grey slightly gravelly clay. Hydrocarbon odours. (Head Deposits) 2.9-6.8: Yellow tan slightly gravelly clay. Slight hydorcarbon staining. (Head Deposits)	Not encountered.	Evidence of hydrocarbon contamination. (1.4-6.8m bgl)	
	BH4305	-	7.3	GL-0.9: Brown very gravelly fine to medium grained sand. Gravel is fine to coarse. Containing tile fragments, granite and cobbles	Not encountered. Made ground believed to be reworked blown sand material, see made ground strata.	0.9-1.4: Brown very gravelly fine to medium clayey sand. Gravel is sub-angular fine to coarse. (Head Deposits / Blown Sand?) 1.4-2.8: Tan slightly sandy clay. Contains tiny calcarous shells and fine gravel. (Head Deposits) 2.8-6.45: Tan grey clay with occasionla fine gravel. (Head Deposits) 6.45-7.3: Red brown very gravelly fine to medium garined sand. Gravel is fine to coarse. (Head Deposits)	Not encountered.		
	BH4306	-	6.4	GL-0.8: Brown soily very gravelly medium grained sand. Occasional rootlets and cobbles. 0.8-1.4: Brown very gravelly fine to medium grained sand, with evidence of concrete powder observed.	Not encountered. Made ground believed to be reworked blown sand material, see made ground strata.	1.4-2.9: Tan sandy clay. Hydrocarbon smell. (Head Deposits) 2.9-4.4: Brown grey slightly sandy clay. Rare coarse gravel. Strong hydrocarbon smell and dark grey lines running through. (Head Deposits) 4.4-5.9: Brown grey clay. Rare fine gravel and olfactory evidence of hydrocarbon contamination. (Head Deposits) 5.9-6.4: Brown gravelly clay. Gravel is fine to medium. (Head Deposits)	Not encountered.	Evidence of hydrocarbon contamination. (1.4-5.9m bgl)	

CLP 6	DIT ID	GI (D)	D (1 ()	W 1 C 1/ 1 D	Superfici	al Deposits	D 1 1 (1 D	1 1 1 C	SPT
GI Ref.	BH ID	GL (mD)	Depth (m)	Made Ground (m bgl)	Blown Sand (m bgl)	Alluvium / Head (m bgl)	Bedrock (m bgl)	Additionl Observations	3F 1
Geomarine Ltd Kensington Place (16-21 July 2009)	ВН4307	-	8.4	GL-1.4: Dark brown gravelly clayey fine grained sand. Gravel is fine to ocarse. Cobbles and brick fragments present	Not encountered. Made ground believed to be reworked blown sand material, see made ground strata.	1.4-2.9: Dark brown gravelly clayey fine grained sand. Gravel is fine to coarse. (Head Deposits) 2.9-3.1: Dark brown clayey fine gained sand. (Head Deposits) 3.1-4.6: Grey slightly gravelly clay. Faint hydrocarbon smell. (Head Deposits) 4.6-6.9: Grey brown slightly gravelly clay. (Head Deposits) 6.9-7.5: Brown grey very gravelly fine to medium grained sand. Faint hydrocarbon smell. (Head Deposits) 7.5-8.4: Grey brown slightly gravelly clay. Rare cobbles. Hydrocarbon smell. (Head Deposits)		Evidence of hydrocarbon contamination. (3.1-4.6m bgl) (6.9-8.4m bgl)	
Amplus Ltd 66-72 Esplanade (21 March - 2 April 2014)	BH4802	-	7.0	GL-0.6: Concrete overlying silty sand and gravel	0.6-2.0: Silty brown clay with fine to medium gravel and light yellow sand 2.0-3.0: Light brown silty sand with fine to medium gravel 3.0-4.0: Light brown silty sand	4.0-5.0: Brown sandy silt 5.0-6.0: Yellow brown sandy silt 6.0-7.0: Light brown silty sandy clay with fine to medium gravels	Not encountered.		Blown Sand N = 34 Alluvium N = 2 to 68
	BH4803	-	11.6	GL-0.25: Concrete overlying gravel	0.25-1.2: Clayey gravelly sand with cobble sized stones 1.2-1.9: Loose yellow and brown sand with fine gravel 1.9-3.0: Loose brown fine sand	3.0-4.6: Very soft brown sandy silt 4.6-5.3: Soft brown and grey sandy silt 5.3-6.0: Soft brown sandy clay 6.0-7.8: Medium dense brown fine slightly clayey slightly sandy gravel 7.8-9.4: Firm brown sandy silty clay with little firm to medium gravel 9.4-10.2: Stiff grey sandy clay 10.2-10.5: Stiff grey clay with fragments of rock	10.5-11.6: Weak grey slightly weathered Jersey Shale Formation with iron stained close bedding		
	BH4804	-	7.5	GL-0.7; Concrete overlying dark grey gravelly silt with metal inclusions	0.7-0.9: Light grey silty clay 0.9-1.2: Light yellow sand 1.2-2.0: Stiff brown sandy clay with fine to medium gravels 2.0-3.45: Dense light brown sand with fien to medium gravels	3.45-4.0: Firm brown and grey sandy silt 4.0-5.0: Soft brown sandy clayey silt 5.0-6.0: Firm brown sandy silt 6.0-7.5: Medium dense to dense brown clayey sandy fine to coarse gravel	Not encountered.		
	BH4805	-	11.7	GL-0.4: Concrete overlying gravelly silt	0.8-2.4: Dense light yellow brown to off whit fine to medium silty sand	0.4-0.8: Dark brown peaty silt overlying brown silty clay 2.4-3.25: Dense off white grey brown slightly silty sandy gravel 3.25-5.9: Firm brown sandy silt with a little fine to medium gravel 5.9-7.6: Medium dense brown clayey slightly sandy gravel 7.6-10.2: Stiff grey sandy clay with fine gravels 10.2-10.5: Stiff brown clay with fine gravels			

Note 1 - Data in records regarding depths and elevations presented in imperial units so subject to online conversion tools to gather indicative metric values.

Note 2 - Elevations provided from Geomarine records are arbitrary levels.

Note 3 – Elevation data for BH unavailable in records. Indicative elevation gained from GPS GeoPlaner website [16].

 $[\]it Note~4$ – Indicative elevations provided from Gloucester Street surface water outfall drawing in Appendix N.

Note 5 - Ground conditions information gathered from States of Jersey Resources Board Gloucester Street surface water outfall drawing and accompanying note states 'The information above is the best available, however its accuracy cannot be guaranteed'.

Figures

Figures

Figure 1 Site Location Plan

Figure 2 Site Plan

Figure 3 Indicative Proposals

Figure 4 Jersey General Hospital Site Walkover Photos

Figure 5 Westaway Court Site Walkover Photos

Figure 6 Jersey General Hospital Existing Basement Extents

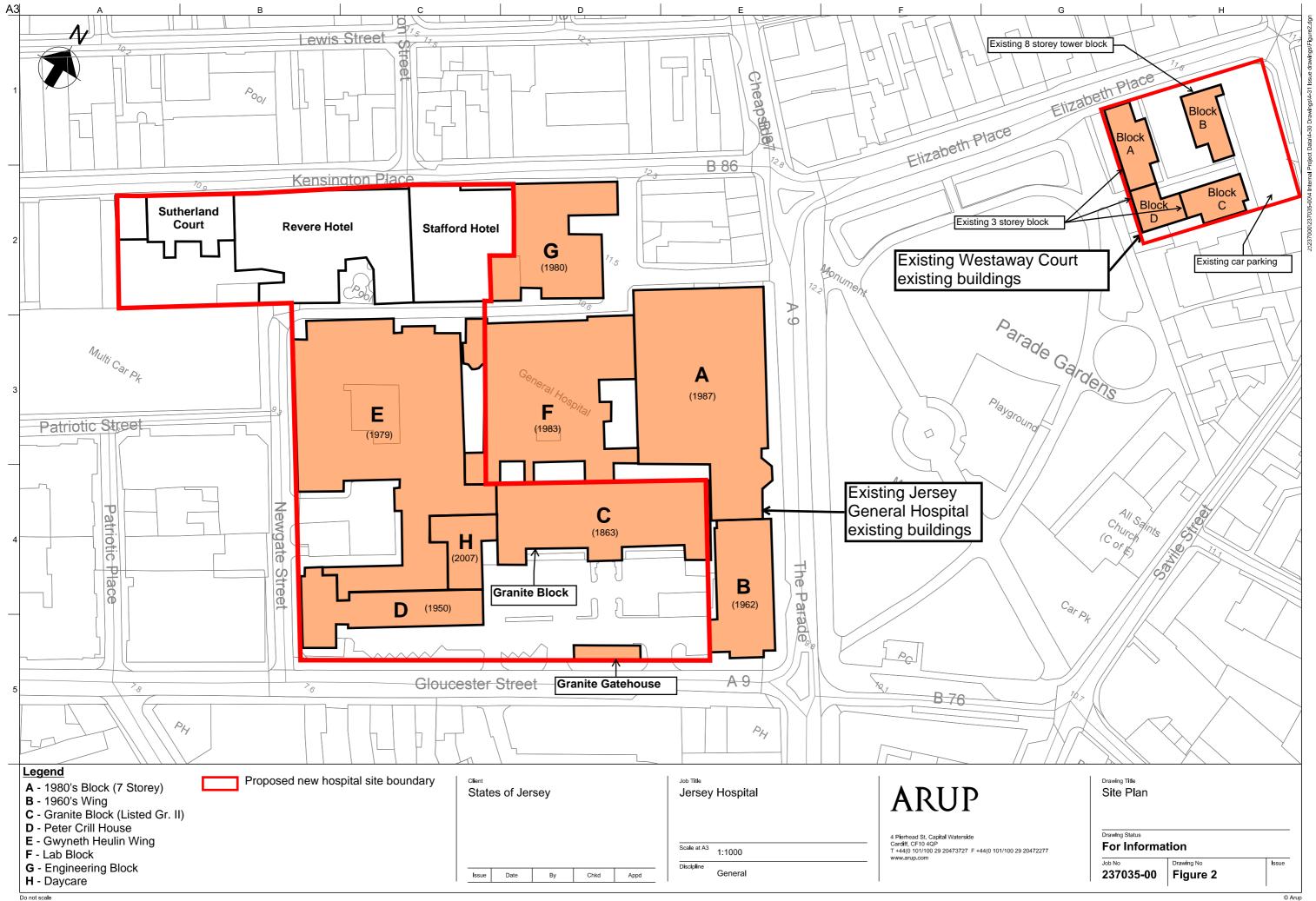
Figure 7 Geological Map Extract

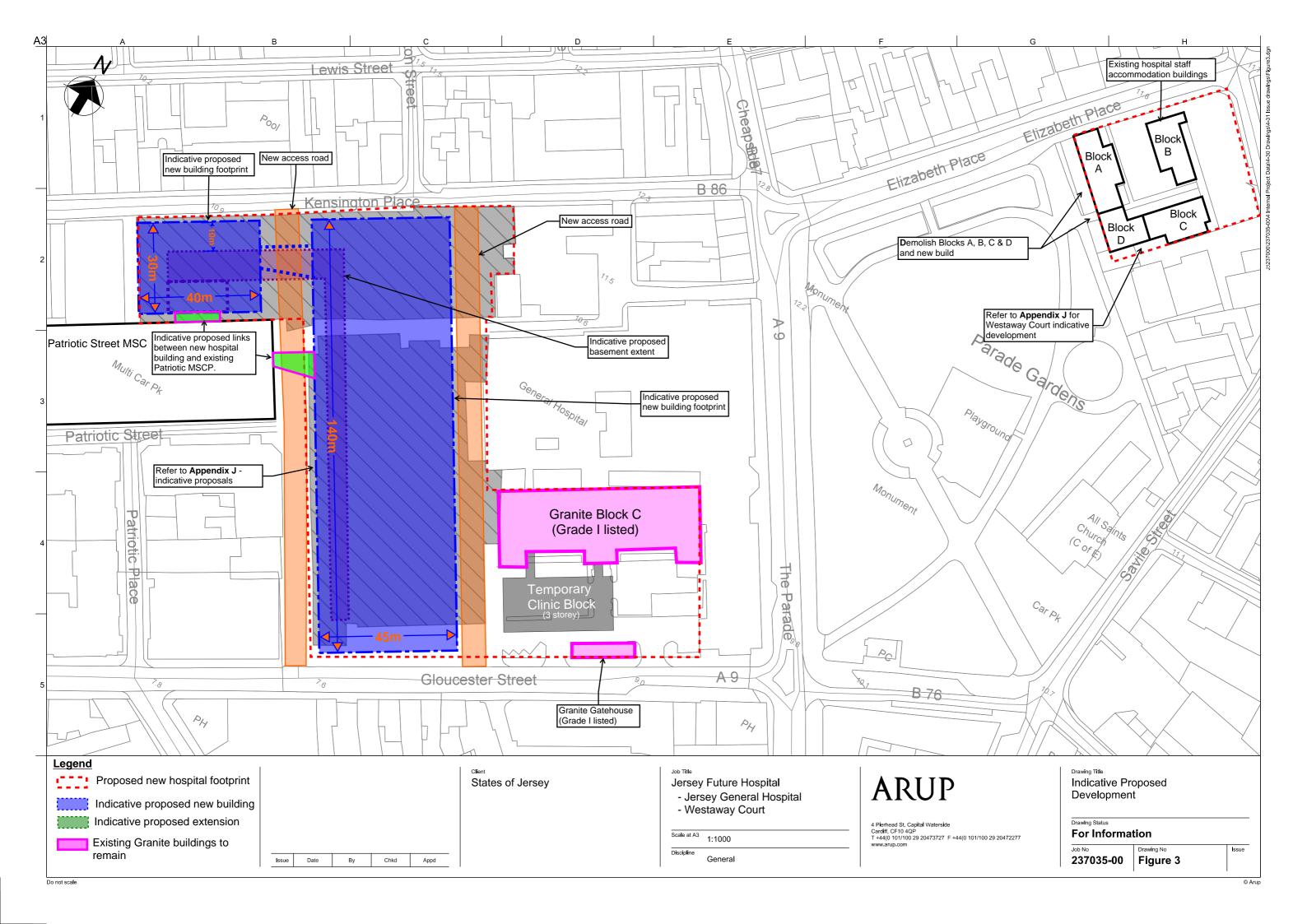
Figure 8 Historical Ground Investigation Locations

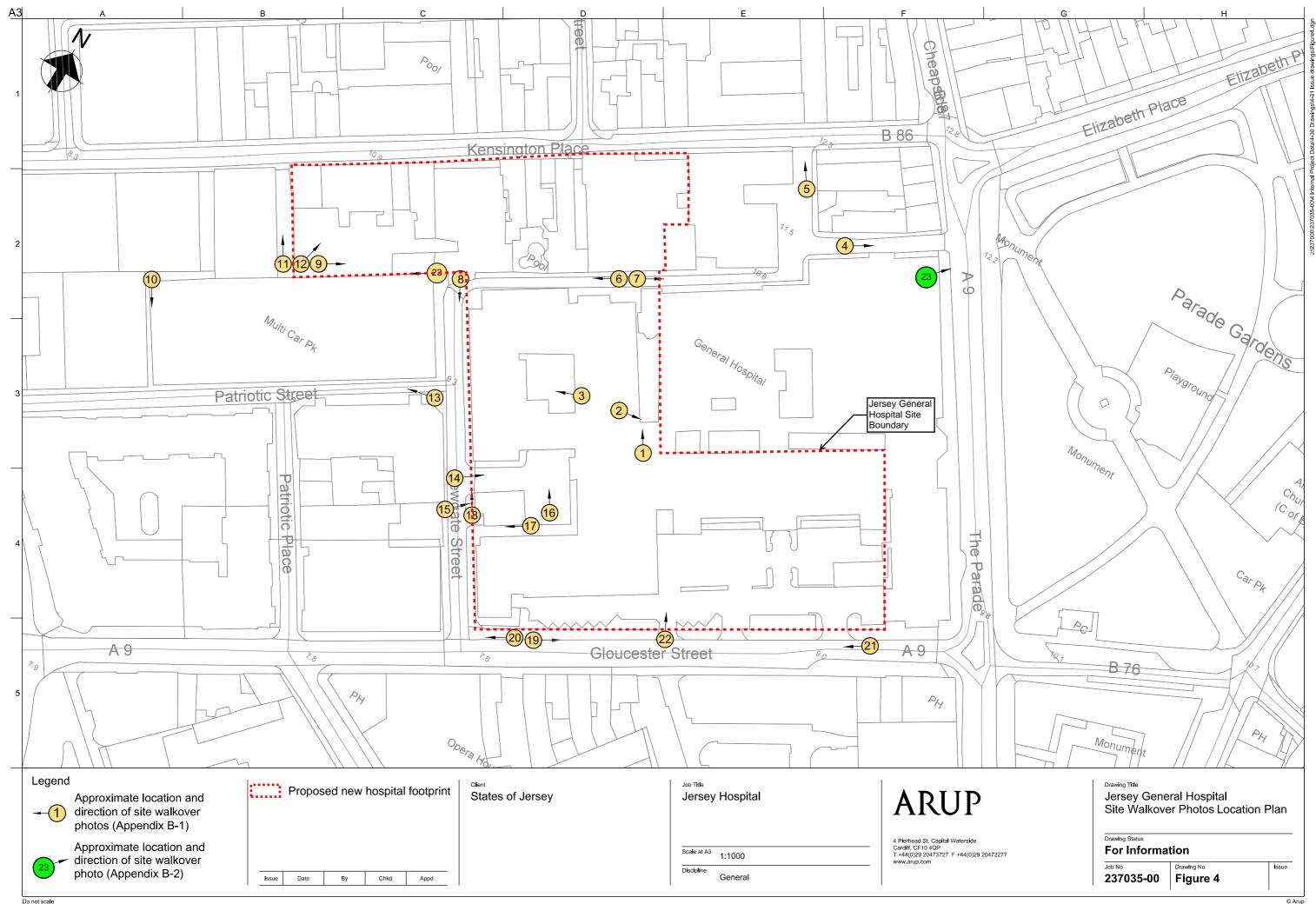
Figure 9 Hydrogeological Map Extract

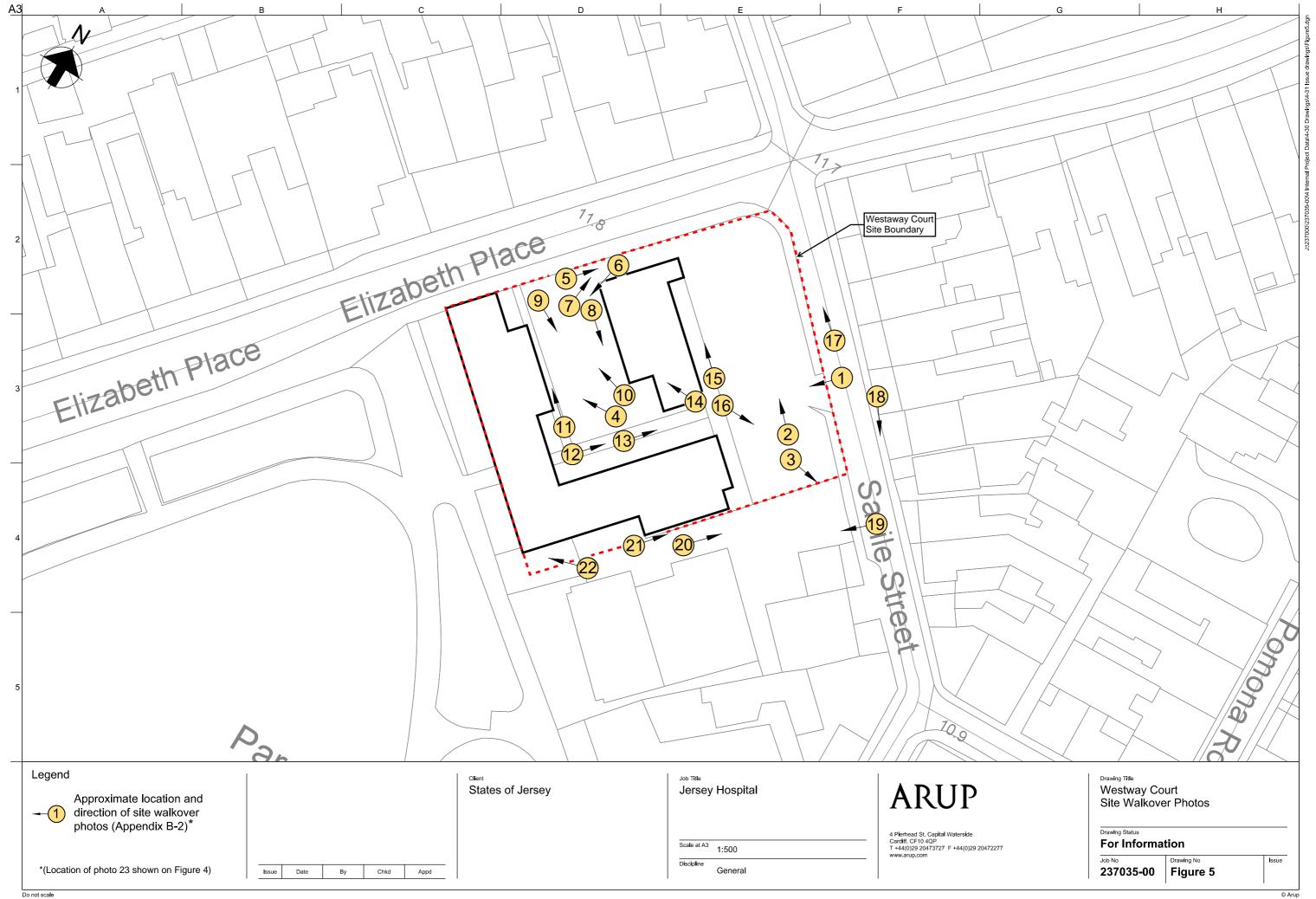
Figure 10 Surface water and Culvert Plan

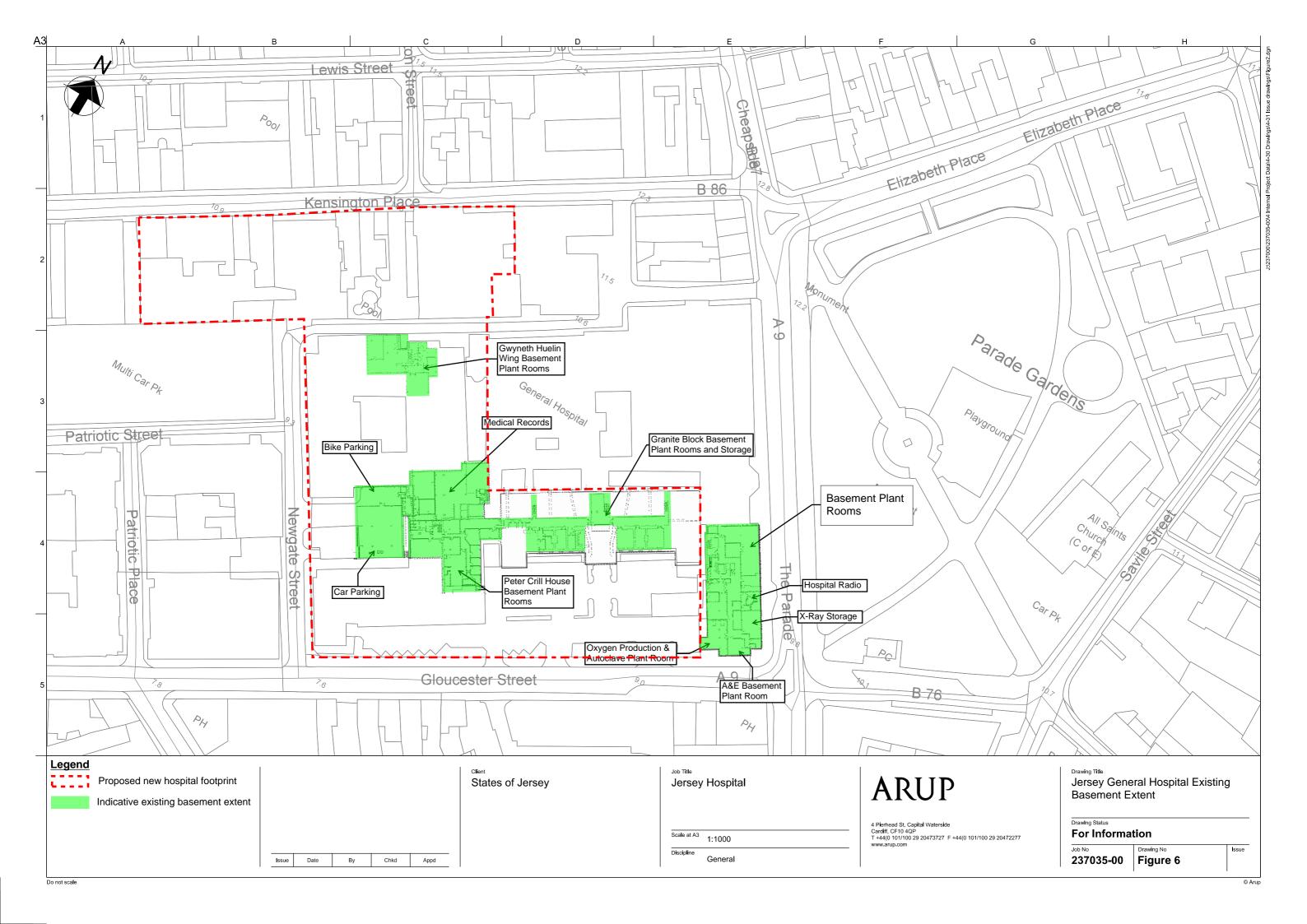
Figure 11 Features & Constraints

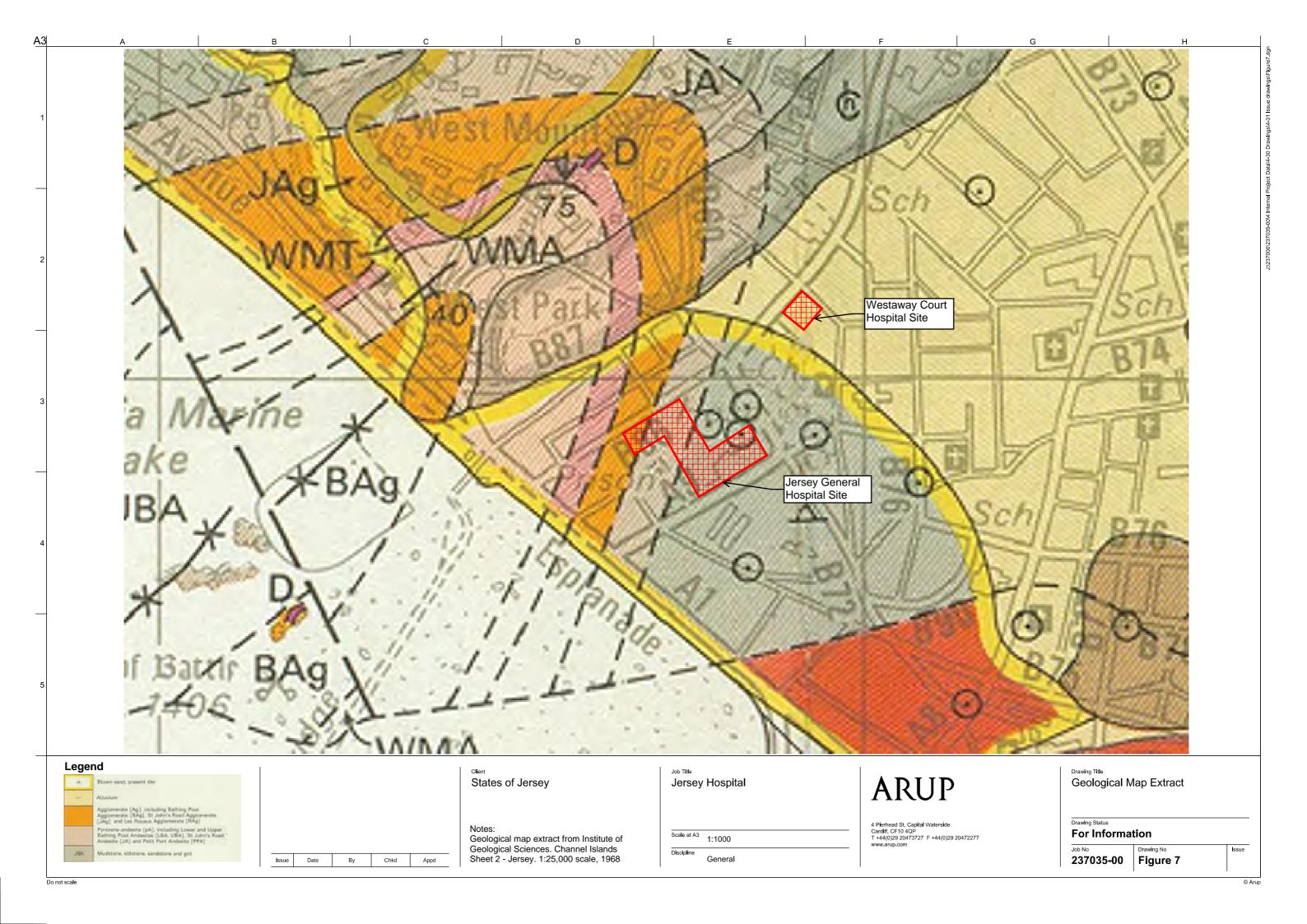


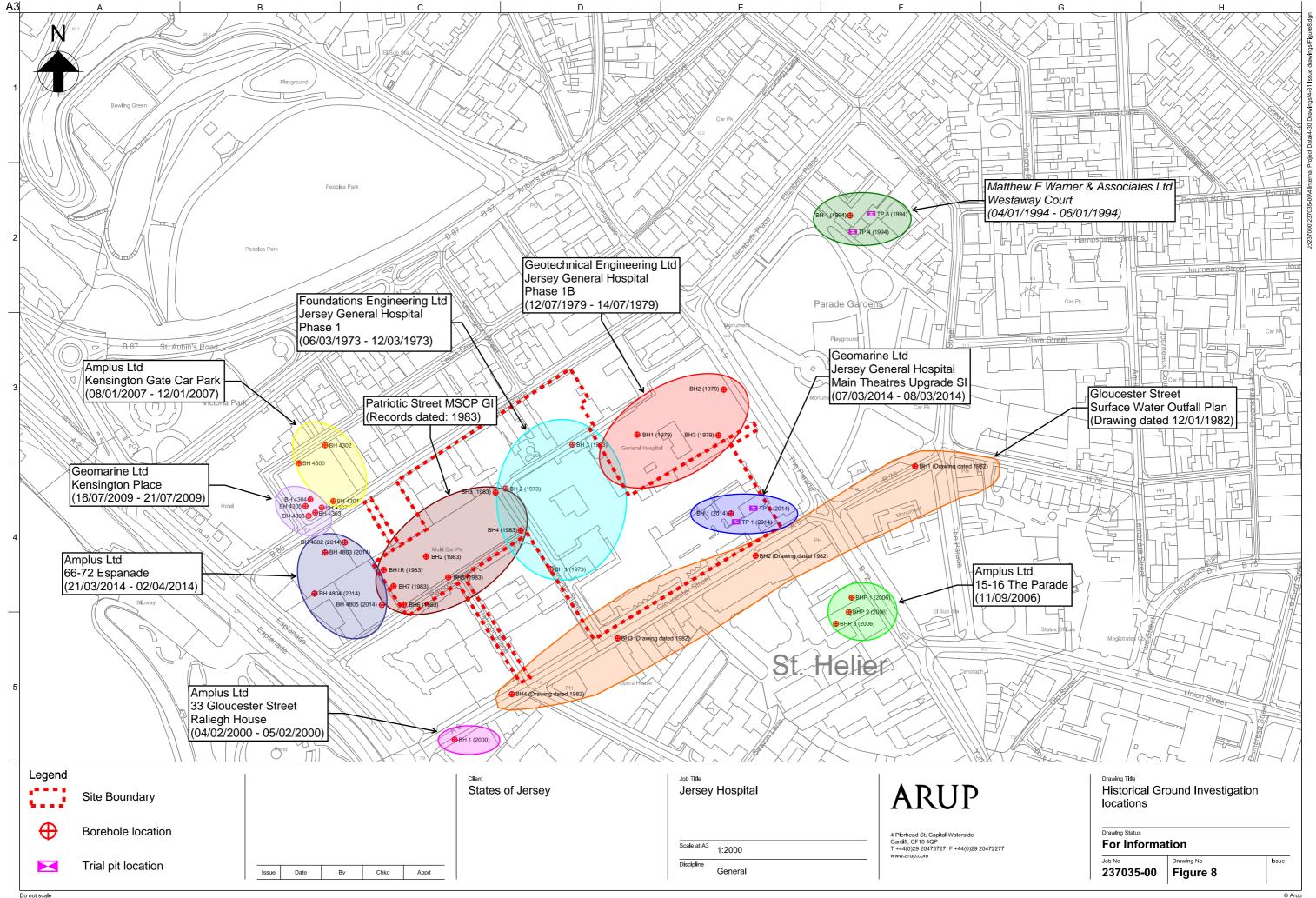


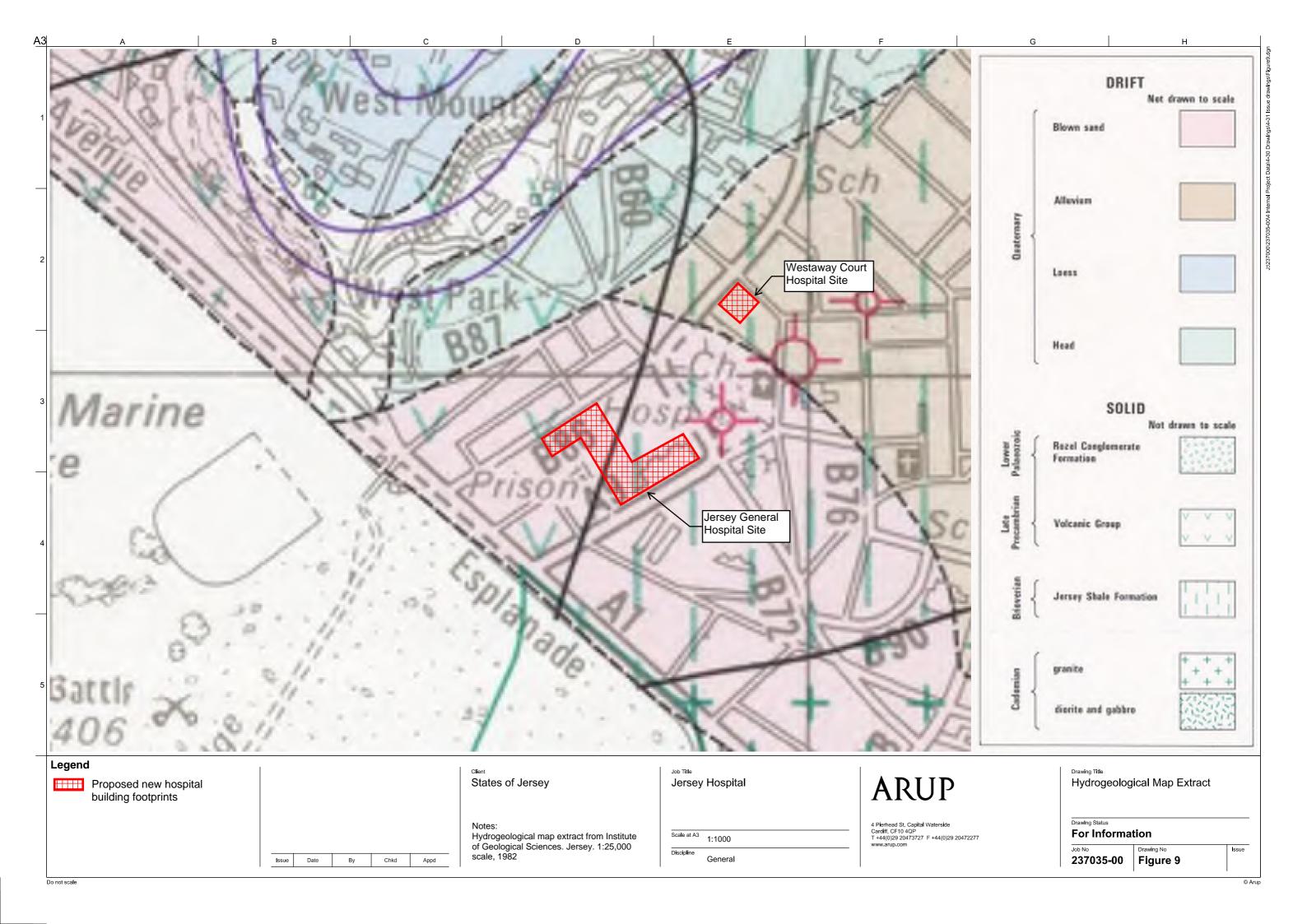


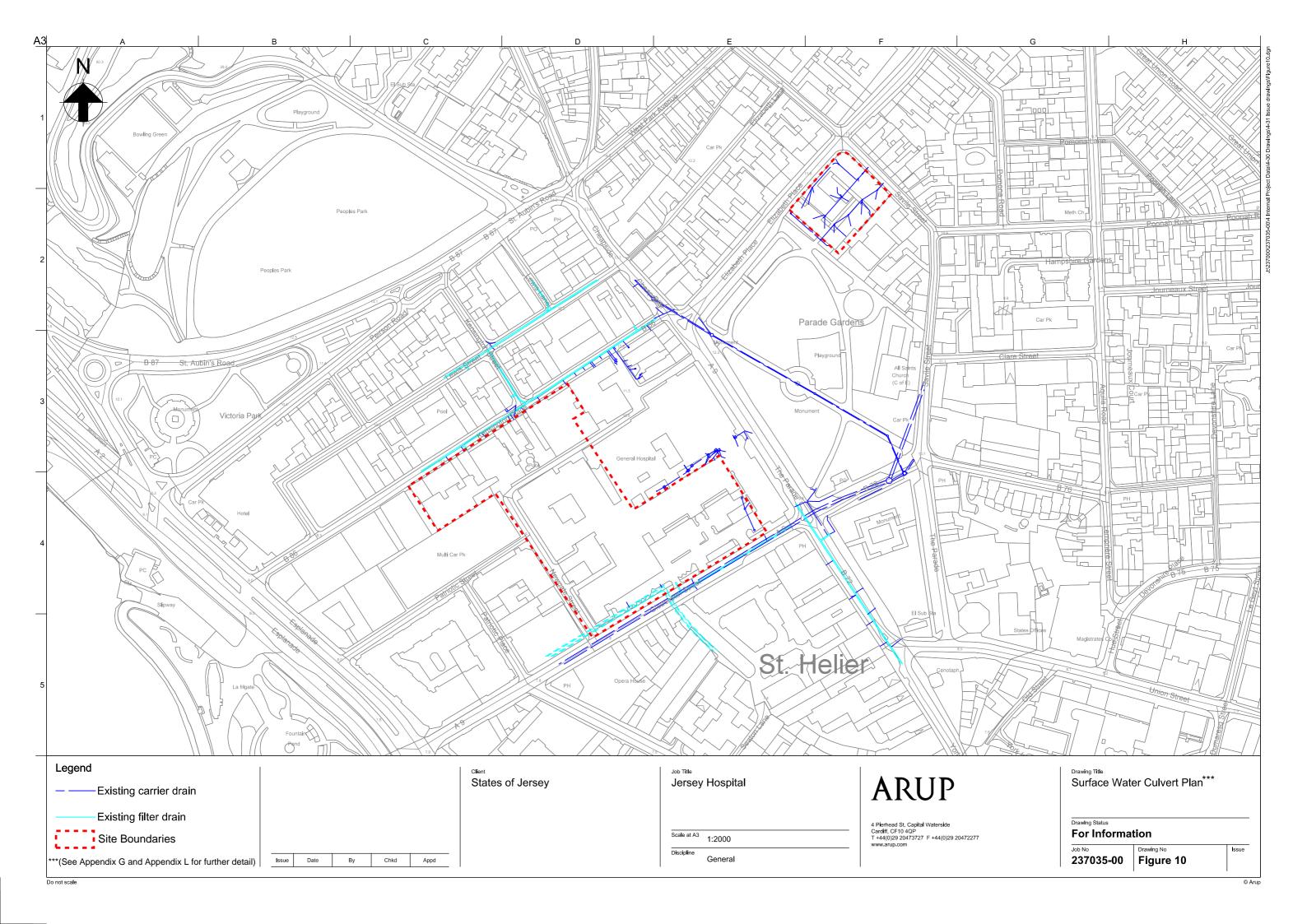


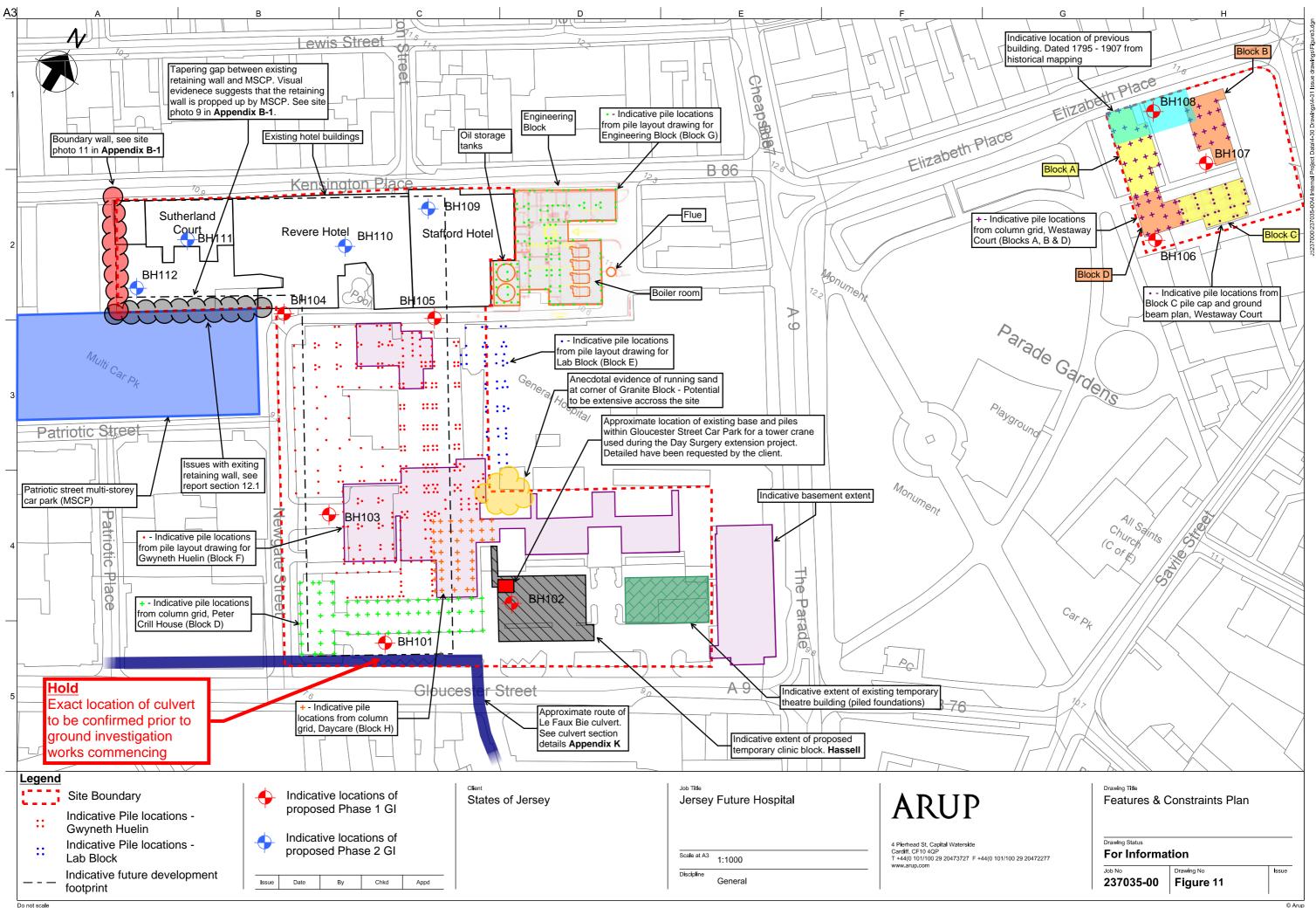












Appendix A

Key Supporting Documents

A1 Key Supporting Documents

Doc	Drawing Reference Details	Drawing	Source (Provided by)	Existing
Ref.		Date		Block
E1-1	Jersey General Hospital Daycare Extension, Proposed Basement Structural General Arrangement, Revision C1	03/04/2007	Rothwell & Partners Ltd	H - Daycare
E1-2	Jersey General Hospital Daycare Extension, Proposed Ground Floor Structural General Arrangement, Revision C1	03/04/2007	Rothwell & Partners Ltd	H - Daycare
E1-3	Jersey General Hospital Daycare Extension, Proposed Ground Floor Structural General Arrangement Sheet 2 –	03/04/2007	Rothwell & Partners Ltd	H - Daycare
	Theatre Corridor, Revision C3			
E1-4	Department of Public Building and Works States Offices, General Hospital Phase 1, General Arrangement Pile	04/06/1976	Edwards & Blackie	E – Gwyneth
	Caps Sheet 2, Revision D			Huelin Block
E1-5	Department of Public Building and Works States Offices, General Hospital, Jersey Phase One Redevelopment,	26/02/1975	Edwards & Blackie	E – Gwyneth
	Pile Layout Sheet 1			Huelin Block
E1-6	Department of Public Building and Works States Offices, General Hospital, Jersey Phase One Redevelopment,	28/04/1976	Edwards & Blcakie	E – Gwyneth
	Pile Layout Sheet 2 – Revision D			Huelin Block
E1-7	Culvert Details, 6-14 Gloucester Street, St Helier, Jersey, Rothwell & Partners Ltd	Feb 2006	Rothwell & Partners Ltd	-
E1-8	Pile Layout, Jersey General Hospital, Phase 1B, Ove Arup & Partners – Revision A	May 1980	-	F – Lab Block
E1-9	Existing Basement Plan, Jersey General Hospital, Health & Social Services, Jersey Property Holdings Design &	Aug 2016	States of Jersey	JGH
	Building Services, Drawing 001			
E1-10	Existing ground Floor Plan, Jersey General Hospital, Health & Social Services, Jersey Property Holdings Design	Aug 2016	States of Jersey	JGH
	& Building Services, Drawing 002			
E2-1	Proposed Link (Block D), Westaway Court, Ove Arup & Partners, Sheet 1	Feb 1993	-	Westaway
E2-2	Layout plans of pile setting out, Pile caps and ground beams, Medical staff accommodation Block C Phase 2, Muir	Mar 1974	Rothwell & Partners Ltd	Westaway
	Wilson Associates,			

Note: All available construction drawings located within **Appendix E**.

Appendix B

Site Walkover Photos

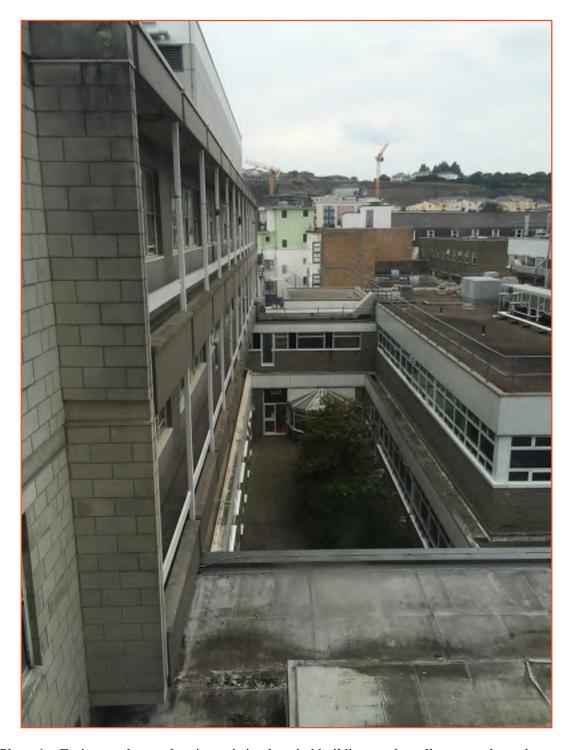


Photo 1- Facing northwest showing existing hospital buildings and small courtyard area between Blocks E and F. View along approximate demolition line.



Photo 2 – View facing east looking at junction between Block C (Granite Block) and Block E.



Photo 3 – View facing west looking at existing extent of multi-storey car park.



Photo 4 – Facing northeast showing exit on to The Parade along the north-western edge of Block A.



Photo 5 – Looking northwest from an internal car park between Block A, Block F and Block G. Exits out on to Kensington Place.



Photo 6 – Facing southwest along alley behind Blocks E and F.



Photo 7 – Facing northeast along alley behind Blocks E and F.



Photo 8 – View looking southeast along Newgate Street showing multi-storey car park entrance.

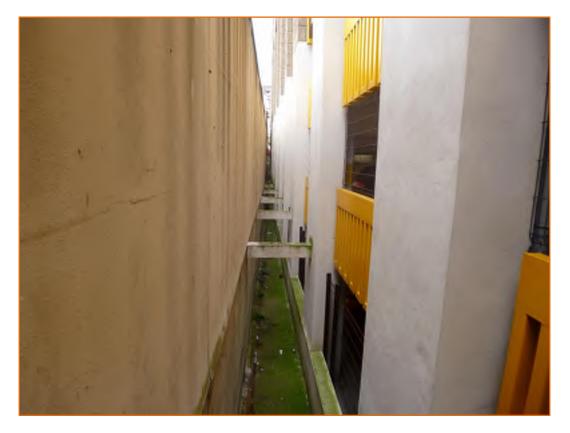


Photo 9 – View facing northeast showing props in tapering gap between Sutherland Court car park retaining wall and multi-storey car park.

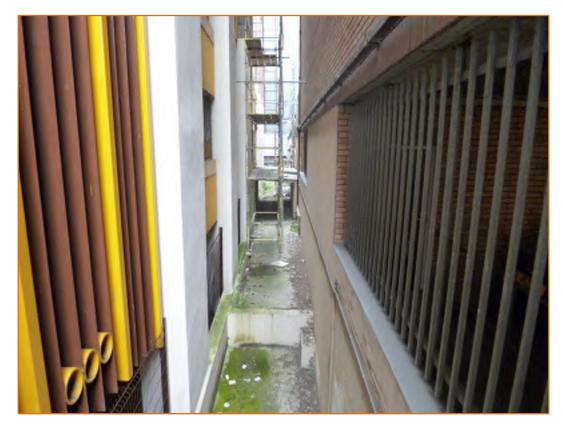


Photo 10- Image showing gap between south-western edge of multi-storey car park and adjacent building.



Photo 11 – View from multi storey car park showing Sutherland Court car park and south-western boundary of site along exiting wall.

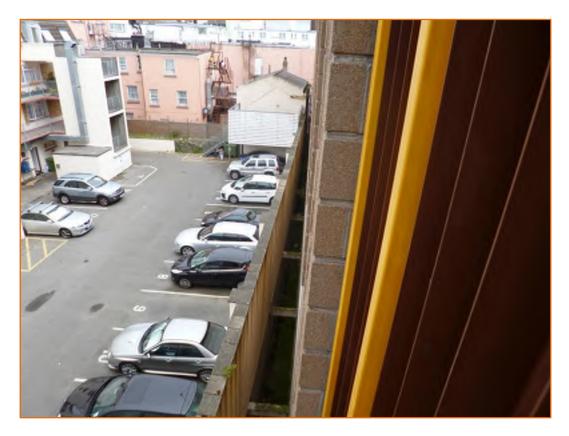


Photo 12 – View from multi-storey car park looking northeast showing Sutherland Court car park and tapering gap as mentioned in Photo 38.



Photo 13 – Facing southwest along Patriotic Street towards sea-front.



Photo 14 – Looking towards entrance to Gwyneth Huelin Wing (Block E) from Newgate Street.

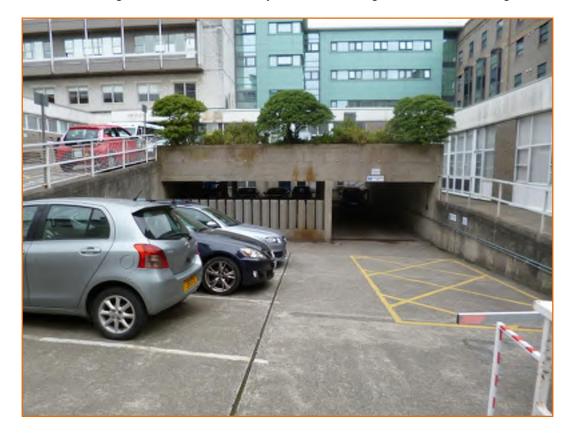


Photo 15 – View into underground car park between Block E (ahead and left) and Block D (right).



Photo 16 – Image showing extent of underground car park mentioned in Photo 44.

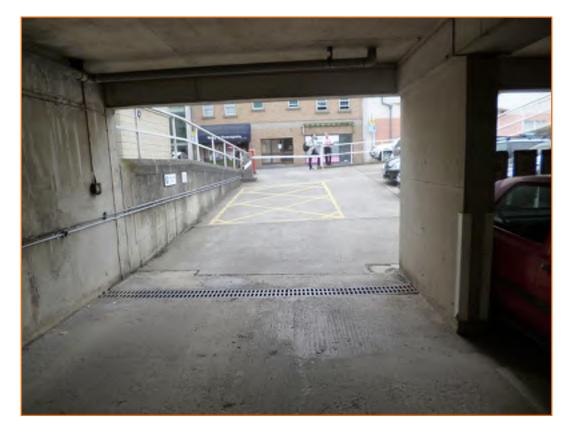


Photo 17 – View out of underground car park mentioned in Photo 44.



Photo 18 – Showing drain access in car park by Block E.



Photo 19 – Facing northeast along Gloucester Street, Block D upper left.



Photo 20 – Facing southwest along Gloucester Street towards sea-front.



Photo 21 – View facing southwest along Gloucester Street towards seafront.



Photo 22 – Showing exit of hospital car park by Granite block. Block C right, Block H centre (glass) and Block D left.



Photo 23 – Showing props between retaining wall and MSCP and unidentified underground structure (highlighted in red) as part of building forming the retaining wall.



Photo 1 – Looking southwest into entrance for Westaway Court main car park from Savile Street.



Photo 2 – Facing northwest looking at Westaway Court main car park adjacent to Savile Street.



Photo 3 – Facing southeast looking at Westaway Court main car park, showing exit on to Savile Street.



Photo 4 – Facing west looking at western end of Block A, location of proposed development.



Photo 5 – Facing northeast looking along the access road into the internal car park.

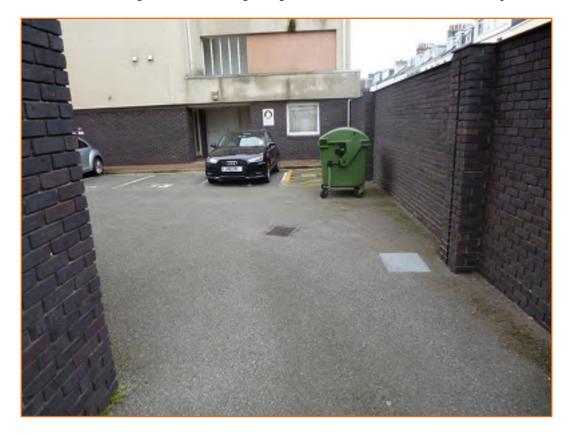


Photo 6 – Facing southwest looking into the internal car park from the access road down the side of the tower block.

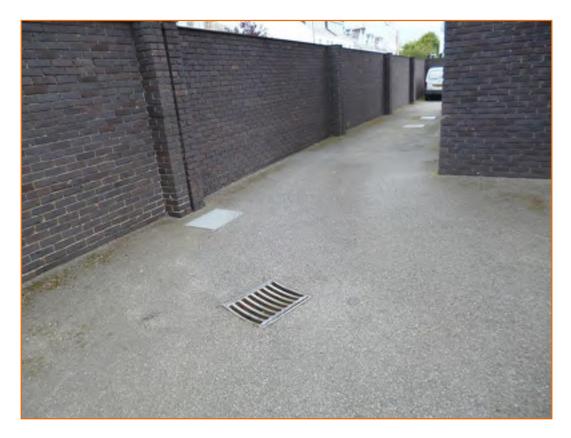


Photo 7 – Facing north showing free standing wall site boundary and vehicle exit of internal car park down access road.



Photo 8 – Facing southeast looking into internal car park/courtyard and Block C.



Photo 9 – Facing east looking at internal car park with Block B on the left and Block C ahead.



Photo 10 – Facing west in internal car park/courtyard, proposed development between the two buildings on first or second floor.



Photo 11 – Facing northwest along Block A building external wall, showing car park drainage.



Photo 12 – Facing northeast in internal car park towards pedestrian exit into main car park.



Photo 13 – Facing northeast towards pedestrian exit of courtyard area.



Photo 14 – Looking at internal car park drainage by pedestrian exit to main car park.

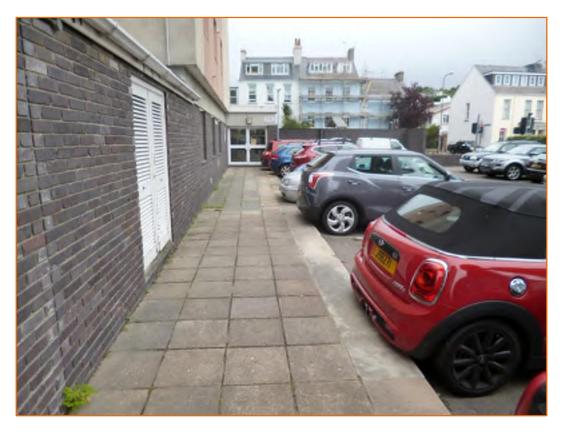


Photo 15 – Facing northwest in main car park towards tower block entrance hall.



Photo 16 – Looking at ramp up on to raised paved area for building access.



Photo 17 – Facing northwest looking along Savile Street towards crossroads at northern point of site.



Photo 18 – Facing southeast along Savile Street.



Photo 19 - Facing southwest into SoJ Health & Social Services Department - Maison Le Pape.



Photo 20 – Facing northeast looking out of SoJ Health Department car park, south-eastern edge of Block C on left.



Photo 21 – Facing northeast showing additional parking along south-eastern edge of Block C.



Photo 22 – Showing drains and additional parking along south-eastern edge of Block C.

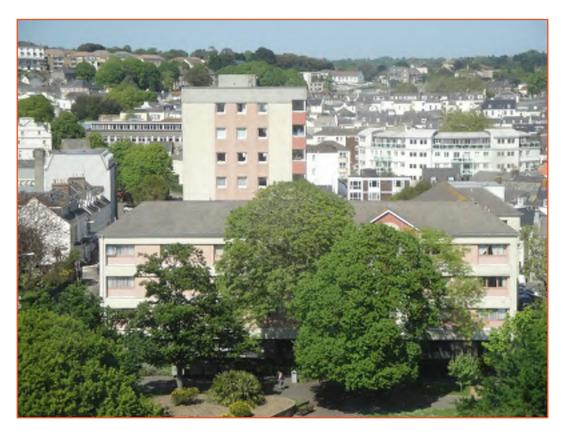


Photo 23 – Westaway Court existing buildings as viewed from Jersey General Hospital Block A facing northeast (not marked on **Figure 5**).

Date taken: 24/05/2016



Photo 1



Photo 2

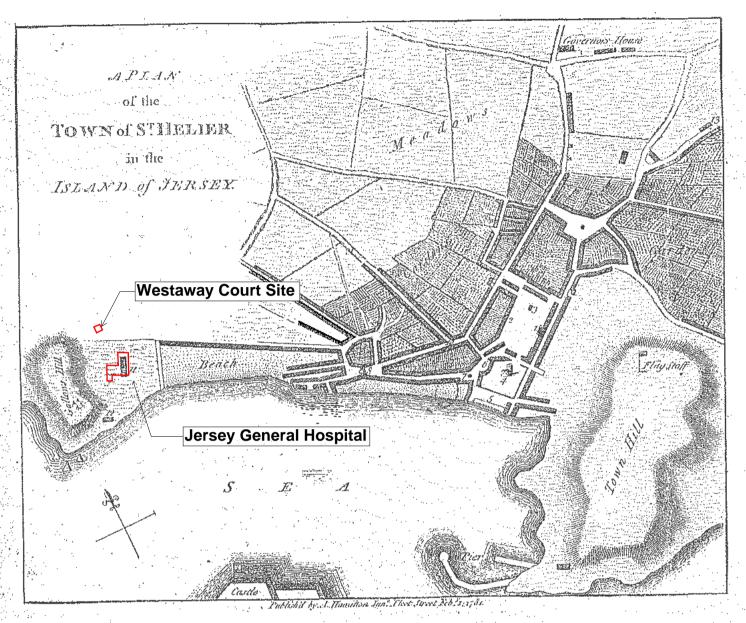


Appendix F-1

Geotechnical Desk Study - Part 2

Appendix C

Historical Plans & Aerial Photos



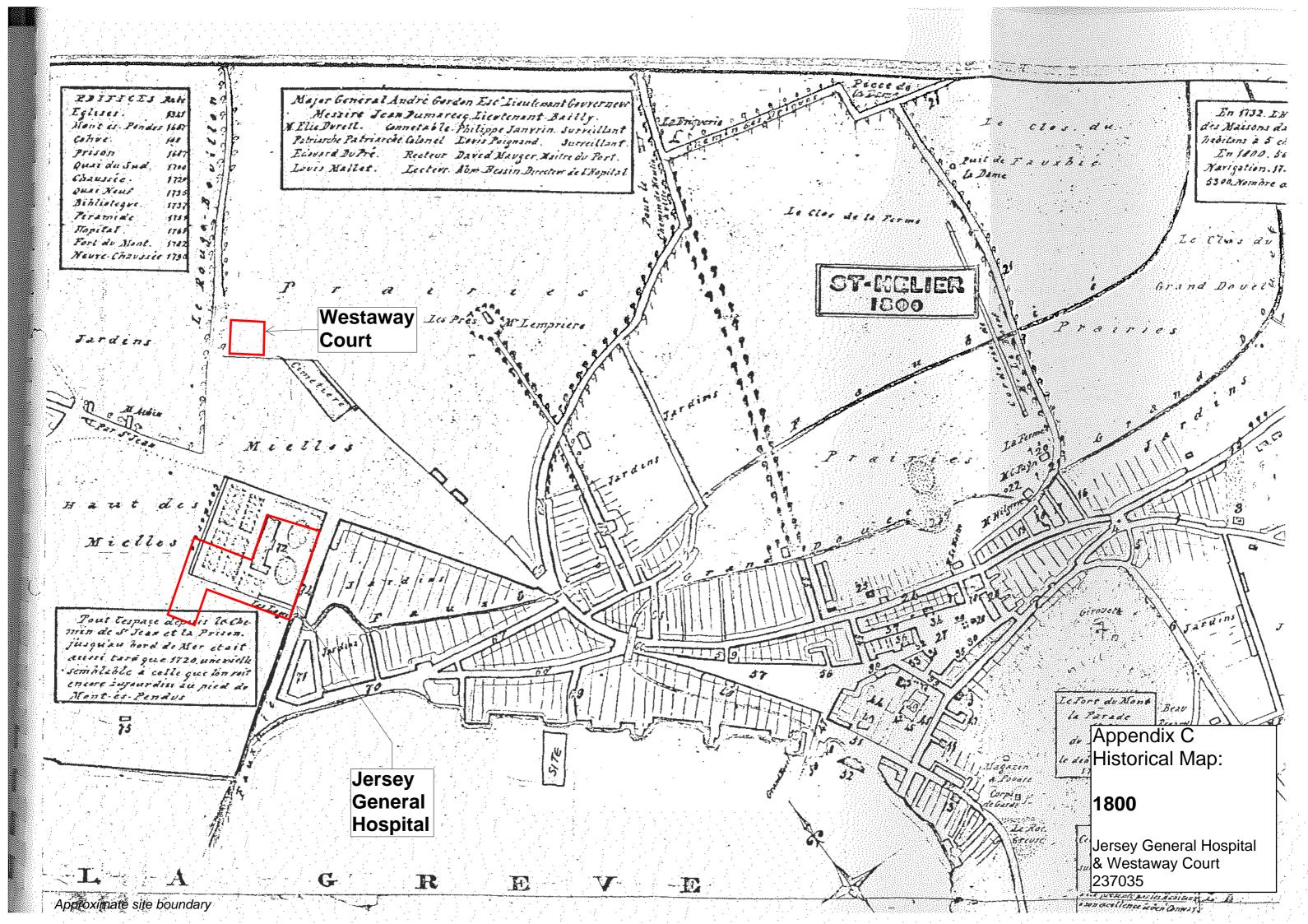
Approximate site boundary

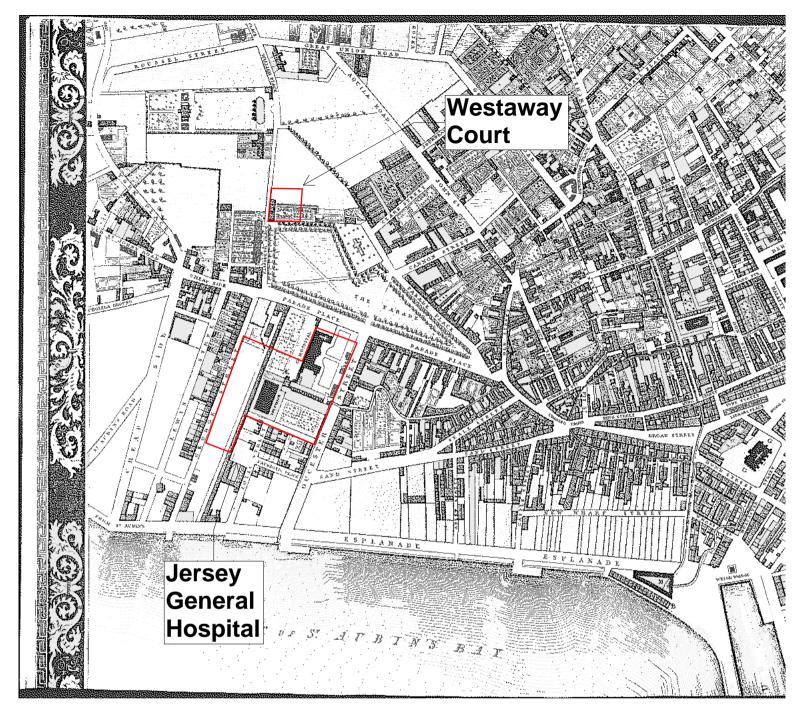
Appendix C Historical Map:

1781

Jersey General Hospital & Westaway Court 237035





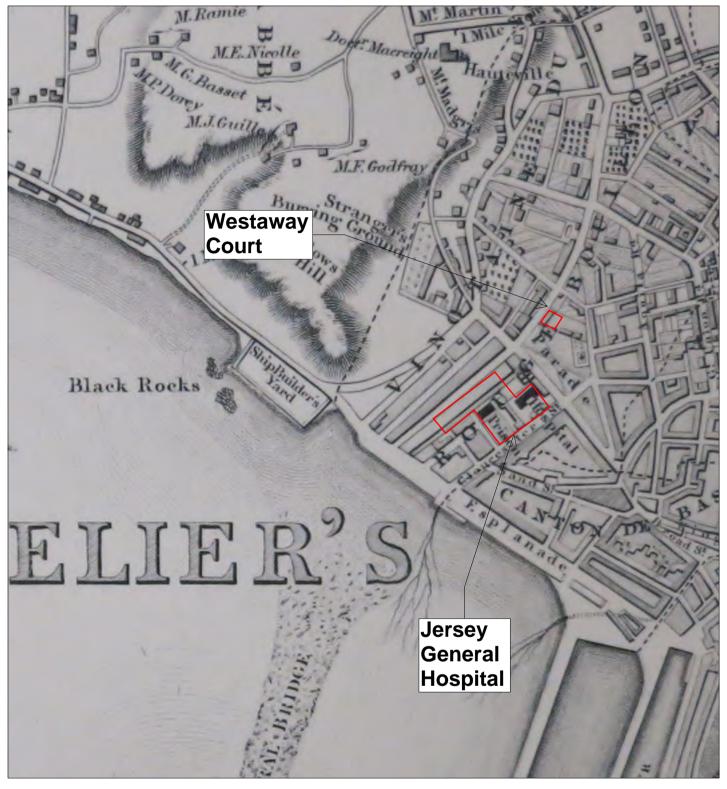


Approximate site boundary

Appendix C Historical Map:

1834

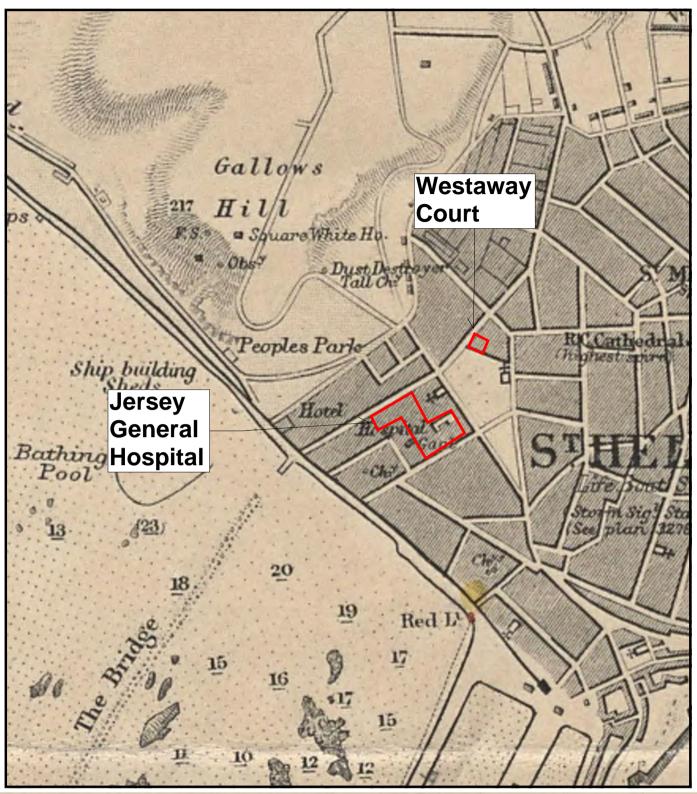
Jersey General Hospital & Westaway Court 237035



Approximate site boundary

Appendix C Historical Map:

1849 Godfray Map

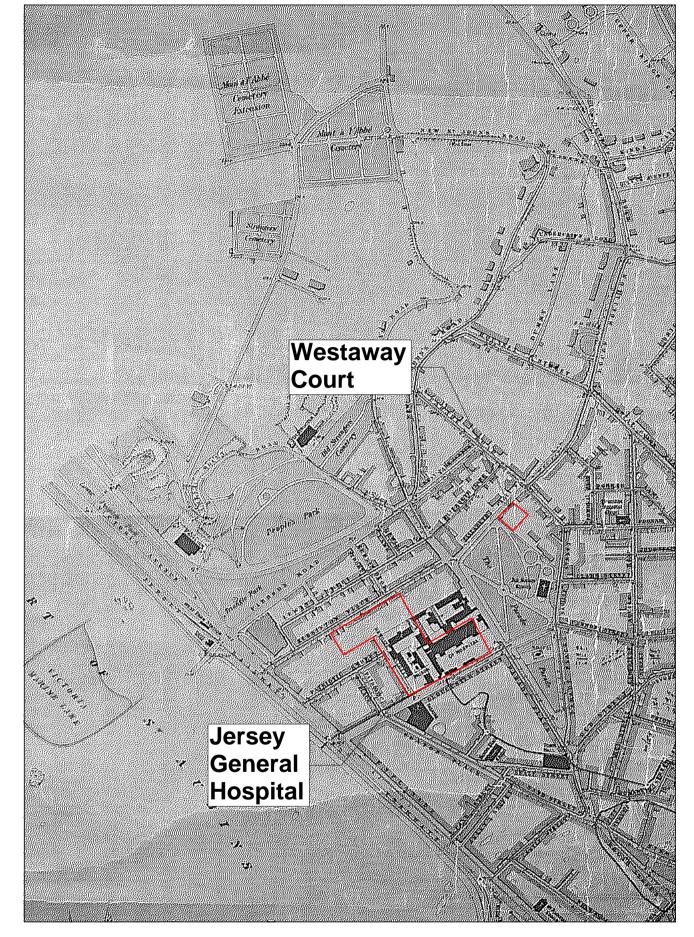


Leaden Published at the Admiralty 10th June, 1968, water the Superintendence of Coptain G.H. Richards R.N. F.R.S. Hydrographer. Large corrections Jan. 1869, Jan. 1900. Sold by J.D. Better, Level for the Admiralty Charte 145 Misories.

Approximate site boundary

Appendix C Historical Map:

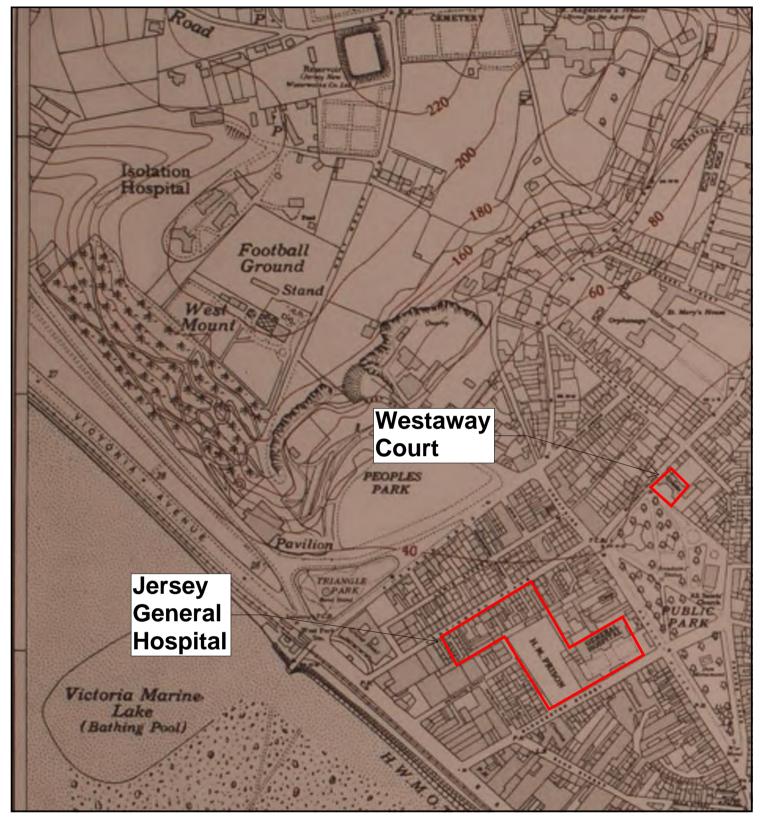
1900



Approximate site boundary

Appendix C Historical Map:

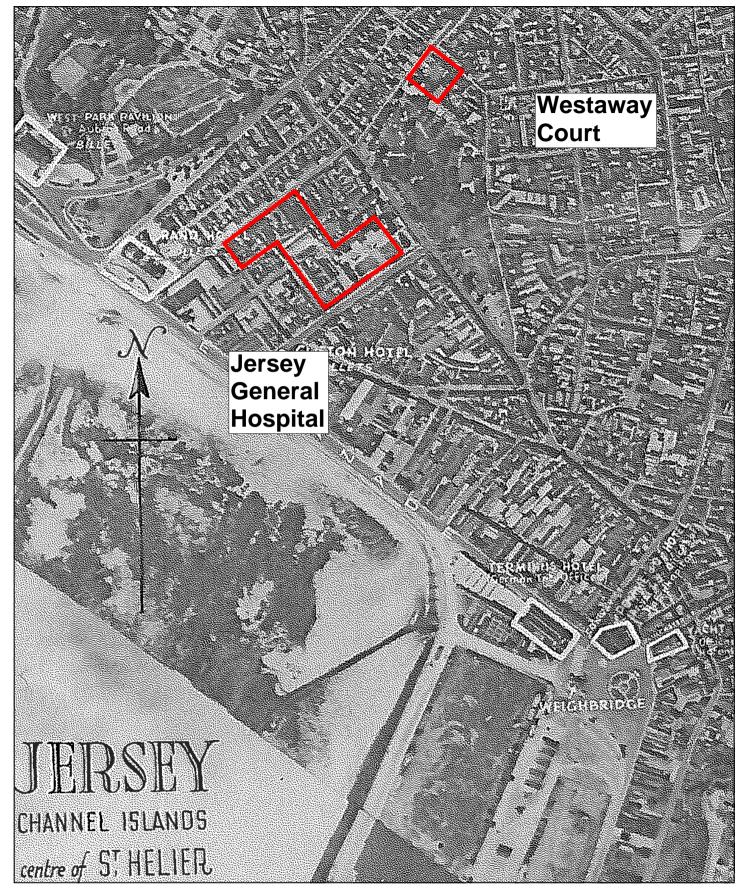
1907



Approximate site boundary

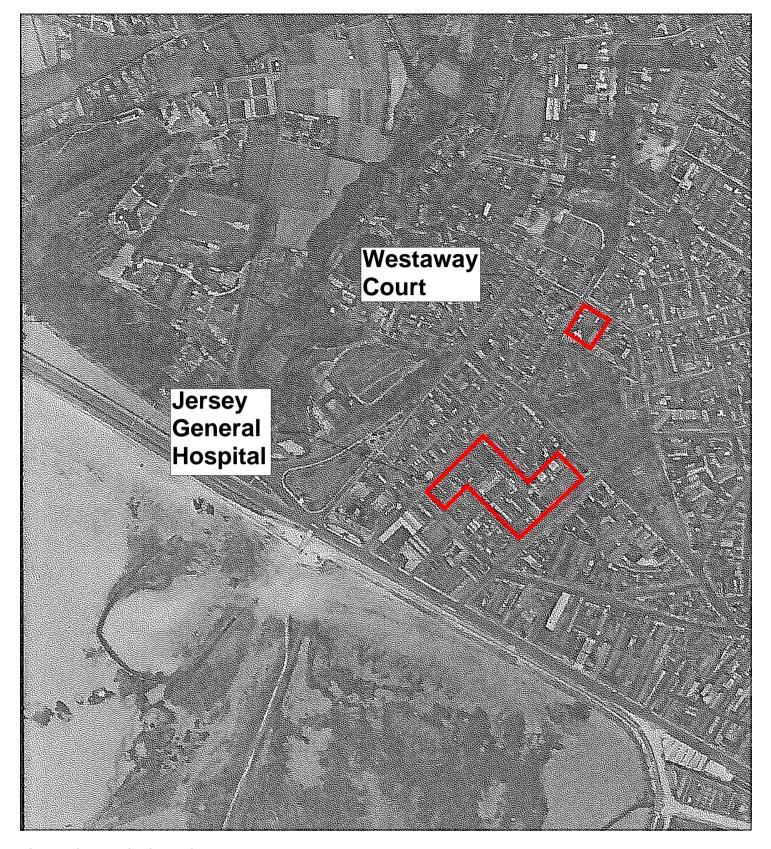
Appendix C Historical Map:

1968



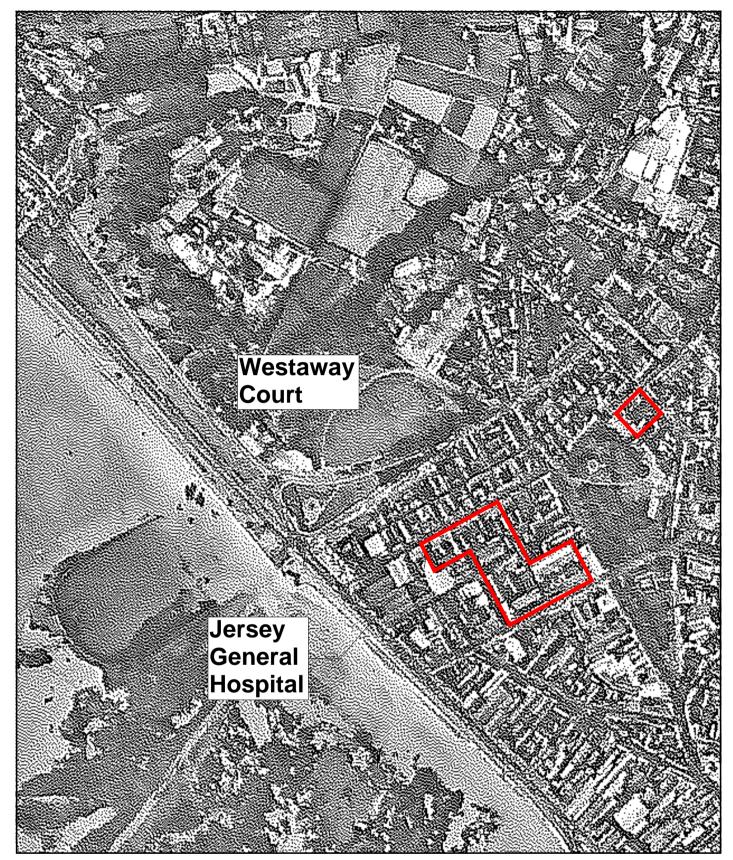
Approximate site boundary

Appendix C
Historical:
1943 Aerial Photo
Jersey General Hospital &
Westaway Court



Approximate site boundary

Appendix C
Historical:
1944 Aerial Photo
Jersey General Hospital &
Westaway Court



Approximate site boundary

Appendix C
Historical:
1965 Aerial Photo
Jersey General Hospital &
Westaway Court

Appendix D

Historical Ground Investigation Records

Appendix D

Historical Ground Investigation Records

- Foundations Engineering Ltd, Jersey General Hospital, Phase 1 (6th/12th March 1973)
- Geotechnical Engineering Ltd, Jersey General Hospital, Phase 1B (12th/14th July 1979)
- Geomarine Ltd, Main Theatres Upgrade SI, Jersey General Hospital (7th/8th March 2014)
- Amplus Ltd, 33 Gloucester Street, Raliegh House (4th/5th February 2000)
- Amplus Ltd, 15-16 The Parade (11th September 2006)
- Gloucester Street surface water sewer outfall drawing (Drawing dated 12th January 1982)
- Patriotic Street MSCP (Records dated 1983)
- Amplus Ltd, Kensington Gate Car Park, (8th/12th January 2007)
- Geomarine Ltd, Kensington Place, (16th/21st July 2009)
- Amplus Ltd, 66-72 Esplanade (21st March / 2nd April 2014)
- Matthew F Warner & Associates Ltd, Westaway Court (4th/6th January 1994)

RECORD OF BOREHOLE No:___

JERSEY ST HELIER HOSPITAL

cation : ST HELIER HOSP ntract No. : CF 669 /1121 H

be of Boring: Shell and Auger

te (started) : 12: 3:73

Borehole Dia : 8 6 6 6 Casing : 6 to 33 6

Ground Level : 32 1 ft OD.

Sheet 1 of 1

£ (31	.u. scaj	. 12 3 13				20	ieet	1 01 1
epth	Water	SAMP	LES		2.	TRATA		DESCRIPTION OF STRATA
of axing	Fevel	Depth	Тура	No.	Legend	Depth	Thickness	
				· · · · · · · ·	333333	G.Z.	/* a*	MADE GROUND-Tormach
		1. 5."	ם .	1 .	/	" a"	****	2" overlying compacted
								sandelone.
	٠							Medium dense light brown
				_			7: 3"	fine billy SAND with pebbles
		(N·20) 5'- 0"	۵	2		• : '	, —	below 7-6
		· ·						
		7:6.	Φ	, 3	000	71.		
		8. 6"	٥	4	2	. 6		Loose light brown/gray
. • 1. •		(N.5) 10:00	۵	5			3-6.	silly SAND.
						240		
		12'. 0"-13'. 1"	U	Ø		~ ~	2:0	Firm light brown sondy very
` · · `		/3.6"	ط	7		41.0"	1	silly CLAY.
		14:0	Δ,	8		* *****		•
		(N.23) 15:0°	Q.	7			4:0.	Medium dense brown silty
		and the second s				. , .		dayey f.m. SAND.
		18'-0"	0	10		g: o *	2:0"	Firm to stiff grey silly CLAY
		19-0-20-2"	U	//		20-0"		11 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		20'-0"	٥	12	000			
		(N. 24) 22' 0"			200		5:0	Medium dense sandy
		22' 6"	0	/3	200			GRAVEL (/ m.e.)
					0°0	. , ,		
		25'- 0"	0	14		25: <i>o"</i>	1.6	Firm grey cilly CLAY.
		25' 6 - 26' 8"	U	15	2	26-6	1	Medium dense dork grey
		26.6	0			28'.0'		silly fine SAND.
3.0"	5' 8'	28'- 0"	Φ	/7	*		1- 6"	Firm grey clayey lominated
· '' ·		29:6"	D	1	**************************************	29 . 6		SILT
		30-0-31-0"	Ü	19			1:0	Still grey slightly willy CLAY
		52' 6"	0	20				with fine grovel - below 32:6"
. •		33.6	1	2/		'6 ' ڈڈ		brown and without gravel.
		۵۰۰۵					2 0	
33' G	· /o': 5	(MAS 35'- 6"	۵	22	€.0.8	35 ' 6	"	slightly weathered very fine grained MUDSTONE.
i at of	8' 3	. Initial 2").	W					grames - 102-10 -
:							-	
		į,						
		<u> </u>		<u></u>	_11			<u> </u>

S: Chibel used for 2 hours 30-6" + 35-6" to prove bedrock.

Water added to assist in shelling, and to prevent sond and gravel from blowing.

RECORD OF BOREHOLE No:

JERSEY :ST. HELIER HOSPITAL . Location

Contract No. : CF 669 / 1121H

Type of Boring : Shell and Auger

Date (started) : 10: 3:73

8 to 20 0, 6 to 34 0 Borehole Dia

Casing

Ground Level : 27.9 ft OD.

Sheet 1 of 1

o e		Water	SAM	PLES		T	STRATA		DESCRIPTION OF STRATA
lime	Carroa	Level	Depth	Туре	No.	Legend	Depth	Thickness	
D 3:		1				SUSSE	G.L.		MADE GROUND: 3" formes
								2:6	over 3" roadelone overlying
ļ]		2'- 6"		granile boulders and slabs.
1			3-0"	ص ا	/	×			
٠.			(N.17) 5:0°	٥	2				Medium dense light brown .
. 1 .						×			slightly silly fim. SAND.
			7-0	٥	3			10-0"	Horizon is sark brown and
						× ×	٠.		very wilty 7'0 10'0"
.					١,,	*			
			N. 22 10. 0°	0	4				
			12: 6	D	5		12'6"		
					'				
			15' 0'-16' 3"	U	6		**.		Soft to firm brown sandy
.]							1	6:0"	silly CLAY
.]		16-6"	Ø	7	=			
			18'-6	0	В		18:6		Soll to firm brown/grey bondy
1000	20:0	5.6			. –	<u>×_×</u> =×			SILT. with some clay.
3.73	4	_	20:0:21:2"	U	9	I			
	20.0	6'3."	21.0	D	10		21:0		Medium dense light grey/ brown
			, ,		,,	****	23:01	2.0	sulty f.m. SAND.
•			23' 0"	<i>D</i>	11		23.0		
			25.0":26: 4"	U	12			3.0	Firm green/brown/grey CLAY.
			26: 0	0	/.5		26:0	1	
			20-0			500		2:0"	Medium dense sondy GRAVEL
			28: 0	0	14		28'. 0"		with some green/grey day bind
		.							Province
٠.		. [30: 0 - 3/: 3"	U	15		-	4.6	Soft to firm grey brown
			3/2 0	ص	16			1	Billy CLAY
			331 - "		17		32'6		Stiff brown billy CLAY with
			32'- 6"	О	''			1'. 6'	traces of graves.
			34' 0"	ے م	18		34'.0"	_ ,	. [
			N1591 35: 0"			心影	1	2 0	Hard grey elightly weathered
			Initial 1/2)		j,	£.0.B	36-0"		porphydia DOLERITE
				W				-	broken with clay smears.
			1	}	*				
				İ					
			L	<u> </u>				<u> </u>	

REMARKS: ground and 1/2 hrs. 34 0"

JERSEY

Location

: ST HELIER HOSPITAL

Contract No.

: CF 669 /1121 H

Type of Boring: Shell and Auger and Rotary Core
Date (started): 6:3:73

RECORD OF BOREHOLE No:

Borehole Dia

Casing

8" 6" HX

8" to 20'-6" 6 to 40'-6"

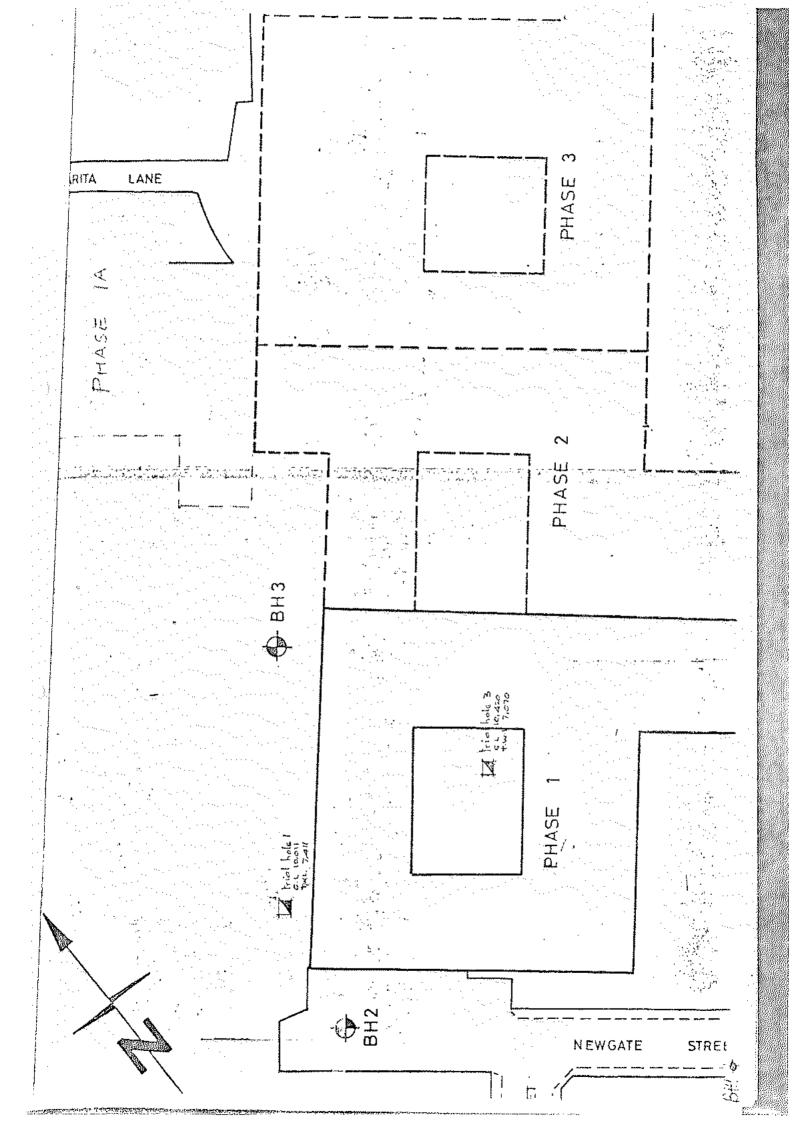
Ground Level: 34.8 ft 0.D. (10166 m 00)

Sheet 1 of 2

ĺ									
e d	Depth	Water	SAME	LES	····		STRATA		DESCRIPTION OF STRATA
Te e	Casing	Level	Depth	Туре	No.	Legend	Depth	Thickness	
د7 ،			/\a	Δ.			0.L.	/: a*	MADE GROUND: concrete ducting.
:								3' 3"	MADE GROUND: Brown band with grovel and brick
	. •		A: 6' (MAI) 5'-0	о Д	2 3		4:6:		
								4'.6"	Dense light brown slightly willy fim SAND
	· . ·		9:0"	۵	4	×	91-01		
			(~.19) 10:0	D	5	×		4.7.	Medium dense dark brown cloyey silly SAND with
	•					V.		7 60	some organic maller.
			13' 6"	Ð	6	×	13:6'		
			15'0"-16'0"	υ	7			3.0	Firm brown yellow sondy CLAY
	· .		16'6	Δ.	8		16 6"		
						*		φ: <u>α</u> "	Medium dense brown/grey
			(N. 22) 20° 0°	0	9	*			silly for SAND
-	•		22' 6"	۵	10		22'6"		
			25' a"- 26': a"	Ų	"		٠	5 6	Firm to stiff light grey sondy willy CLAY
			-			y .	28°0"		
			28: 0*	Д	12	3.0			Medium dense sondy GRAVEL (I.m.c.)
			[w·23] 30' 0"			, 0 o		A (O)	GRAVEL (f.m.a)
			52% o	ص	د.⁄	200	32:0"		,
				W		34 -		5' 0"	CLAY.
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8510-361 /	U	14	X		.	
		7	37. 0"	٥	/ <u>\$</u>		37.0	2' &"	Still grey/green / brown CLAY.
_			39' 6"	0	16		39 : 6 40 : 0")	r'. o ·	Dense GRANEL and cabbles.

EMARKS: Water odded to assist

> Three Trial pite dug to locate of them.



DOREHOLE LOG

CLIENT STATES OF JERSEY

DEPT. OF PUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL

DATE 12-14 JULY 1979 GROUND LEVEL 10-30M. AOD.

BOREHOLE No 1 (Sheet 10 + 2)

SCALE 1:50

رن	propress and	casing record	de renption	SP1/	core	o c pth	He ve'	
	12 JULY	. !						
			Made Ground and with some gravel and brick.		٠			
			y ard was rice.					
				1		-1.98	9.30	2
		rui	Mading daying broading looser	Ñ . (17)		1.17	• • • •	
			Medium dense becoming looser with increasing depth, while fine		o			,
• .		•	SAND	. ,	3			
					grilling.	2.00	. •	
		kii		4. (10)		2.17		
	The state of the s		becoming pale grey fine and medium. SAND See Remarks 2.	1				
			SAND See REMORES 2.	!				-
	j			1			<u> </u>	1
	Smick water	rui.		TH= (6)		3.17		-
	at 4 00m.		•	1		1		
	lievel ofter			1		1		
	isinking 4 ox	• •		4		4.17	6-30	-
	Botore waite	nil '	Medium dense orange proximising	₩ •(e)				
	HUSK 4-00		fire Sand	1	1	4.50		
	den Acu -			-	12 7	4.80		Į.
· · .	PM After Husting in			·į	8	.]		1
	casing -at	Ì	_	T		5.51		ľ
	surface	5.15 P.M.5-G	5-80-5-85m. band of sity fine 500	n -(16)			10
	13 JOLY		with the grave.		1		1	
	A.M. J-45	S	6.25-6.30m. band of party	:		. j . '{	<u> </u>	
. •			cemented silty fine sand	_		_6-30	4-00	-
			Medium dense orange mortled grey			6.65		
		6.49	fine soudy Silt with some iron-	14.02)	0 63		
		1	situited partices. Lamitated from	*		- [17.
			6.30-6.50m. and 7.45-7.50m. A little clayey below 7.50m.	1	† 	1		1,7
		. 4	To make condend town to make	1		7 67	į	1
		7.51	1	ो्भ ÷(a;) <u>2</u> 7	ţ	1	ڒڒٳ
· . ·			Madure days a could amore walked	-	Δ.	1	2.30	1
		1	Medium dense grey green motified orange silly fine Sano and fine	, ب		6.30	2.00	\
		1	GRAYEL.	1,		5 60	$\mathbf{p}_{\mathbf{j}}^{\dagger}$	10
		8.44		4)	.]		[·
			Dense grey silly fine SAND and fine and mealum CIRAVEL	_		l l		10
		1		ļ			:	1 0
		_	See Remarks 2.		<u> </u>	_ = > 6	0.70	
			Continued in different strotum on Sheet	2.				
٠			A CONTRACT THE RESIDENCE OF THE PROPERTY OF TH					
	1	1		:		1		
	;	j		} :	į	1	[
				i	; ;			
E	1	had start	le, open-drive or prepared from drill coxe	<u></u>	GEL	JOB No	FK	LL SUR
	U(+C(5))		nes egent ette et et etenemise vett – i sene		1		1 '	

REHOLE LOG

STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS JERSEY GENERAL HOSPITAL 12-14 JULY 1979 GROUND LEVEL 10-30M AOD. BOREHOLE No 1 (Sheet 2 of 2)

SCALE 1:50

propress and	COSIMA		SPT/	core.	<u> </u>		<u></u>
y water level		Ge kChpt-on	RPT	sample	depth	he we!	•
	!	<u> </u>		1	1		<u>. </u>
1	1	1		i i			i E
· — —	·				9.60	0.70	! }
13 JULY	9.50	First gray bounded fine savay SILT	J. Can	T	9 67	0.70	6,20
		with pase grey time sand landmations,	(20) : أ				
	1	dark grey clayey silt bands, some		9			, ,
	<u>ج</u>	brown staining and black organic		وساانه			, , ,
	₹	inclusions. Occasional rounded fine	:	ક			
1	ن ا	oravel amond 9-60M. Becoming	1 .		10.71	-	* _ ~
) है। ० -इड	. Slighty clayey or increasing depth.	1.(15)	N .	$H \cdot DO$	-0.70	
	F	Shiff and Taminated below to 95m.	•	§ 5			
	•			Ü		*. *	· .
	11-29	Very stiff grey mottled yellow grzy	- - - - - - - - - - - - - - - - - - -		11.45		
		clayey sardy SILT with strong and lyghy weathered iron-stowned	ا دين آ				
	[highly weathered iron-shirted		준			* v _*, *
	i: ▼ 1つ.ラ∡	. Iraaments of meta-sillstones.	į	4	12.20	-1.90	· •
	12:24	CONTRACTOR VINE TO THE PROPERTY OF THE PROPERT	, #	g 5	12.36	ĺ	7×
•	c		I (•(128)	≛ ¶5			ر د م
		1 THURS WELD REPORT OF THE PERSON AND THE PERSON AN		drilling Zank, pio	-12.75	-2:45	
	d i3-002	fragments of META-SILTSTONES,	l	27.			つー
	ন্ত	friable below approx to este	ļ	5 17	1	.	× ×
	į	Constant]		ĵ	į	7/
	Ĵ 13·35	Completely weathered very weak		dianord an.	- 1	1	سرد
	<i>b</i> 7	pale grew fine grained gravel		올ի성	i	ļ	v х
		META-SILISTONE Programments		-इ । ब	-	Ì	~
	,	in a silfy clay matrix.	ļ	HÝL	_14-20	-3· 2 0	<u> </u>
M 2-60	3.35	Moderately weathered very strong pale	ł	Nater-Fluste	į		
- JULY	AM14 55	greensh grey lightly metamorphosea	į	三丁의	1	· ·	
M 1 45	į	Chiorite rich MUDSTONE WITH COLCINE	ľ	2	Ī	į	
fore pulling		crystals, occasional pyrite and	- 1	\$	15.20	_ / 50	
1.96 I Durson	LCCOACLET	numerous calcite veins.	i		رسم ددا۔	-4-90	
P. M. 1.45							
16-19JOLY	.]	End of boretole.		1			·
1.45	· . [2					٠.
		Remarks		1			
		. Starter pir excavated to 0-75% depth.				1	٠.
	j	8.90-9.50m.	1				
	[5. SPT records.	1	· . į	1	-	****
	1		į				٠.
	- 1				· · · . {	.	·
		2.01 = (3) X 0 0 2 0 2 (2) A 4 (2)		. 1		i	
		2.01 - (3),3,2,2,3 8.44-(5),8,10,11,12		1	. 1	. 1	
		3-01-(2), 1, 2, 2, 1 9.50-(16), 7, 4, 4, 5					
		3-01 - (2), 1, 2, 2, 1 9-50 - (16), 7, 4, 4, 5 4-00 - (2), 1, 2, 1, 2 10-55-(5), 3, 3, 4, 5	وارونيات د واست		-		
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 11-29 - (16), 7, 9, 8, 14		paragui ferben verrenam Lel	***************************************	deployment of territoria errows	
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32		e add tries necessaria in contrata	***************************************		
	A de la constanta de la consta	3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 11-29 - (16), 7, 9, 8, 14		e made by the section of the section	***************************************		
	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32			TYPE I MAN TO ANALYSIS OF THE PROPERTY OF THE		
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
	100 m m m m m m m m m m m m m m m m m m	3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					

BOREHOLE LOG

BOREHOLE No 2 (Sheer 1 of 2)

CLIENT STATES OF JERSEY

DEPT. OF PUBLIC BUILDING AND WORKS

DATE 14-17 JULY 1979 GROUND LEVEL 11-60M. ADD. SCALE 1:50

+C10Qy	progress and		de rection of	SPY/ RPT	core. sample	depth	be vel	
	14 JULY							
			MADE GROUND - sand with					
			some gravel and brick fragments.					
				. •				
						1.20	10-40	
		Г					10 , -	
			MADE GROUND -yellow brown very			•		192
			silly fine sand with some poorly		ā	1.80	7.50	77.
			cemented pairthes.	Å·67)	=	1.99	٠.	
		rúi	MADE GROUND-pale yellow grey	선 177)	ਤ	İ		///
	ļ		and brown mothed fine and			1		$\times \times$
	Dawy below	1	medium sand.			200	ಕ.ಕಂ	XX
• •	3.30m.	ļ -				}	ļ	7.5.
·	Smock water	rul	Loose pale yellow fine SAND.	Ψ • (2)		3.04		
	ar 3.97	141		TW		 3.30	8.30	-
	level after		Medium dense yellow and brown				<u> </u>	
	striking 3-97		mediom and fine SAND.			3.77	•	
, .					A	4 00	7.60	-
٠.	P. M. 3.97	nil	Loose brown silly medium to fine SAND.	N (5)			•	
	! .		TRANSITIONAL	7 50		4.50	7.10	
٠. ٠	16 JULY	[Mad days provide oral is pieces					1
	A.M. 3.94	1 1	Med dense greenisk grey in places mortizd orange poorly laminated fine					٠ <u>-</u>
·. ·		nil	SOUNDER CHARGE BOOK GLEST	l Alimenta	1	5.02		** X
	}	10.	lammations and bands of claye,					
		1	silf. Some from nodules and			5.57		Y
٠.	1	i iin	staining.	- (1			7
						6.00		~ * * *
		5.86	Becoming less sandy with increasing	4			}	Y X
			depth.	1	•	6.56		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
		5.86	TRANSITIONAL	1.(12)	民,	6:56	4.90)
٠.			Blue arey mottled yellow poorly		- 0	7.00	,	Y , ,
			laminated fine sandy SILT with	1				* *
		6-86	some from staining along borninations.	İ	i	1		
			Clayey between 7.40 k and B. 20m.	J		7.5€	1	Y
٠.		6.86	Band of yellow cemented silty fine	4-(12)	4	İ		21.
· .			sard at 7.90m.	ì		8.04	1	¥. ±
		7.56	·		1			
					4	L8:50	3-10	-
-			Continued in different stratum on Sheet 2.		1	1	1	
			Prince Hills Westerney and a sender and an an equal and a send and a second section of the principal of the second	1				-
					1			i i
		1			-			1 .
427						1	1	
2								
100		. مذراء						
			ه د د موسید ده د		1 3 3 3 Y	·],	
W-15,00	A COMPANY	All Control of the Control	e, open-drive or prepared from drill core		CEL	IOB No.	FIG	• • • • •

SOREHOLE LOG

CLIENT STATES OF JERSEY
DEPT. OF RUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL S.TE

DATE 14-17 JULY 1979 GROUND LEVEL 11-60M. AOD. SCALE 1:50

BOREHOLE No 2 (Sheet 2 of 2)

оюду	progress and	٠ .	aes⊂nptio∩	SPT/	core.	depth	Se vei	
						_8 50 8 60	3 10	202
	16 JULY	7.86		14 (41)			j	
		1.00	Dense yellow silly fine SAND	1				$\triangle \mathbb{Z}$
	, a trace t		and fine and measure suppregular		₽		. 1	<u></u>
			GRAVEL WITH a little subrounded		drilling 0-	9.40	. į	,
			gravel.		हे ह	9.80	į	250
						9.95	į	7
		7.79		N (35)		10.20	1.40	1000
			The Comments					
		·	Firm pale grey silly fine SAND		8		į	
. ·			with arey hine sandy sill laminations becoming time sandy		· •	10.72		
		10-72	SILT with some sandy laminations,					
	1	انا	with occasional organic patches.	1	1	11:15	O-45	¥
		D 10-72	TRANSITIONAL	₩·(Œ)	[11.60		
· .	Before water	, ,	T IKWADII IDAWT	1	준.	11.75	•	
	Hush - Dry	153	Firm grey laminated very silly fine	*	1	12.15		200
		12.01	Spardy (LAY WITH OCCASIDAD)	-r <u>v</u> =(100)	! !	12.20	-0-60	* * * ×
	<u> </u>	12.30	ordanic politices. A little rine	_ ` '		12,30		2
	Ì		aravel below 11-80m. Becoming		drilling			· •
	P. M. 3.64	P.M. 12:45	a greenisk grey sandy SILT		₹ ₹			2
	17 JULY				8			
· · · .	A.M.3-60	12.95	· · ·		dumond core	S		
			Shong moderately weathered grey to greenish grey META-SILTSTONE.		12 17	3	٠.	¥
	Before pulling		from -starred along most		1 2 1			y
	CORING 3-94	? [discretifuities. 3 joint sets	}	3	4		
			recognisable, one vertical, one	Ì	1 . 1			۲
	İ		60° dip. loirly separation approx		2			\ \v
			lorunt, one 75 aip, joint separation.	· •	à			1
	P.M. 5-7	8	approx. 40 mm.		Water-flush) ×
		12-2-	The state of the s	1	1	TE-01	-3.4	
	18-21 July	Y TECHNOLOGY	A little clay snearing or joints			1		
	B-17		above 13 som. Some joints open				1	
		1	to 2 mm. or calcite infilled,	•				1
			penerally < 1 mm.					
			Numerous calcille veins.					
			End of borehole.		•			}
			Remarks. II. Sharter pit excavated to 1-00m depth.		.]			
			2. SPT records.					
			1.83-(5),5,44,4 7.40-(5),4,5,4;					
			288-(4),2322 8.44-(6),9,10,10,1		. }			
			3.97-(2),1,1,2,1 9.79-(5),9,12,B,1					
•	The second		5.42-(4) 3,4,4,3 11-12-(6),3,3,4,					
			6.40 - (5) 4,3,4,4 12.00 - (6),24,26	-[
			3. Piezometer installed: tip at B.Gom. response zone B.10 - 9.10m.	-			1	{
			trakuse roug and - Sugar		1			
				<u>_l</u>			<u> </u>	<u></u>
Market Sept.	CONTRACTOR OF THE PARTY OF THE	shed same	ole, open-drive or prepared from drill core	;	,	JOB.No.	FIG	

BOREHOLE LOG

CLIENT STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS

SITE

JERSEY GENERAL HOSPITAL

DATE 18-20 JULY 1979 GROUND LEVEL 10:00M. AOD

BOREHOLE NO 3 (Sheer lof 2)

SCALE 1:50

⊋≠0 / 00	progress and water level		σεεςτώτι ο υ	SPT/ RPT	core, sample	G epih	Sevet	
	المال الكا				<u> </u>			
			MADE GROUND - Sand with some					
	i		gravel.	. *.				
			<u> </u>					160
				<u> </u>				K
						-125	6 75	
				T		1.42		-
		rùl	tat at a material language	r (15)				
			Medium dense pale yellow grey		5			12.60
			fine Sand becoming white below 1-60m.		drilling grant		٠.	' . '
			pack t-point.		8	2.49		13.5
		rú(+ (2)				
1		1970 		1			-	
1			Loose white fine and medium SAND.			• •	7.∞	1
	Dough below					3.20		-
	3-20FL	[Loose brown fine and medium Sand	! ! T		3.49		> -
		.5·20	with occasional dark brown silly	H = (6)				
			patthes.			4.00	6.00	
			Crompe brown silly medium to fine		•			1
			T SAND.			- 4·25	5.75	TV.
			TRANSITIONAL J					÷ .
		4.28	Medium dense blue group poorly	į	8 1	4.80	5.20	* -
			laminated very silky fine Sans.	<u> </u>	8			l'v
			TRANSITIONAL	{ !				Ţ,
Ì		4.28	<u> </u>	4 : ((5)		5.36		, v
		•	Firm blue arey mothed uslow laminated hine sandy SILT with	I				z " w
		į	some iron-stational along levels.			ေသ		* * ·
		6.00	5-60 -5-80m. Wer sill pour his		•	w. W		· > `
			extensive iron-staining.					1540
				1,	-	6.56	٠.	Į,×,
		6.00		r =(13)				J
			Breakly war blue and clause from	*				J
		7:36	Becoming more blue and clayey from 7.10-7.20m.		_	ļ	i I	J = 1
		/ 26	7-10-7-2016.		<u>Z</u> .	7-36		Y.
				<u> </u>				Ĭ,
			The same of the Control of the Same of the		. *	77.78	3:33	
	Smick water	1	Dense yellow silly fine SAND with some fine gravel.	4.(35)	A	+6:36		FO
	or 8.26 Level after	7.36	Some time graves.	T		8.25		10
	striking 6-00	1	Dense to medium dense grey becoming	[Ø	6 ∙65	İ	15.0
	1 2 2		brown silly Sand and him and		!	0 03	<u> </u>	c ?
L	_1		medium subrounded to subangular			9.00	1.00	
Γ-		T	GRAVEL, strongly ironstained at	1		[
	10.00		8-60 m. Occasionally subrounded]
			coarse gravel.					
								l
	The second of		Continued in different stratum on Sheet 2.					
	J • 1				1			1
*				1	-		Ì	
Total .	4 E] ;-	•				ļ	
		Bar.	•	1			ļ ·	
A OLY	and the Philipper to seem	aprobational de la companya de la companya de la companya de la companya de la companya de la companya de la c	el open-drive or prepared from drill core	 	-	OB No.	FIG	<u> </u>

OREHOLE LOG

LENT STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL

18-20 JULY 1979 GROUND LEVEL 10-00M AOD.

BOREHOLE No 3 (Sheat 2 of 2)

SCALE 1 50

-ФСУ	progress and water level		de #chptión	SPT/ RPT	core eample	depin	level	
	WAIG! HEVE						1	
1	İ							
	:						i	
	•						-	
- 1				.		1900	1.00	I STATE OF THE
	18 JULY	9.00	Firm orange orawn silky fine SAND	3, 120		9.16		Sec.
	P.M. 3-26	PM.9 20	(100mm) becoming blue grey laminated	4.62	· <u>ह</u> '			
	דיוער פו		slightly clayey fine sandy SILT with		<u> </u>	9 55	1	
	A.M. 3:40		more than one includes and		י ש	9.75	į	_1 _2
			black organic inclusions,		ω I	10.00	Ì	
		9.20	9.75-9 BSM. very wer sill bound,		203		- 40	٧ - ٧ - ١
			_ becoming very silly fine SAND _ r	-ţ	· .	10.40	-0.40	<u>,`</u> =`:=`:
٠.		15	between 10 00 and 10 20 m.	N: - (14)	_	10.55		-
		F 3-20	TRANSITIONAL /	4,000	ρīg	10.80	i	
•		£ 11-∞	Shiff blue grey laminalted very silty	┪	5 1	11.00	- 1.00	~ *
		K)	CLAY WITH OCCOSIONAL SUPPOUNDED		drilling			,,,,,,,
		K.	Fire gravel		के हैं			 سر با _ا سر
	j		1		2 1			مست مرار دا
	ļ		Highly weathered rock fragments in		8			, x
		*	a silfy CLAY.		ā			
	P. M. 3.60	PMIZO	Highly weathered strong dark grey,		chomorto		Ì	x '
	20 JULY	1	in places laminated, lightly		S			1
	A.M. 3-60	•	metamorphosed MUDSTONES with			<u>.</u>		ļ. Ÿ.,
	Before posting		class smeather on some wint haces.		3 .] [
			Becoming grey META-SILTSTONE.		7			X
	meng 3-60	1	moderately weathered and massive		Mer. Aust			
	P.M. POC	12-01	1 1 . The second second second second second second second second second second second second second second se		31	13.50	-3· <i>5</i> 0	*
 :	1	TECOVERE	most wint surfaces Seaton sets				٠.	
٠.,	l service i		of high angled joints. Average					
			separation 200-300 mm.					·
			Becoming dark grey and more					} ·
			fine grained below 13 00m.					
			Laminated in places with				•	
			occasional banas including] .
			pyrite crystals.				· ·	
			! " " "					1
			Bedding approx.10° dip.		1 .			
	**********		<u> </u>	.		· [- · · · i		
	***************************************		End of borehole.					
٠.	1		Remarks.					
٠. `			1. Starter pit excavated to 0 7Em depth.			.		
			2. SPT records.			·		
			1.33 - (5),4,4,4,3 6.40 - (4),3,3,3,4					1
	1		2-33 - (4), 2, 2, 3, 2 7.60 - (8), 9, 8, 8, 10					
	January States		3-33-(2), 1, 2, 1, 2 9.00-(6), 8, 9, 4, 4					1
		•	5.20 - (4), 3,4,4,4 10.40 - (6), 3,4,4,2	5				
			3. Piezometer installed: Yip at 13 com.					1
			response zone 12.50 -13.50m.					}
							1	
					.]			1
	ું ફે	1					1.	1
33		4				1		1
				ŀ	-∤-	- **	ļ	1 34
			· ·					1
-000		20 Que -	le open-drive or prepared from drill core	- K-356/65		JOB No.	 	URE

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Saleto .

B. Spin

PHASE IB - GENERAL HOSPITAL - JEF EY C.I.

Geomarine Borehole No. Les Ruettes, La Grande Route de **Borehole Log** St Jean, St John, Jersey, JE3 4FN Tel: 01534 856566 GEOMARINE BH₁ Email: enqueries@geomarine.je Sheet 1 of 2 Project No. Hole Type Jersey General Hospital, Main Project Name: Co-ords: 564726.84 - 5448673.17 Theatres Upgrade SI CN 1343 ВН Scale Location: St Helier Level: 13.00 1:50 Logged By 07/03/2014 - 08/03/2014 Client: **Property Holdings** Dates: **KMS** Samples and In Situ Testing Water Depth Level Well Legend Stratum Description Strikes (m) (m) Depth (m) Type TARMAC 0.10 12.90 DRILLERS DESCRIPTION: TYPE 1 (MADE 0.30 12.70 GROUND) 0.50 12.50 DRILLERS DESCRIPTION: FILL comprising bricks, concrete, etc. (MADE GROUND)
DRILLERS DESCRIPTION: Orange coarse 0.80 12.20 SAND. (BEACH DEPOSITS?) Orange brown gravelly SILT. (BEACH DEPOSITS?) 1.20 N=6 (1,1/1,2,1,2) 1.20 - 1.65 SPTL 1.45 11.55 Grey-white fine SAND. (BLOWN SAND) 2 2 40 10.60 Grey brown laminated sandy SILT. (ALLUVIUM) 2.70 N=10 (2,2/2,3,3,2) 280 10 20 SPTL 2.70 - 3.15Grey mottled brown silty SAND. (ALLUVIUM) 3 3.25 9.75 Green grey sandy SILT. (ALLUVIUM) 3 55 9 45 Green grey laminated SILT. (ALLUVIUM) 4 4.05 N=13 (3,3/4,2,3,4) SPTL 4.05 - 4.50 5 5.45 N=9 (2,1/2,2,3,2) 5.45 - 5.90 SPTL 6 7 7.15 N=16 (3,4/4,4,4,4) SPTL 7.15 - 7.60 8 8.69 N=22 (4,6/6,5,4,7) 8.75 4.25 Grey silty cobbly GRAVEL. Gravel is medium to SPTL 8.69 - 9.14 coarse, sub-rounded Cobbles are rounded. S 9 Gravel is of mixed lithology becoming a weathered Jersey Shale with depth. (ALLUVIUM)

Remarks

Ground level is arbitrary level. Water strike at 4.05m rising to ground level after 30 minutes. Borehole backfilled with grout on completion.



Continued on next sheet

Geomarine Borehole No. Les Ruettes, La Grande Route de **Borehole Log** St Jean, St John, Jersey, JE3 4FN Tel: 01534 856566 GEOMARINE **BH1** Email: enqueries@geomarine.je Sheet 2 of 2 Project No. Hole Type Jersey General Hospital, Main 564726.84 - 5448673.17 Project Name: Co-ords: Theatres Upgrade SI CN 1343 ВН Scale St Helier 13.00 Location: Level: 1:50 Logged By Client: 07/03/2014 - 08/03/2014 **Property Holdings** Dates: **KMS** Samples and In Situ Testing Water Depth Level Well Legend Stratum Description Strikes (m) (m) Depth (m) Туре Results 10.10 N=47 (6,9/8,9,11,19) 10.21 2.79 Grey blue rock recovered as medium to coarse 10.10 - 10.55 SPTL angular gravel of rock. 11 12 12.67 0.33 End of borehole at 12.67 m 13 14 15 16 17 18 19 20

Remarks

Ground level is arbitrary level. Water strike at 4.05m rising to ground level after 30 minutes. Borehole backfilled with grout on completion.



GEO	MARINE S	St Jean, S el: 01534	es, La Grande Route de t John, Jersey, JE3 4FN			Tri	al Pit Log	Trialpit No TP1
Desis			Hospital, Main Theatre	- Projec	nt No		Co-ords: 564730.80 - 5448668.93	Sheet 1 of 1 Date
Project Name	: Jersey (e SI	nospitai, iviairi Trieatre	CN 13	343		Level: 13.00	08/03/2014
				10			Dimensions 0.4	Scale
Locati	on: St Helie	r					(m):	1:25
Client:		/ Holding			ı		Depth 0.50	Logged GW
Water Strike	Sample Depth	Type	n Situ Testing Results	Depth (m)	Level (m)	Legend	Stratum Description	
> 0)	200	.,,,,	. toodito				TARMAC	
				0.10	12.90		BACKFILL - TYPE 1	
				0.25	12.75	*********	CONCRETE FOOTING	
							@ 0.25m Concrete footing protrudes 250mm from the v	vall.
				0.50	12.50		End of pit at 0.50 m	
							·	
								1 -
								2 -
								3 -
								4 -
								-
						1		

Remarks: Trial pit to identify foundation of retaining wall. Ground level is arbitrary level.

Stability: Good



		Geomarine Les Ruettes	s, La Grande Route de							Trialpit N	No
GEON	MARINE	St Jean, St Tel: 01534 8	John, Jersey, JE3 4FN			Tr	ial P	it Log		TP2	
				ļ						Sheet 1 c	of 1
Project Name:	Jersey Upgrad	General H	ospital, Main Theatre	S Project	t No.			64743.02 - 5448	676.87	Date	4.4
ivaille.				CN 13	343		Level: 1 Dimensions	3.00	0.4	08/03/20 Scale	
Location	n: St Heli	er					(m):		0.4	1:25	
Client:	Proper	ty Holdings	3				Depth 1.20	0.5		Logged GW	d
e a	Samp	les and In	Situ Testing	Depth	Level			_		I	
Water Strike	Depth	Туре	Results	(m)	(m)	Legend		Stratum D	escription		
2 07	· · ·	71		0.40	40.00		TARMAC				-
				0.10	12.90		BACKFIL	L - TYPE 1			
											-
											-
											-
											-
											-
				0.95	12.05		<u> </u>				-
				0.93	12.03		CONCRE@ 0.95 Cd	TE FOOTING	es 250mm from wall.		1 -
				1.20	11.80						-
				1.20	11.00			End of pit	at 1.20 m		-
											-
											-
											-
											-
											2 -
											-
											-
											-
											-
											-
											3 -
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Remarks: Trial pit to identify foundation of retaining wall. Ground level is arbitrary level.

Stability: Good

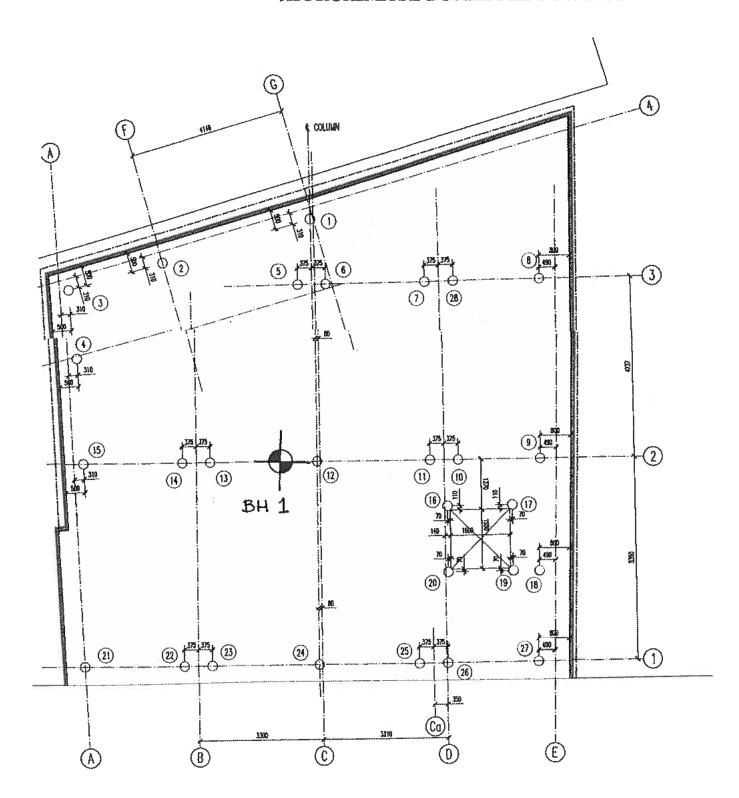




Boring Method	<u>IPLU</u>	Diam	eler		on & Georgians Specialists Governing		33 Gloucester Street, St Helier, Jersey Client	- [¹
Excavated Sitemaster	using a Rig		<u>. /</u>	sed to 8.94m			Raleigh House Ltd	
		locat as	dos Bite)	plan	Dates 04/02 05/02		Engineer Rothwell and Partners	
Depth m	Samples / Tests	Casing Depth m	g Wate Depth	Field Records	Level (mOD)	Depth m (Thickness)	Description .	
							Loose soil and rubble fill (driller's description)	-
						E (0.80)		×
1.70-1.44						0.80	Medium dense dark and light brown fine to coarse SAND with rare gravel	- 8
1.44-1.89	x 0.24 SPT N=20		DR	Y 6,4,4,5,5,6		E (0.85)		
1.44-1.57 1.57-1.68 1.68-1.86	x 0.13 x 0.11 x 0.18					1.65		
1.86-1.95 1.95-2.04 2.04-2.22	x 0.09 x 0.09 x 0.18	1.9	5			(0.60)	Medium dense light brown fine to medium SAND with rare rounded and sub-angular gravel	
2.22-2.50 2.50-2.95 2.50-2.95	X 0.25 CPT N=78 X 0.45		DR	Y 12,17,20,18,22,		2.25	Medium dense to very dense light brown fine to coarse SAND with rounded fine to medium gravel	
2.95-3.22	x 0.37					(0.75)		
3.32-3.40	× 0.08			Water strike(1) at 2.95m, rose to 2.82m in 15		3.00	Medium dense brown fine to coarse SAND becoming light grey in colour	
3.40-3.85 3.40-3.95	SPT N=24 × 0.42	3.95	8.99	mins. 4,6,7,6,6,5		(1.00)		
3.95-4.50	x 0.55					4.00		
4.50~4.95	SPT N=5	:		7 3 0 1 0 5	į		Soft light blue grey clayey SILT	* K
4.50-5.50	X 0.83		∡.16	1,1,0,1,2,2		(1.40)		
]		1		X_
5.50-6.00	x 0.50			04/02/00:3.2Bm		5.40		*
ا				05/02/00:2.88m	<u>†</u>	(0.50)	Soft dark brown organic SILT	:
6.00-6.45 6.00-6.88	SPT N=18 × 0.60		2.45	1,2,3,5,5,5	E	5.90 (0.35)	Soft light blue grey clayey SILT	, =
	Ė				n di di di	6.25	Fire to stiff light blue orey county	*
5.88-7.10	× 0.00	İ	Ì		F	ſ		
7.10-7.50 2.50-8.00	x 0.00 x 1.12				HT THE	_ 6.B8	Medium dense brown and grey sandy fine to medium GRAVEL	
					and the	(0.92)		
0.00-8.45 0.00-8.64	SPT N≈24 x 0.53	8.00	2.32	3,3,4,6,6,8	ուսակայանումում անուդերի	7.80	Soft to firm dark blue grey slightly sandy	K.
	x 0.30			ļ	· Hill	8.30	Clayey SILT	* 7
	× 0.00	6.94			E	(0.64)	Soft to firm dark grey silty CLAY with rare gravel	-
	TCR SCR I	RQD 0	FI 0	1	min.	B.94	Grey rock fragments in grey clay matrix	×
	100 0 (- 100 10	0 30	0			1	Dark orey slightly weathered fire and a	***
.60	91 0	0 :	10+		131111111111111111111111111111111111111	(1.01/	very closely jointed sub-vertical discontinuities, iron-staining on planar	**** **** ****
marks				1				Logg
v drilling	erom 1 20m -	mering s	a Sice				(app.ox)	Ву
cuid water	lling with wa struck at 2.9 ymbob and abbæv	ကောင်းရှင်း	ivsh fi i and	rom 9.00m - 10.06m rose to 2.82m bg1	m in 15 m	inutes	1:50 Figure No.	MFW

			n & Gept pacialists Gound L		33 Gloucester Street, St Helier, Jersey			
			ased to 8.94m			Raleigh House Ltd	Job Number 0139	
	/	location as site	plan	Dates 04/02/00 05/02/00		Engineer Rothwell and Partners	Sheet 2/2	
Depth Sam	ples /Tests	Casing Wa Depth De	ster oth Field Records	Level (mOD)	Depth m (Thickness)	Description	legend	
0.06			05/02/00:2-73m			Borehole completed at 10.06m		
ware and the same	ed from	ground 1	evel to 1.20m bgl			Scale to (approx) By	ed de de de de de de de de de de de de d	

APPROXIMATE BOREHOLE POSITION



PILE LAYOUT.

Amplus Ltd Foundation and Geotechnical Specialists

Boring Mathod Twintech TD308	Casing Diameter	Ground Level (mOD) Dates 11/09/2006		Cilent Tillyard for 18 the Parade Limited	Job Number 0948	
	Location as site plan			Engineer Beaumont Structural Consultants	Sheet 1/1	
Depth (m) Sample / Tests	Casing Water Depth Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend
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Remarks			THE THE THE THE THE THE THE THE THE THE			
randas robe hole drilled using a Twintech robe hole drilled using 110mm au 0.46m Refusal: presumed weathe to ground water strike using this m	308 drilling rig gers to refusal at 10 red rock head and s).46m bgl end of probe hole			Scale (approx)	Logged By GW

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Boring Met Twinlech Ti		1 '	Casing Diameter 110mm cased to 9.90m			Level (mOD)	Client Triyord for 18 the Parade Limited	Job Number 0948	
		Location es site plan			Dates 11/09/2006		Engineer Beaumont Structural Consultants	Sheet	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (th) (Thickness)	Description	Legend &	
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emarks obe hole dri	lied using a Twintech	308 drillin	g rig		F***		Scale (approx)	Logged By	
oe noje dri 10m Refusai ground wat	lled using a Twintech lled using 110mm au i: presumed weathere ler strike using lbis m	gers to refu ed rock hea ethod of b	usal at 9.: ad and er oring.	90m bgi nd af probe hole	· · · .		(approx)	GW GW	
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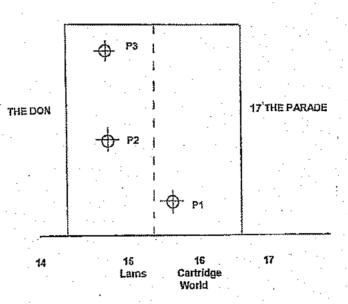
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BEAUMONT
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Amplus Ltd
Foundation and Geotechnical Specialists

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DRAWN BY: M.R.

CHECKED BY: 88.

SCALE: 1 to 50/500.

REG. DRG. N° T.S. 693. STATES RESOURCES RE Plan & Section of Turnel and Sewer.

701 Beach Outfall, Plan & Section.

702 Details of M.H.No.J - Drop M.H.

703 Details of M.H.No.Z - Tide Flap/Access M.H.

704 Location Plan

1 ypical Details. Gloucester Street
Surface Water Outfall BARTLEY, B.Sc.(Eng.); C.Eng; M.I.C.E; F.I.Mun.E; M.I.W.E.S. Plan 81 B.B. CURVES INCREASED TO 200m RADIUS
2 B.B. WORKING AREA IN PARK AMENDED.
2 B.B. Level of Connel at MH2 altered
and gradient MH2 to Ch.240.009
existing sewer details added.

BETAILS

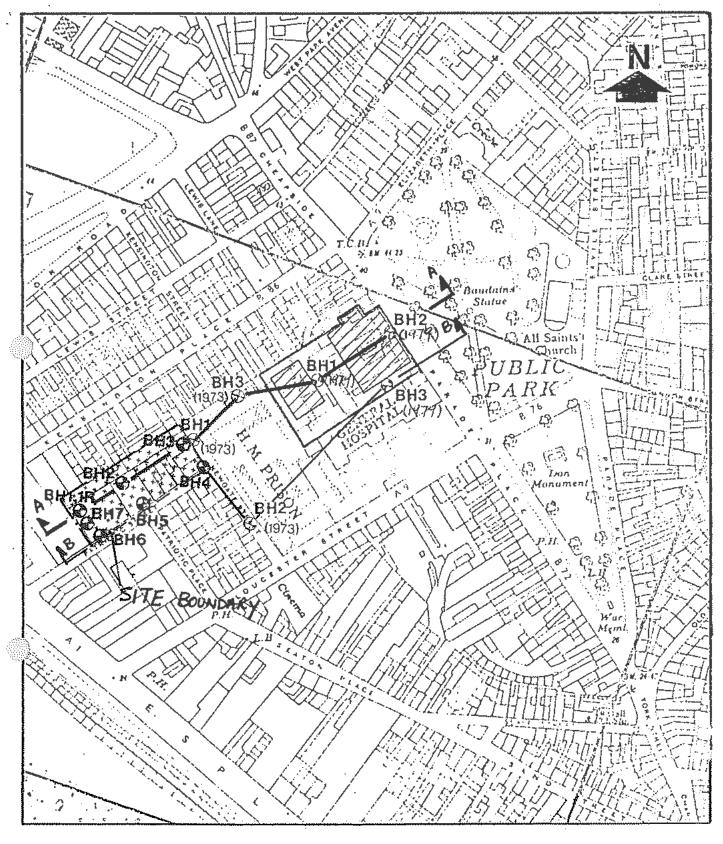
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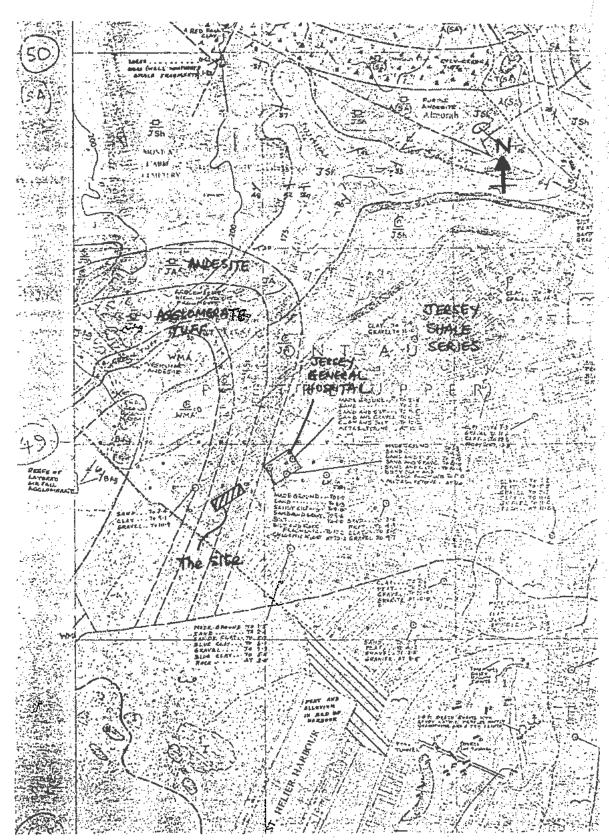
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				economica de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del companya del companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya		12289			
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	\$ 10 K 10	J. W. C.				Link			L



Scale 1:2 500

SITE PLAN SHOWING BOREHOLE LOCATIONS

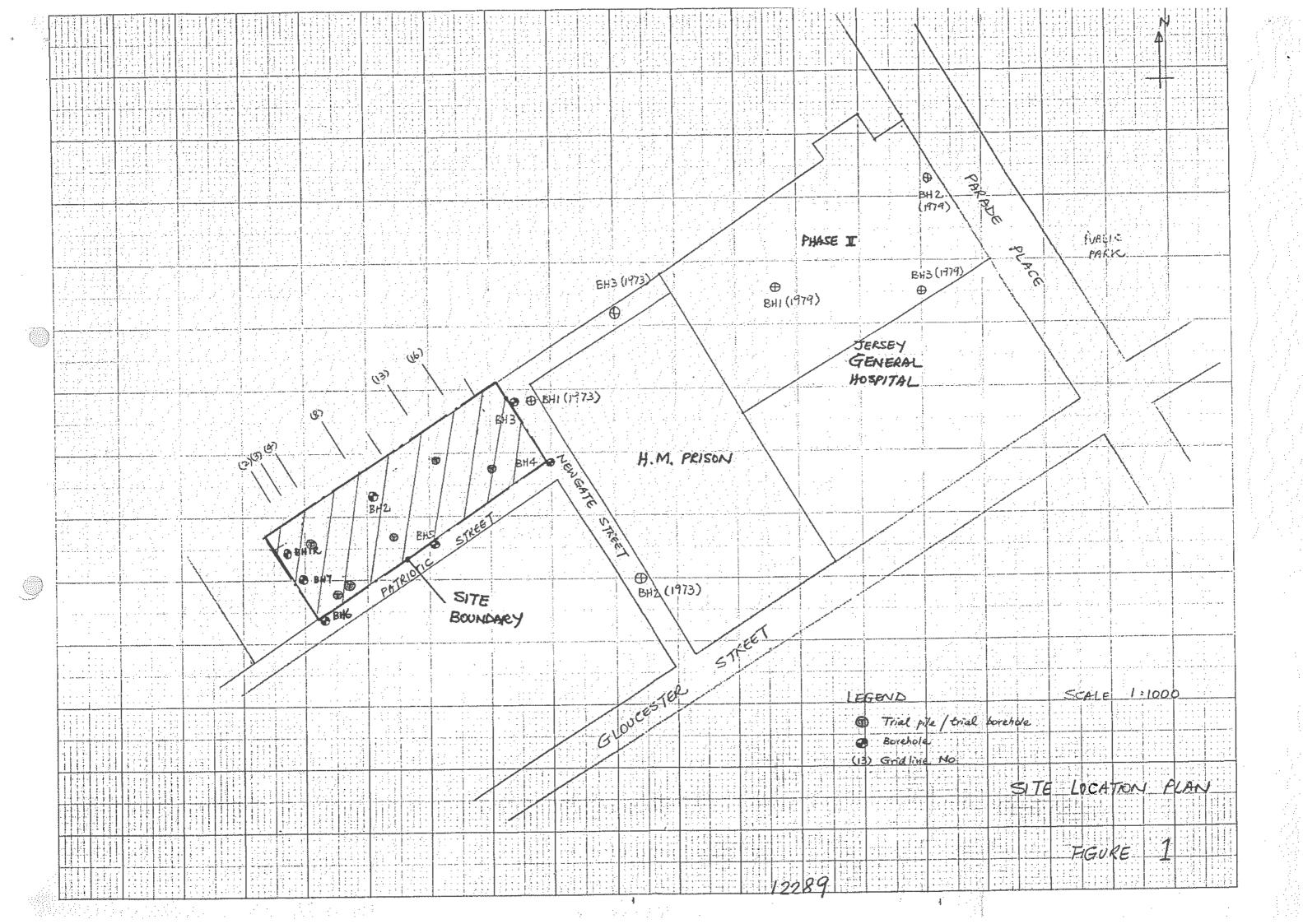
FIGURE 1



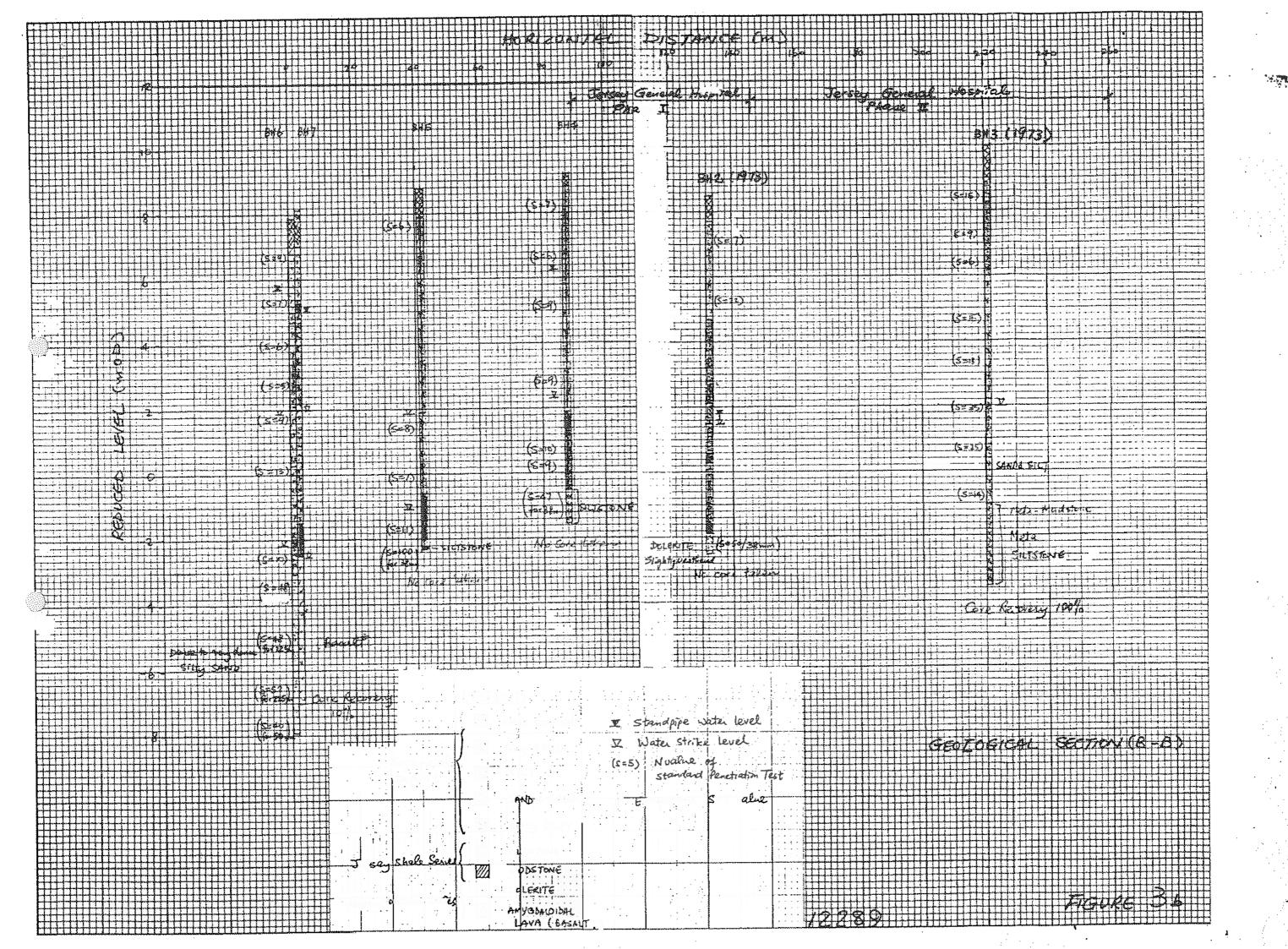
GBOLOGICAL MAP (UNPUBLISHED), STATE OF JERSEY SOURCE: GEOLOGICAL MUSEUM (LONDON)

SCALE = 1:10000

GEOLOGY OF SITE SHOWING UNDERLYING ROCK STRATUM
FIGURE 2



			H0&120	VTAL DISTANCE (	m)		
	2	30 40	. 80	0		200	240
		Assent Site	Jersey General H		ey General		······································
			6H3 (47%)	(70)	(1977)	)-oaf 55)	BH2 (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971) (1971
	BH	H1R BH21					
					<b>3</b>	-17)	(=9)
		(S-5) -	(S=77-X)	(5=19)		=lo) ::::: ::::::::::::::::::::::::::::::	(\$=5)
		(s=7) - <b>I</b>	(S=7)-1 (\$\sigma 5)		\ <u>\</u> \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		<b>4</b> ( <b>3</b> =(4·)
\( \text{\ } \)			(5=23)			(5)	
<u>\$</u>		(S=15)	(s=7)-(	(S=22)	1	=1/6)	(\$ = 15)
9			(S=3) (S=24)		7 (s	212)	U(G=17)
797	v	(S=15)-1 <del>1</del>	(S=4)	1	¥ (\$	:=8)	F(\$341)
CED C		7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 玉	(G=33)	:2)	s4i)	(<=35)
) (=} (=)	) <u> </u>	(S=6)-;	(S=6)-1 5		16	=20)	(5=13)
		(S=II)-4	(S=M) MIDSTONE ATING TO A S=45/SOMM		<b>!</b> " `	=15)	(S=100)*
		(S=50) SILBSTONIE	Lava No Core tisten	5=55 <b>/s</b> own We	ithered X		770VE
		No core taken	No core taken (S=40 (For 150mm)	Delegie M	eta-	= 118)	<b>X</b>
-4	(S=50 for, 25)	Amygdaloidal Leva (Agglomande?) with fourthers		Core Recovery	SILTOTONIE X	Core Reinsung	Core Kerorery 100%
		in ever hater		95%, 100%, 100%,	Madame	270%	
-6		Core Recovery regligible					
	LEGEND		20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
8		▼ Standpipe water level					
	Superficial 图 SILT Deposit	✓ Water Strike level (s=5) Nualise of	**************************************		1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	GEOLOGICAL	SECTION (A-A)
/	Deposit SAND & GRAVEL	Standard Penetration Te  * Extrapolated SPT value	<b>6T</b>				
	STITE CLAY						
Jesse	Shelo Series Shelo Series MODETONE						
Jersen	Volcznic Sevied						FIGURE 3 a
	AMYGDALOIDAL LAVA (BASALT					12289	





Boring Met			Diamete			evel (mOD)			Job Numbe
Fraste PL K	19	11	3mm cas	ed to 8.90m	9	9.60	Regal Construction (Jersey) Ltd		0762
		Locatio	n site plan			01/2007-	Engineer Peter Brett Associates		Sheet 1/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thidkness)	Description		Legend
					99.56	(0.04)	CONCRETE		- Elizabet
					99.40	(0.16)	Hardcore		100
							Very loose to loose brown fine to medium SAND are gravel	nd little	
						(1.80)			
20-1.70	X 0.22			12/01/2007:0.00m					
20-1.65	SPT N=4		DRY	13/01/2007:DRY 2,1/2,,1,1					
70-2.00	X 0.00								
00-2.23	X 0.00				97,60	(0.40)	Soft dark brown sandy SILT		
23-2.50	X 0.76				97.20	2.40	Soft to firm brown slightly sandy SILT		
50-2.95 50-3.50	SPT N=10 X 0.53	1.90	DRY	2,2/3,2,2,3		(0.60)	Social irin brown signey sandy SiLi		
					96.60	3.00			
					30.00	- 3.00	Soft to firm blue grey slightly sandy CLAY/SILT		-
50-4.00	SPT N=3 X 0.50	3.40 4.00	DRY	1/,1,2					
.00-4.40 .00-5.00	U 0.40 X 0.55	4.31	2.83	12 blows					
						(3.30)			
.00-5.45	SPT N=5	4.31	3.95	1,1/1,1,2,1					
00-6.00	X 0.50	5.92	5.05	1,111,11,2,1					
					E	-			
					1				
.00-6.50	X 0.74				Ē				-
					93.30	6.30			
.50-6.95	SPT N=36	6.20	3.06	1,2/5,9,10,12			Dense blue grey very clayey fine to coarse GRAVE	L	**
.50-7.12	X 0.62	6.75			Ė				-
12-7.67	X 0.00				THAT	(1.50)			
					1				
					E				
67-7.75 75-7.76 76-7.80	X 0.00 X 0.00 X 0.60	7.30		13/01/2007:3.27m	91.80	7.80	Very dense brown clayey sandy fine to medium GR	AVEI	
temarks						-	, vener oroni objej salvy lile to ingula GR		100
xploratory h ry drilling fr	cavated by hand from note drilled using the om 1.20m - 9.13m	Fraste PI I	Rig					(approx)	Logged By
ock core dr 70 drilling fi	illing with water flush rom 4.00m - 4.40m -	12 blow or	m - 10.23 ounts	7m				1:40	MRW
round level	s are not Ordnance I	Datum						Figure N	lo. 2.BH1

AIV	B & Brose	a Campor N	naid Pater	stri 13 44	, <b>.</b>	pecialists			Kensington Gate Car Park, St Helier, Jersey	E
Boring Met Fraste PL R			i	Diamete 3mm cas	r ed to 8.90m	Ground i	Level ( 99 60	mOD)	Client Regal Construction (Jersey) Ltd	Jo N:
			Locatio	n site plan		Dates 12/ 15/	/01/200 /01/200	)7- )7	Engineer Peter Brett Associates	Si
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mQD)	Dei (n (Thick	pth n) (ness)	Description	Leg
7.80-8.22 7.80-8.25	X 0.00 SPT N=	52	7.80	4.90	3,4/7,15,12,16			(0.50)	Stratum as above	
3.22-8.33 3.33-8.38 3.38-9.13	X 0.11 X 0.50 X 0.75		8.00 8.11 8.90			91.30	 	8.30 (0.80)	Soft to firm brown sandy StLT	
	TCR	SCR	RQD	 		90.50		9.10		
l.11 l.13 • • • • ·	100	90	âū	6	tere tra _{nd} an	90.50		. 8.10	Moderately strong grey slightly weathered ANDESITE, iron-stained joints	
l. <b>79</b>					1,0,0,0 + 1,114.		- - - - -	(1.17)		
	100	75	25	10		20.00	<u> </u>			+ + + + + + + + + + + + + + + + + + +
0.27				   	15/01/2007:3.21m	89.33		10.27	0	-
٠٠.							[  -  -		Consplete at 10,27m	
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Remarks							******		Scale (approx	t) E
		7 4 4 7 44		1	Marie Company			· · · · · ·		



Boring Meth	hod	,	Ground I	evel (mOD)	Client		Job		
Fraste PL Ri	9	11:	3mm cas	ed to 8.30m	9	9.40	Regal Construction (Jersey) Ltd		Number 0762
		Location	n site plan		Dates 16/ 18/	01/2007- 01/2007	Engineer Peter Brett Associates		Sheet 1/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	instr
					99.30	(0.10) 0.10 (0.90)	CONCRETE  Layers of concrete and sand	10000	
0.80-1.20	X 0.35				98.40	1.00			
1.20-2.00	X 0.57						CONCRETE		200
.00-2.73	X 0.73					(2.80)			
2.73-3.67	X 0.30			16/01/2007 17/01/2007:2.24m					
1.67-3.82 1.82-4.27 1.82-4.73	X 0.10 SPT N=0 X 0.38		2.00	r	95.60	3.80	Very soft to firm grey/brown slightly sandy CLAY with a little fine gravel		
.73-5.00	X 0.45								
.00-5.45 .00-6.00	SPT N=5 X 0.52	4.80	2.00	1/_2,3		(3.00)			
00-6.45 00-6.60	SPT N=11 X 0.52	4.80 6.42	2.14	1,1/2,2,3,4					
.60-7.00	X 0.50				92.60	6.80			
00-7.45 00-7.35	SPT N=31 X 0.35	6.42 7.25	3.06	3,44,7,10,10			Firm to stiff orange/brown sandy CLAY with a little fine to medium gravel		
35-7.62 62-6.13	X 0.27 X 0.00								
Remarks tarter pit ex- xoloratory h	cavated by hand from	n ground le	evel to 1.	20m bgl				Scale (approx)	Logged By
ry drilling fro	cavated by hand from ole drilled using a From 3.82m - 9.24m illing with water flush excometer with tip insi-	from 0.80	m - 3.82r	m, 9.24m - 10.47m				1:40	MRF
andpipe pie round levels	ezometer with tip insi s are not Ordnance I	talled at 10 Datum	0.40m bg					Figure N	

Boring N Fraste Pl		-q		i	Diameter 3nım cası	ed to 8.30m	Ground t	L <b>eve</b> l 99 40		Client Regal Construction (Jersey) Ltd		i N	ab umb: 076:
				Location as	n site plan		Dates 16/ 18/	/01/20 /01/20	)07- )07	Engineer Peter Brett Associates		S	heet 2/2
Depth (m)		Sample	/ Tests	Casing Depth (m)	Water Depth (m)	field Records	Level (mOD)	D _i (Thic	epth (m) :kness)	Description	Legen	Water	ins
8.13-8.60	3	X 0.00		8.30		17/01/2007 18/01/2007:2.90m							
8.63-9.00	3	X 0.23				· ·			(2,40)	· · · · · · · · · · · · · · · · · · ·			3.1
9.00-9.24 9.00-9.3	4	X 0.40 CPT 80/	155 SCR	8.30 RQD	2.23 FI	2,3/5,25,,50	50.00	}_ 		Stratum as above		:	
9.24	٠. إ	TCR 15	0	KUD			90.20		9,20	Moderately weak grey slightly weathered ANDESITE, very closely jointed	*****		
9.50		100	0					 - -		to the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of			
9.66		100	0						(1.27)			<u> </u>	
9.93		100	10	0	10+			<u></u>					
10.47	.			<u> </u>	ļ 	18/01/2007.2.99m	88.93	-	10.47		******		TA.
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Installation			Dimensi	_TD For	Specialis	10	_	Kensingtor	0010 0	on rone, s	A TTOWN,	Josey		_	BH2
Standpipe		er						Client Regal Con	struction	(Jersey)	Ltd				lob Number 0762
			Location as site		Ground t	evel (m/ 9.40		ngineer Peter Brett	Associa	tes					Sheet 1/1
egend 🖁	Instr (A)	Level (mOD)	Depth (m)	Description				Gr	oundwa	ter Strik	s Durin	g Dritting			
					Date	Time	Depth Struck (m)	Casing Depth (m)	Inflo	w Rate	5 min	Read 10 min	Ings 15 min	20 min	Depth Seale (m)
		98.20	1.20	Bentonite Seal			(14)								0
								Gre	oundwat	er Obser	vations	During D	rilling		
							_	Start of St	_				nd of Si		
					Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Wate Leve (mOD
					16/01/07 17/01/07 16/01/07	am am am	2.73 8.13	8.30	2.24 2.90	97.16 96.50	pm pm pm	2.73 8.13 10.47	7.25 8.30	2.99	96.4
							-	Instru	ment Gr	roundwa	ter Obse	rvations			
				Gravel Filter	Inst.	A] Type	: Stand	pipe Piezor	meter						
						Inst	trument	[A]							
		-			Date	Time	Depth (m)	Level (mOD)				Remi	irics		
					18/01/07 06/02/07	14:42	3.07 2.64	96.33 96.76							
		89.20 89.00	10.20	Piezometer Tip											



Boring Meth Fraste PL Ri			Diameter	r ed to 9.21m	Lot come of	evel (mOD)	Client Regal Construction (Jersey) Ltd	Job Numb	13 ber
	•	Locatio			Dates		Engineer	Sheet	
		1	site plan		08/	01/2007- 01/2007	Peter Brett Associates	1/2	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legen	d
					100.03	(0.07)	CONCRETE	1000	
							Loose light brown fine to medium SAND		
						(4.42)			
						(1.43)			
.20-1.50	X 0.00								
1.50-1.60 1.60-1.67	X 0.00 X 0.47	1.65	DRY		98.60	1.50	Very soft red brown sandy SILT becoming firm with depth	100	
1.67-2.12 1.67-2.30	SPT N=11 X 0.00	1.65	1.46	2,2/2,3,3,3					
2.30-2.50	X 0.52			08/01/2007:1.46m					
2.50-2.92 2.50-2.95	X 0.15 SPT N=10	2.85 1.65	DRY	09/01/2007:DRY 1,2/2,3,3,2					
2.92-3.50	X 0.32								
3.50-3.95 3.50-4.50	SPT N=0 X 0.90	2.85	2.00	1/ .					
						(5.50)			
4.50-4.95	SPT N=11	4.40	2.22	1,1/2,3,3,3		(0.50)			
4.50-5.50	X 0.50	1.40	-44	1, 112,0,0,0					
	-								
5.50-5.95 5.50-6.10	SPT N=13 X 0.60	4.40 5.83	2.85	1,1/2,3,4,4					
3.10-6.50	X 0.40			09/01/2007:GLm					
6.50-6.90	U 0.28			11/01/2007:1.37m					
5.50-7.14	X 0.57								
7.14-7.50	X 0.00				93.10	7.00	Dense grey and brown clayey very sandy fine to coarse GRAVEL with occasional cobbles	200	
							GRAVEL with occasional cobbles	1307	
7.50-7.52 7.52-7.67 7.67-7.87	X 0.00 X 0.00 X 0.00	7.30				(1.50)			
7.87-7.93	X 0.00					(1.50)			
Remarks Starter pit ex Exploratory h	cavated by hand from	m ground i	level to 1.	20m bgl			Scale (approx	Logge	ıd
Dry drilling for Rock core dr	cavated by hand from hole drilled using a Fi orn 1.20m - 9.42m, 5 filling with water flush from 6.50m - 6.90m	9.64m - 9.6 n from 9.42	9m 2m - 9.64	m, 9.69m - 10.97m			1:40	MFW	
uro aniling n	is are not Ordnance						Figure	No.	

Boring Me	thod		Casing	Diameter	-	Ground l	.evel (mOD)	Client	Job
Fraste PL			i		ed to 9 21m	8	00.10	Regal Construction (Jersey) Ltd	Nun 0
			Locatio	n site plan	W1374444	Dates 06/ 12/	01/2007- 01/2007	Engineer Peter Brett Associates	She
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Lege
7.93-8.33	X 0.00		8.10				(1.50)		
8.33-8.46 8.46-9.26 8.46-8.91	X 0.50 X 1.20 CPT N	-48 · · · ·	9.21 8.10	3.22	4,7/7,13,14,16	91.60	8.50	Stratum as above  Firm to stiff brown sandy SILT with occasional grey fine to	
	0.7.1.	<b>"</b>	0.10	G.24	44.77.44			Firm to stiff brown sandy SILT with occasional grey fine to medium gravel	
9 42-9 64	X D OR		  -  -  -			. 1	(1.10)		
9.42-9.64 9.28-9.40 9.40-9.42 9.64-9.69	X 0.00 X 0.00 X 0.12	SCR	RQD	FI	11/01/2007:3.07m	90,50	- - - - 9.60		
9.69	1		1		12/01/2007;2.14m X 0.27	30.00		Moderately strong tight grey slightly weathered ANDESITE , iron stained planar discontinuities	
		i   			· · · · ·				
	95	90	75	5			<u>(1,37)</u>		
					12/01/2007:3.40m	89.13	- 10.07		
10.97					12/01/2507.5.46/4	00.13	10.97 	Complete at 10,97m	
								Compete at 10.37%	
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Damaeka	1	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>			
Remarks		***		`. · · · · .				Scale (approx)	Log By
					`				!

G≡	OMARINE				La Por St Sav JE2 7h	arine (Jer te, Rue D four, Jers HT geomarine	u Pont 54303	Borehole N  1  Sheet 1 of
Projec	ct Name			Р	roject N			Hole Type
(ensi	ngton Place				49		Co-ords: -	WLS
ocati	ion: Kensin	gton Pl	ace					Scale
							Level: -	1:50
Client:			uction (Jersey)	) Limited	i		Dates: 21/07/2009	Logged B
	fikes Depth (m)	Type	Situ Testing Results	Depth (m)	(m AOD)	Legend	Stratum Description	
	0.00-0.55	D					Brown very gravelly soily fine to medium grained to coarse, sub-angular. Occasional cobbles. Slight hydrocarbon smell. (MADE GROUND)	SAND. Gravel is fine
	0.55-0.81	D		0.55			Brown soily gravelly fine to medium grained SAN	D. Gravel is fine to
4	0.81-0.98	D		0.81		30.00	coarse , sub-angular. Layer of pale brown/ white sand. (MADE GROUP	
100	0.98-1.16	D		0.98		100		
	1.16-1.40	D		1.16			Brown soily gravelly fine to medium grained SAN coarse, sub-angular. Layer of pale brown/ white sand, (MADE GROUN)	(D)
						====	Light brown gravelly fine to medium grained SAN coarse.	ID. Gravel is fine to
	0.62 5/20						Increased sand content. (MADE GROUND)	
	1.40-2.90	D					Pale brown/white slightly gravelly fine to medium is fine to coarse, sub-rounded. Coarse cobbles p	grained SAND. Gravel / resent. (MADE GROUND)
							Greyf tan sandy CLAY. Strong hydrocarbon sme Sand is fine grained with angular fine to coars occasional brick fragments at 1.40m.	II. (HEAD DEPOSITS)
	2.90-4.40	D		2.90			Grey CLAY. Contains calcareous shells. Strong hydrocarbon smell. (HEAD DEPOSITS) Sub-angular coarse gravel fragments at 2.90r	n.
	4.40-5.90	D		4,40			Grey slightly sandy CLAY. Rare gravel fragments sub-angular. Hydrocarbon smell. (HEAD DEPOS	s. fine to coarse, NTS)
				5.90			Tan slightly sandy gravelly CLAY. Gravel is fine to	
	5.90-6.70	D					sub-angular. (HEAD DEPOSITS)	o coase,
				6.70			Reddish colour, highly gravelly at 6.60m.	
							End of Borehole at 6.80 m	1
	s: Slotted w	Type	Results				lain well from 1.80m to ground level w	

Remarks: Slotted well from 6.80m to 1.80m with gravel pack. Plain well from 1.80m to ground level with bentonity surround. Well cover flush at surface.

AGS

	Name toл Place	~~	.,	- 7	roject N 49	eomarine lo.	e Sheet 1 c	уp
cation		gton P	lace	l			Level: - Scale 1:50	e 
ent:	Regal	Constr	uction (Jersey) I	imited	 		Dates: 17/07/2009 Logged	
Wate	er Sampl	es & In	Situ Testing	Depth	Lavel		NH NH	
Strike	95 Depth (m)	Туре	Results	(m)	(m AOO)	Legend	Stratum Description	
	0.00-1,40	D					Dark brown very gravelly ctayey fine grained SAND. Frequent cobbles. Gravels are fine to coarse, sub-angular, cohesive. Brick fragments and rootlets present. (MADE GROUND)  Clay texture at 0.40m	
							Tan/ brown CLAY at 0.80m	
	4-11-100-11-11-11-11-11-11-11-11-11-11-11			1.40			Grey slightly gravelly CLAY. Gravel is fine to coarse. Hydrocarbon smells. (HEAD DEPOSiTS)	
	1.40-2.90	. و		٠				
				2,90			Yellow/ tan slightly gravetry CLAY. Gravel is fine to coarse, sub-rounded. Slightly stained from hydorcarbon. (HEAD DEPOSITS)  No recovery from 2.90- 5.90m	<del>-</del> .
							No recovery from 2.90- 5.90m	٠.
	5.90-6,80	D		• •			I magazina ang panggan ang Mitting ang military ang military ang military ang military ang military ang militar Military ang military ang military ang military ang military ang military ang military ang military ang military Military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang m	
				6.80	3-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1		Reddish slightly sandy gravelly CLAY from 6.65- 6.80m	
	6.80-7.30	D.			·		End of Bosehole at 7.40 m	
			T TO THE TOTAL THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF		. !			
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			1 + 1 1 + 1 1 + 1	3				

surround. Well cover flush at surface.

GEO	MARINE				La Por St Savi JE2 7H	irine (Jers te, Rue D our, Jers iT eomarine	u Pont S 4305	Borehole N 3 Sheet 1 of
Project N	lame			P	roject N			Hole Type
Kensingt	on Place			7-	49		Co-ords: -	WLS
_ocation:	Kensin	gton Pla	ce				Level: -	Scale 1:50
Client:			ction (Jersey				Dates: 19/07/2009-20/07/2009	Logged By NH
ell Water Strikes	Depth (m)	Type Type	itu Testing Results	Depth (m)	(m AOD)	Legend	Stratum Description	
	0.00-0.51	D		0.51			Brown very gravelly fine to medium grained SAND, Gra- coarse, sub-angular. Contains sile fragments, granite (MADE GROUND)	wel is fine to and cobbles.
	0.51-0.89	D		0.89			Brown very gravelly clayey fine to medium grained SAN to coarse, sub-angular. Contains tile fragments, (MADE	D. Gravel is fine ! GORUND)
	0.89-1.36	D					Brown very Gravelly fine to medium clayey SAND. Gravel is fine to coarse, sub-angular. (HEAD DEPOSIT	S)
	1.36-2.80	D		1.38			Tan slightly Sandy CLAY. Contains tiny calcareous she fine. (HEAD DEPOSITS)	ills. Gravel is
	2.80-4.70	2.80 2.80 D 8.45		Tan/ grey CLAY. Occasional fine gravel. (HEAD DEPO	SITS)			
	6.25-6.45 6.45-7.25						Red/ brown very gravelly fine to medium grained SAND. coarse, sub-angular. (HEAD DEPOSITS) Tan very gravelly SAND/ CLAY at 6,45m Gravel is fine to medium, sub- rounded.	Gravel is fine to
				1.63			End of Borehole at 7.25 m	
				*				
	-	Type	Regulto	1				

GEON	MARINE				La Por St Savi JE2 7h	arine (Jers te, Rue Di lour, Jerse IT eomarine.	S 4306	Borehole N 4 Sheet 1 of
Project N	ame			P	roject N			Hole Type
Kensingto	on Place			7.	49		Co-ords: -	WLS
ocation:	Kensin	gton P	Place				Level: -	Scale 1:50
Client:	Regal	Constr	uction (Jersey)	Limited			Dates: 20/07/2009	Logged By NH
Mater Strikes	Sampl Depth (m)			Depth (m)	Level (m AOD)	Legend	Stratum Description	n
	0.00-0.65	D	(Victoria)	0.65			Brown soily very gravelly medium grained SAND Gravel is fine to coarse, sub-angular, cobbles, ( Brown very gravelly fine to medium grained SAN	D. Occasional rooflets. (MADE GROUND)
	0.79-1.43	D		0.79			fragments. Gravel is fine to coarse, sub-angula Brown very gravelly fine to medium grained SAN Gravel is fine to coarse, sub-angular. Concrete	r. (MADE GROUND)
	1.43-2.90	D	Type Results (m) (m AOD) C  D  D  0.65 0.79  D  1.43		GROUND) Tan sandy CLAY. Hydrocarbon smell. (HEAD C Brown very gravelly SAND at 1.55m	sular. Concrete powder observed. (MADI smell. (HEAD DEPOSITS) 1.55m		
	2.90-4.40	D					Brown/ grey very slightly sandy CLAY. Rare ang hydrocarbon smell, dark grey lines running through the sand sand sand sand sand sand sand sand	igh. (HEAD DEPOSITS)
	4.40-5.90	D					Brown/ grey CLAY. Rare fine gravel. Hydrocarb	on smell (MADE GROUN
	5.90-6.35	D					Brown gravelly CLAY. Gravel is fine to medium, GROUND) Reddish very gravelly SAND at 6.30m  End of Borehole at 6.55 m	sub-angular, (MADE
		Тура	Results					F

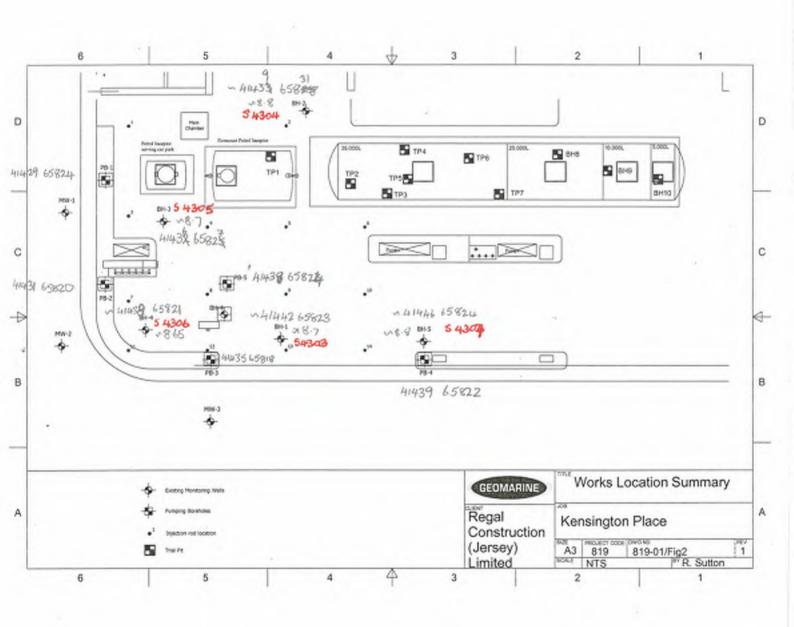
Remarks: Slotted well from 6.55m to 2.00m with gravel pack. Plain well from 2.00m to ground level with bentonite surround. Well cover flush at surface.



1	EON	ARINE	•				te, Rue Di our, Jerse		Borehole I
-	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	Service Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the C				JE2 7H		5 40-7	Sheet 1 of
ro	ject Na	ame			Р	roject N	with an indicated published		Hole Typ
		n Place			100	49	711	Co-ords: -	WLS
oc	ation:	Kensin	gton P	lace					Scale
								Level: -	1:50
'Ea	nt:	Pagal	Conote	votice ( lessev)		,		5.1	Logged B
alle	TH.			uction (Jersey)	Limited			Dates: 16/07/2009	NH
I	Water Strikes	Depth (m)	es & In	Situ Testing Results	Depth (m)	Level (m AOD)	Legend	Stratum Description	
		0.00-0.50	D					Dark brown gravelly clayey fine grained SAND. Grav sub-angular. Cobbles, brick fragments and rootlets.	el. fine to coarse. (MADE GROUND)
					0.50			Tan fine to medium grained SAND. (MADE GROUN	D)
					0.80		12.55	Dark brown gravelly clayey SAND. Gravel, fine to co	arse.
		0.95-1.25	D		1.40			sub-angular. Occasional cobbles, brick fragments as Interbedded tan sand. (MADE GROUND)	nd rootlets.
					1.00		35.55	Dark brown gravelty clayey fine grained SAND. Gravel is fine to coarse, sub-rounded. (HEAD DEPO	SITS
							20.25	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
		1.40-2.90	D						
							32-85/1		
							200		
		2.90-3.10	D		2.90		10000	Dark brown clayey fine grained SAND. (HEAD DEPC	NOTED V
		2.0.10			3,10		77.75	Grey very slightly gravelly CLAY. Fine gravel, sub-ro	
								hydrocarbon smell. (HEAD DEPOSITS) Black/ grey clayey SAND at 3.10m	oroco. Fami
								Hydrocarbon smell. Layer of black hydrocarbon- stained CLAY at 3.30	
		3.10-4.60	D			1		Early of State Hydrocardon Statistic CEAT 813.30	JITI J
							3.5		
ı							拉記		
					4.60		77	Greyl brown slightly gravelly CLAY. Fine gravel, sub-	rounded, cohesive.
							TE	(HEAD DEPOSITS)  No recovery at 4.60m to 6.10m	
							THE R		
							목됩		
							13.5		
						1			
1							목됩		
		6.10-6.90	D				1		
					6.80			Reddish/ brown very gravelly clayey fine grained SAN	D. Ground in fina
		6.90-7.50	D		0.80			to medium, sub-angular. (HEAD DEPOSITS)	/
		VIII-1190			7.50			Brown/ grey very gravelly fine to medium grained SAN to coarse, sub-angular, Rare cobbles present, Faint (HEAD DEPOSITS)	ID. Gravel is fine hydrocarbon smell.
						-	EE.	Grey brown slightly gravelly CLAY. Gravel is fine to	coarse,
		7.50-8.40	D			1		sub-angular. Rare cobbles present. Hydrocarbon sm Very gravelly CLAY at 7.50m	ell. (HEAD DEPOSIT:
					8.40		TEN.	End of Bovehole at 8.40 m	
								CHU U COMPOR IX 0.40 M	
1			Type	Results					
w	ovivo:	No inetall-	ation (	Backfill to surfa	100				

Remarks: No installation. Backfill to surface.





115mm cased to 7.00m	Boring Meth	IPLU:	,	Diamete		Specialist:	Level (mOD)	66-72 Esplanade, St Helier Client			BH1
Depth   Sample   Tests   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canada	Inspection pi	it to 0.90m	1			o.ou.io	as res (silve)			No	umber
1,00-1,00			-		plan	21	/03/2014- /03/2014			Job Num 15 She	
MADE GROUND - Convented   Mapper   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Conve	Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water	Instr
Remarks ispection pit excavated by hand on 21.03.14 to 0.9m, dry and stable, backfilled before drilling light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bo	0.00-1.00 1.00-2.00 2.00-3.00 3.00-4.00 4.00-5.00 5.00-6.00	X 0.75  X 0.78  X 1.00  X 1.00	1.00 2.00 3.00 4.00 5.00 7.00	DRY DRY DRY	28/03/2014:3.75m		0.10 (8.158) (0.30) (0.30) (0.30) (0.30) (0.30) (0.30) (0.30) (0.30) (1.10) (1.00) (1.00) (1.00) (1.00)	MADE GROUND - Sity sand MADE GROUND - Gravel (Hoggin) Sity brown CLAY Light yellow SAND Brown CLAY with fine to medium gravel  Light brown sity SAND with fine to medium gravel  Light brown Sity SAND  Brown sandy SILT  Yellow brown sandy SILT  Light brown sity sandy CLAY with fine to medium gravels		A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PAR	
spection pit excavated by hand on 21.03.14 to 0.9m, dry and stable, backfilled before drilling Vindow sampling from 1.20 - 7.00m	Domeste										
1:50 MFW	Remarks Inspection pit Window same	t excavated by hand pling from 1.20 - 7.0	on 21.03.	14 to 0.9	m, dry and stable, bed	ckfilled befo	ore drilling		Scale (approx)	B)	gged
		F-19 11311 120 - 170							1:50		MFW

	MP	LU			ation & Ge Specialis		ical	Site 66-72 Esp	olanadę,	St Helier					Borehol Number BH1
Installat Single l	tion Type Installation		Dimensi Intern	ions al Diameter of Tube [A] = 50 n	ทยา			Client Dandara	Jersey Lt	(ci					Job Number 1503
			Location as per	r site plan	Ground	Levei (m	OD)	<b>Engineer</b> Dandara							Sheet 1/1
egend	ਜ਼ੇ ਗਿstr ⊗ (A)	Level (mOD)	Depth (ni)	Description					roundw	ater Strik	es Durin	a Drittin	a		***************************************
Tall.	<u> </u>	(ISIOD)	(111)		<u>!</u>			7	i		<u> </u>		dings		~
				Cement/Bentonite Grout	Date	Time	Depth Struck (m)	Casing Depth (In)	Inflo	w Rate	5 min		15 min	20 min	Depth Seale (m)
			0.70												
			4.00	Gravel Filter						*.					· .
			1.00											***************************************	
						<u>:</u>	<u>!</u>	Gr	กมาสพล	ter Obse	rvations	During f	) Villina	<u> </u>	<u></u>
			٠.								1				
					Date	Time	Depti Hole	Start of S Casing Deptil		Water Level (mOD)	Time	Depth Hole (m)	End of Si Casing Depth (m)		Water Level (mOD
					27/03/14 28/03/14			5,00	(m) 3.75	(mOD)	17.00 17.00	5.00	5.00 7.00	(m) DRY 3.90	(mOD)
					Longon	05.00		0.00			17,55	7.50	7.50	0.80	
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										roundwa	ter Obse	rvations	v. v-1		
				Slotted Standpipe	înst.			d Standpip	e						
		.		Olones Standarps	Date	Ins	trumen	! [A] 			•. • • •	Rein	arks	•	
						Time	Depti (m)	Level (mOD)							
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Remarks	5. ^{11.}					. * * • • • • • •			. •	****					
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Source No: 4803

	Inspection pi	t to 1.20m	-	Diamete 3mm cas	r ed to 6.18m	Ground	Level (mOD)	Client Dandara Jersey Ltd	Job Number 1503
0.00-1.13	Praste PL Ri		TAGE OF		plan	21			Sheet 1/2
0.00-1.13	Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (rh)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend
1.13-1.28	0.00-1.13	X 0.50					E (6°15)	MADE GROUND - Concrete	
1.15.1-28							E '0.25		1923
1.05-1.90				1.2			(0.95)	Clayey gravelly SAND with cobble sized stones becoming light yellow sand	
1.05-3.06	1.13-1.28	X 0.40	1.18		-		1.20	Lanca and Lanca CAMB and Security	
1.90-3.05		101717					E	Loose yellow and brown SAND with line gravel	
1.05-3.50	1.55-1.90	X 0.00					(0.70)		
1.05-3.50 SPT N=2 2.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.05-3.51 X 0.10 3.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-5.04 X 0.41 5.04 Substitute (1.58) Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft	1.90-3.05	X 0.20					1.90	Loose brown fine SAND	120022 120022
1.05-3.50 SPT N=2 2.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.05-3.51 X 0.10 3.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-5.04 X 0.41 5.04 Substitute (1.58) Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft					-		Ē		1000
3.05-3.51 X 0.10 X 0.95	-				-		(1.15)		
1.05-3.51							E		
1.05-3.51   X 0.10   X 0.95   X 0.53   X 0.53   X 0.53   X 0.53   X 0.54   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41	0.05-3.50	SPT N=2	2.16	DRY	0.0/0.0.1.1		3.05	Non-ord house and OH V	200
1.10-4.63						-		very sort brown sandy SIL1	
.10-4.63	.51-4.10	X 0.95	-				-		
83-5.08   SPT N=5   X 0.41   S.04   St.   0.1/1.0.2.2   Soft brown and grey sandy SILT	1						(1.58)		(VE)
83-5.08   SPT N=5   X 0.41   S.04   St.   0.1/1.0.2.2   Soft brown and grey sandy SILT									883 -
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	1.10-4.63	X 0.53	4.16				Ē	- 1	333
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	22 5 00	ODT N. S		~			4.63		323
1.04-6.28			5.04	GL	0,1/1,0,2,2	*	=	Soft brown and grey sandy SILI	
1.58-6.96	i.04-5.28	X 0.22					(0.66)		
98-8.41 SPT N=33	.28-5.58	X 0.30					5.28	Soft brown sandy CLAY	
1,986-8,41 SPT N=33	5.58-5.96	X 0.38					(0.68)		
1.386-8.41 SPT N=33 SPT N=33 SPT N=33 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 S							5.96		
1.82-6.95	i.96-6.41 i.96-6.43		6.18		2,5/6,8,9,10		E		
1.92-6.95	.43-6.65	X 0.22			-		E		
95-7.24	.65-6.92	X 0.00					Ė		
33-7-57 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.8			0.00		02/04/2014/24/2		h	14	3.2
337-57   X 0.00   7.88   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0			0.00				Ē.		
1.28-8.94	.33-7.78	SPT N=26		2.35	5,3/6,7,7,6		Ē.		
1.28-8.94	.57-7.68	X 0.00	1.00				7.78	Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination o	200
1.94-9.39 SPT N=14 (.94-9.38 X 0.00 Stiff grey sandy CLAY Siff grey sandy CLAY (0.77) Stiff grey sandy CLAY (0.77) Seale (approx) By drilling from GL to 10.46m								Firm brown sandy sity CLAY with little firm to medium gravel	
1.94-9.39 SPT N=14	28-8.94	X 0.66	8.68				E		
94-9.39 SPT N=14		V-S-MI					(1.62)		
.94-9.38	*						- (1.02)		
.38-9.63 X 0.65 9.18 9.40 Stiff grey sandy CLAY .63-9.85 X 0.22 .85-10.17 X 0.32 (0.77)  Remarks rey drilling from GL to 10.46m  Scale (approx) By					4,3/2,3,4,5		E		
.63-9.85 X 0.22 (0.77)  Remarks respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling rry drilling from GL to 10.46m			0.40				0.40		
.85-10.17 X 0.32 (0.77)  Remarks specifion pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the f			9.18				9.40	Stiff grey sandy CLAY	2
Remarks respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling rry drilling from GL to 10.46m							(0.77)		
respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling larger GL to 10.46m By		A V.36					<u> </u>		
they coming of 11.50 M	repection pit by drilling fro	om GL to 10.46m	on 21.03	.14 dry 8	stable, backfilled bef	ore drilling		Scale (approx)	Logged By

oring Methorspection pit raste PL Rig	to 1.20m	1	Diamete 3mm ças	r ed to 6.18m	Ground	Levo	i (mOD)	Client Danidara Jersey Ltd	Job Num 15(	ber
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Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	(Th	Depth (m) Ickness)	. Description	Legen	id j
0.17-10.46	X 0.29						10.17	as previous		
ĺ		:					(0.29) 10.46	Stiff grey CLAY with fragments of rock		
0.46-10.53 0.53-10.90	C 0.00 C 0.45							Weak grey slightly weathered Jersey Shale Formation with fron stained close bedding (no solid core recovery)		
0.90-11,55	C 0.65					E	(1.09)			
						<u> </u>	()			
			 	04/04/7054/4 4400		=	11.55			
*				04/04/2014;1.44m		=		Complete at 11.55m		
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temarks	excavated to 1.20m	on 21 03	.14 dru 8	stable, hackfilleri hefe	ore driffing	F	·	Scale (approx)	Logg By	jed
y drilling fro	m Gi. to 10.46m	antie 1700	⊬ i⊸ mily o	stable, backfilled befo	nie miniti			(approx)	By-	
Mark Politics	עניוו טו								;	

Insta	llatio	п Туре		Dimensi	ons				Client			····				BH2
						·			Dandara .	Jersey Lte	d 	<del> </del>		·····	<u>}</u>	Number 1503
				Location as per	t site plan	Ground	Level (m		Engineer Dandara							Sheet 1/3
egen	y y	instr (A)	Level (mOD)	Depth (m)	Description				G	roundwa	nter Strik	es Durin	g Drillin	9		
						Date	Time	Depth Struck (m)	Casing Depth (m)	inflo	w Rate	5 min		dings 15 min	20 min	Depth Seale (m)
											* * * .					-
300 F															-	
									Gr	oundwai	er Obse	vations	Burina D	) rilling	·	-
																/4.1
						Date			Start of S	,,	,			End of S		
						Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
						03/04/14 04/04/14	08.00		6.18	1.95		17.00 17.00	6.95 11.55	6.18 9.18	2.40	(1100)
						04/04/14	04.00	0.00	0.10	1.50		17.00	11.00	9.16	1.44	
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									Instr	ument Gr	oundwa	ter Obse	rvations			
						Inst.	[А] Туре	:					**************************************	^^!!-		
	}		j				ins	trument	[A]							
			ļ			Date			T				Rem	arks		
_	30000		vinope suc.				Time	Depth (m)	Level (mOD)							
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AMPLUS I Borehole Foundation & Geotechnical Number Specialists 66-72 Esplanade, St Heller ВН3 Casing Diameter Ground Level (mOD) Client Job Number Inspection pit to 1.20m Competitor Rig 115mm cased to 7.00m Dandara Jersey Ltd 1503 Dates Location Engineer Sheet 25/03/2014-26/03/2014 as per site plan Dandara 171 Casing Depth (rh) Water Depth (m) Depth (m) (Thickness) Depth (m) Water (mOD) Sample / Tests Field Records Description Legend Instr 0.00-1.00 WS 0.17 1.00 (8,13) MADE GROUND - Concrete (0.32)MADE GROUND - Gravel, metal sheet 0.45 (0.25) 0.70 (0.20) 0.90 MADE GROUND - Dark grey gravelly sit Light grey silty CLAY Light yellow SAND 1.00-1.45 1.00 1.00-2.00 SPT N=23 (0.30)DRY 1.3/4.5.6.8 1.20 Stiff brown sandy CLAY with fine to medium gravels WS 1.00 2.00 (0.80)2.00 2.00-2.45 2.00 2.00-2.70 SPT N=68 DRY 8,9/12,17,17,22 Dense light brown fine to coarse SAND with fine to medium gravels WS 1.00 2.70 (1.45)WS 0.30 2.70-3.00 3.00 3.00-3.45 SPT N=31 2.85 8,12/10,8,7,6 3.00 WS 1.00 4.00 Firm brown and grey sandy SILT (0.55)4.00 4.00-4.45 4.00 4.00-4.70 SPT N=2 3.84 0,0/0,0,0,2 Soft brown sandy clayey SILT WS 1.00 4.70 (1.00)WS .30 4.70-5.00 5.00 5.00 5.00-5.45 SPT N=12 4.92 1.2/2.2.4.4 Firm brown sandy SILT 5.00 5.00-5.72 WS 1.00 5.72 (1.00)5.72-6.00 WS 0.20 6.00 6.00 SPT N=24 6.00-6.45 WET 2,1/3,5,6,10 Medium dense to dense brown clayey sandy fine to 6.00 6.00-6.63 coarse GRAVEL WS 1.00 6.63 6.63-7.00 WS 0.31 7.00 25/03/2014:5.12m (1.50)26/03/2014:4.57m 13,11/12,18,19,19 SPT N=68 7.00-7.45 5.05 7.00 7.00-7.50 WS 0.35 7.50 26/03/2014:2.23m Complete at 7.50m Scale (approx) Logged Inspection pit excavated on 21.03.14 from GL to 1.2m, dry & stable, backfilled before drilling Window sampling 1.2 - 7.50m Hole unable to be extended below 7.50m because of dense ground Slotted pipe installed, response zone 7.00-1.00mbgl 1:50 MEW Figure No. 1503.BH3

ΑN	/P	LU	SI	Founda	ation & Ge Specialis		cal	<b>Site</b> 66-72 Esp	olanade,	St i felier					Borehole Number BH3
Installati Single In	ion Type nstallation		Dimens Intern	ions al Diameter of Tube [A] = 50 r	ຕກາ			Client Dandara	Jersey Et	d			***************************************		Job Number 1503
			Location	1	Ground	Level (m	(00)	Engineer							Sheet
			as pe	r site plan				Dandara							1/3
Legend	हिंह (A)	Level (mOD)	Depth (m)	Description				G	iroundw	ater Strik	es Durin	g Drilling	3		
ैं <u>दि</u> ष्टे इड्डाइड					Date	Time	Depth Struc	Casing Depth	Inflo	w Rate		Read		1	Depth Sealed (m)
				Cement/Bentonite Grout		······································	(m)	(m)	<u> </u>	<del> </del>	5 min	10 min	15 min	20 min	(m)
			0.70	Gravel Filter				1		•.••					
			1,00				-						 		
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								Ģr	oundwa	ter Obse	rvations	During C	rilling		
i dela (					ļ			Start of S	hift		T		End of SI	 aift	
					Date		Depti		,	Water	ļ	,			Water
			٠.		<u> </u>	Time	Depti Hole (m)	Casing Depth (m)	Water Depth (ni)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
		·			25/03/14 26/03/14	07.30		6.63	4,57		17.00 17.00	6.63	6.63 7.00	5.12 2.23	
					20.00(1)	01,44		1 3.00	1,07		17.00	1.04.	1.00	2.10	٠.
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								Instr	ument G	roundwa	iter Obse	rvations			
				Slotted Standpipe							····				
					inst.	[A] Type	: Slotte	d Standpip	e	<i>-</i>					
						Ins	trument	t [A]							
		•			Date		·····	- <del></del>				Rema	arks		
						Time	Depti (m)	Level (mOD)							
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o 1.2m	t hand excavated	113		ed to 2.28m sed to 9.21m	Ground	Level (mOD)	Client Dandara Jersey Ltd		Job Numb 150
raste PL Ri	9	Location	n		Dates	100,0044	Engineer		Sheet
		as	per site p	olan	02	//03/2014- //04/2014	Dandara		1/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
					1	(0.20) (0.20) (0.20)	MADE GROUND - Concrete	W. 1883	150
						(0.20)	MADE GROUND - Gravelly silt		
					1 5	(0.20)	Dark brown peaty SILT	4.1	
						(0.20)	Brown silty CLAY	1 325 200 200	
					1 3	E- 1	Dense light yellow brown to off white fine to medium silty SAND		200
00 4 05	ODT N-04			0.000.0.40.40		E	medium silty SAND		48
20-1.65 20-1.54	SPT N=34 X 0.34			2,2/6,8,10,10		E			
.54-1.71	X 0.20					(1.62)			
71-1,88 88-2.08	X 0.17 X 0.20					=		1000	133
08-2.28	X 0.20	2.26			3	E			
28-2.42	X 0.17	2.20				2.42		222	
42-2.65	X 0.00			28/03/2014:DRY			Dense off white grey brown slightly silty sandy GRAVEL	8.72	器
65-2.71 42-2.87	X 0.00 SPT N=45			01/04/2014:WET 5,11/11,12,12,10		(0.83)		1000	
71-2.85 85-3.25	X 0.43 X 0.40	2.68 3.25				E ' '			133
25-3.70	SPT N=7	3.25	GL	2,1/1,2,2,2		3.25	Firm brown sandy SILT with a little fine to medium	00000	
25-4.06	X 0.50	4.00	OL.	2,171,2,2,2			gravel	200	
				-		E		1888	器
				1		E		233	
06-4.56	X 0.50					=		X (1)	
								18.50	
56-5.01	SPT N=9		3.25	0,1/2,2,2,3	1 4	(2.67)			
56-5.12	X 0.50	4.30				E	4.		
12-5.42	X 0.33	4.68				È		1800	
42-5.92	X 0.50	5.68				E		23.5	
			1 - 8			E		399	
92-6.37	SPT N=28		GL	2,3/4,7,8,9		5.92	Medium dense brown clayey slightly sandy	70.00	
92-6.34	X 0.42	6.23				Ē I	GRAVEL	1	
34-6.53	X 0.19					E		75	100
53-6.92	X 0.39	6.68				E			
92-7.00	X 0.00		1			(1,68)		930	100
00-7.14 14-7.43	X 0.00 X 0.00								
		7.00				E			100
43-7.54 54-7.89	X 0.00 X 0.60	7.23				7.60		12.22	(0.9
		-				E	Stiff grey sandy clayey SILT with a little fine to medium gravel		100
89-8.34 89-8.27	SPT N=20 X 0.38	8.23	3.00	3.4/5,5.5,5	- 1	E	100000000000000000000000000000000000000	200	
27-8.58	X 0.31	100	4			E		4.6	
						(1.61)		Will the	
58-9.21	X 0.63		- 0			E			273
						E			
			9.00			9.21		200	200
21-9.66 21-9.49	SPT N=25 X 0.41	9.21	2.51	2,5/5,6,6,8		E	Stiff grey sandy CLAY with fine gravels		
49-9.79	X 0.27			01/04/2014:5.63m		F		1 200	1
79-9.96	X 0.20			02/04/2014:5.47m		7.60 (1.61) 9.21 (1.01)		27-33 32-33	1009
emarks									1 854
	excavated by hand, 10.62m	backfilled	before d	Irilling				Scale (approx)	Logge By
tary Drilling		one 11.60	- 6.00mh	eal				1:50	MEW
and below									
								Figure N	

C.22-10.49 C.49-10.62 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF	Haring Mad	hod	Cacina	Diamete	<u> </u>	Grave-d	t	d (mon)	Client		-	E
Depth   Sample   Tests   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Dep			113 0.9	3mm case )8mm cas			Leve	ei (mou)	Dandara Jersey Ltd		. N	ŧŧ
10.22   X 0.30   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.20   X 0.27   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X					alan	21. 02	/03/2 /04/2	2014- 2014	_		5	) E
2.22-10.49  X 9.27  C 9.49-10.62  SFT 6775  4.21  6.025,0,0,6  1.0-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10	Depth (iii)	Sample / Tosts	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	{ <b>Th</b> i	Depth (m) ickness)	Description	Legen	Water	
0.22-10.42	9.96-10.22	X 0.30						10.22	i de la companya de la companya de la companya de la companya de la companya de la companya de la companya de			T A A A
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7.72-11-5 C 0.36 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20 C 0.20	10.49-10.62	X 0.00				·	<u>-</u>		core recovery, recovered as slightly clayey sandy	(277.17)		Sections
O2/04/2014/2.05m  11.63  Complete at 11.65m  Complete at 11.65m	10.72-11.15	C 0.66						(1.14)	5-4-6:	4444444		1
02/04/2014:2.05m	11.10-11.00	0.30	<u> </u>									74000
Remarks  Complete at 11.85m  Complete at 11.85m  Complete at 11.85m					0.004/0.044/0.05			11.63				
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installation Type Single Installation			Dimensi Intern	ons as Diameter of Tube (A) = 50 r	Client Dandara Jersey Ltd							Job Number 1503				
			<b>Locatio</b> as pe	i r site plan	Ground	Ground Level (mOD) Engineer  Oandara								Shee 1		
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Consulting Civil Engineers and Geotechnical Specialists

## BOREHOLE LOG 1

Client Date Ove Arup

4 - 6 January 1994

Site Elevation Westaway Court St Helier

Sheet Scale 1 of 2 1:50

Progress/ Water levei	Casing (m)	Sample no./core	Sample /test	Depth (m)	Piezo- meter	Description	Depth (m)	Level	1 - 1
4.1.94		DI		0.10		Brown fine to medium slightly gravelly SAND with pockets of dark brown silt and organic material.	-		1
	0.75	D2 B1 D4 D3	SPT N=7	0.60 0.75- 1.50 0.75 0.75- 1.20		Loose light brown/grey fine slightly silty SAND with lenses of coarser brown/orange sand. The sands become darker and finer with depth.	0.60 -		
	1.50	B2 D6 D5	SPT N=6	1.50- 2.25 1.50 1.50- 1.95			-		
	2.25	B3 D8 D7	SPT N=5	2.25-3.00 2.25 2.25-2.70			,		
	3.00	B4 D10 D9	SPT N=12	3.00-3.75 3.00 3.00-3.45		Firm brown/crange slightly gravelly sandy clayey SILT with grey lenses of sandy clayey silt where the sand fraction reduces with depth.	3.00 -		X X
	3.75	B5 D12 D11	SPT N=11	3.75- 4.50 3.75 3.75- 4.20		·	-		x _ x
pm/3.90m 5.1.94	4.50	B6 D14 D13	SPT N=7	4.50- 5.25 4.50 4.50- 4.95		Firm brown/orange slightly gravelly clayey fine sand SILT. Including occasional lenses of grey clayey sandy silt.	4.50 y		×
! 	5.25	B7 D16 D15	SPT N=3	5.25- 6.00 5.25 5.25- 5.70				-	XXX
	6.00	B8 D18 D17	SPT N=8	6.00- 6.75 6.00 6.00- 6.45	<u> </u>	Firm black/dark brown sandy clayey SILT becoming alightly gravelly with depth.	6.00 ~	-	×
	6.75	B9 D20 D19	SPT N=13	6.75- 7.50 6.75 6.75- 7.20			-		× × ×
	7.50	B10 D22 D21	SPT N=13	7.50- 8.25 7.50 7.50- 7.95	11		_	- - -	× ×
	8.25	B11 D24 D23	SPT N=14	8.25-9.00 8.40 8.25-8.70	1//	Firm to stiff green/grey slightly gravelly (angular) sandy clayey SILT becoming darker and less clayey	8.40		×
	9.00	B12 D26 D25	SPT N=15	9.00- 9.75 9.00 9.00- 9.45	1//	with depth.		-	×××
	9.75	B13 D28 D27	SPT N=27	9.75-10.50 9.75 9.75-10.20		Continued sheet 2 of 2			X X
Equipment	/Methods			ssive boring 0.70m to 15		$\approx 0.70 \mathrm{m}$ to $15.00 \mathrm{m}$ ( $150 \mathrm{mm}$ casing) by C I Irrigation (D 00 litres.	rilling) Lin	iited.	
				o avoid servi 00m for an h		half an hour.	Job No. 94,000		gure

Consulting Civil Engineers and Geotechnical Specialists

## Borehole $\log 1$

2 of 2

Westaway Court St Helier Sheet Site Client Ove Arup 1:50 Scale Elevation Date 4 - 6 January 1994

Progress/ Water level	Casing (m)	Sample no./core	Sample /test	Depth (m)	Piezo- meter	Description	Depth (m)	Level (mOD)	Legend
5.1.94	10.50	B14 D30 D29	SPT N=16	10.5-11.25 10.50 10.5-10.95		Firm to stiff green/grey slightly gravelly (angular) clayey sandy SILT becoming darker and less clayey with depth.			× -
	11.25	B15 D32 D31	SPT N=20	11.25-12.0 11.25 11.25-11.7		Very stiff blue/grey slightly gravelly very silty CLAY.	11.30 _		x x x x x x x x x x x x x x x x x x x
vater struck 13.60m, Fast inflow, Rose to	(150) 13.50 12.75	D33 B16 D34	SPT N=23	12.50 12.75-13.5 12.75-13.2			-		X X
7.50m. om/5.90m 6.1.94 sin/5.90m	13.60	U2 B17 D35 D36	SPT N=31	13.50 13.6-14.25 13.60 13.6-14.05		Dense blue/grey slightly clayey SILT and SAND.	13.60 ~	7	X   X   X   X   X   X   X   X   X   X
pm/6.00m	14.25	B18 D37	SPT N=60+	14.25-14.9 14.25-14.7		Moderately strong slightly weathered blue/grey fine grained igneous rock (Basalt?).  Bitte/black fine grained basic igneous rock, as above.	14.30 14.90		V V V V
	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the 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Equipment						n 0.70m to 15.00m (150mm casing) by C I knigation (Dri	-		

Water added from 0.70m to 15.00m, 200 litres.

Chiselling from GL to 0.70m to avoid services for half an hour. Remarks Chiselling from 14.90m to 15.00m for an hour.

Job No. 94.002 Figure

Consulting Civil Engineers and Geotechnical Specialists

# Trial pit $\log 3$

Client Date Ove Arup

5 January 1994

Site

Elevation

Westaway Court St Helier

Sheet Scale

1 of 1 1:50

Vater Ævel	Sample No.	Sample /test	Depth (m)	Description of Strata	Depth (m)	Reduced Levels		Legend	
				mangati / mronn	0.20	k x/l			
				TOPSOIL / TURF Brown fine SAND	0.40	<del> </del>			·····
			ļ	Brown the SAND	0.40			······································	
				(Loose to medium dense) off-white light	-				
				brown fine SAND	-				
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	T	rial pit exc	avated by C	hannel Island Drilling Limited with MF 860 b	ackboe. I	it size 3.0m	ıx0.8m in p	lan.	
: mare - 1	Water	-					<u> </u>	Job No.	Logged by

Consulting Civil Engineers and Geotechnical Specialists

# TRIAL PIT LOG 4

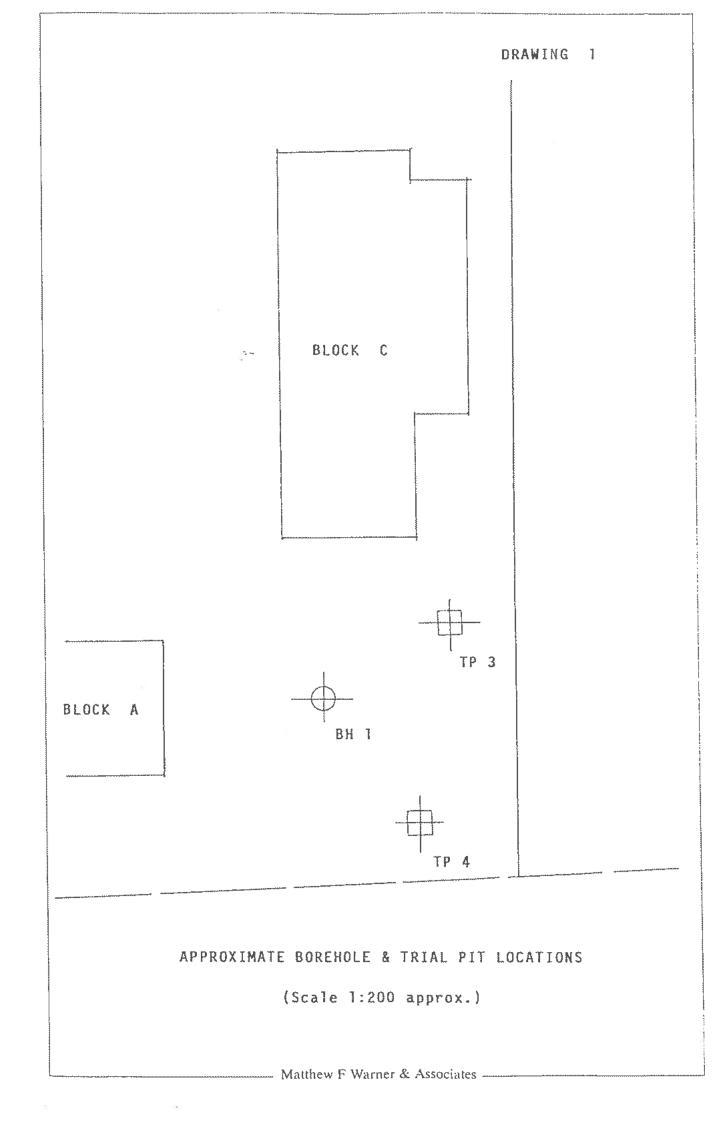
Client Date Ove Arup

5 January 1994

Site Elevation Westaway Court St Helier

Sheet Scale 1 of 1 1:50

Trial pit excavated by Channel Island Drilling Limited with MF 860 backboo. Pit size 3.0mx0.8m in plan.  Trial pit excavated by Channel Island Drilling Limited with MF 860 backboo. Pit size 3.0mx0.8m in plan.    Job No.   Logasco. No.	Water Level	Sample No.	Sample /test	Depth (m)	Description of Strata	Depth (m)	Reduced Levels		Legend	
Commendate Trial pit excevated by Channel Island Drilling Limited with MF 860 backboo. Pit size 3.0mx0. 8m in plan.					TOPSOIL / TURF			$\times$	······································	
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MADE GROUND: brick, stone in grey sity matrix, slightly organic  (Loose) off-white line SAND  2.50  END OF TRIAL PIT  Trial pit excavated by Channel Island Drilling Limited with MF 860 backboo. Pit size 3.0mx0.8m in plan.					(Loose to medium dense) off-white light	0.60		XXX		
ailty matrix, slightly organic  (Loose) off-white fine SAND  2.50  END OF TRIAL PIT  Trial pit excavated by Channel Island Drilling Limited with MF 850 backboe. Pit size 3.0mx0.8cm in plan.  Trought Water    Job No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest b					brown fine SAND (Fill)	l .				
ailty matrix, slightly organic  (Loose) off-white fine SAND  2.50  END OF TRIAL PIT  Trial pit excavated by Channel Island Drilling Limited with MF 850 backboe. Pit size 3.0mx0.8cm in plan.  Trought Water    Job No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest by No.   Loggest b					MADE GROUND: brick, stone in grey	l _				
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			None						94.002	MFW



## **Appendix F-1**

Geotechnical Desk Study - Part 3

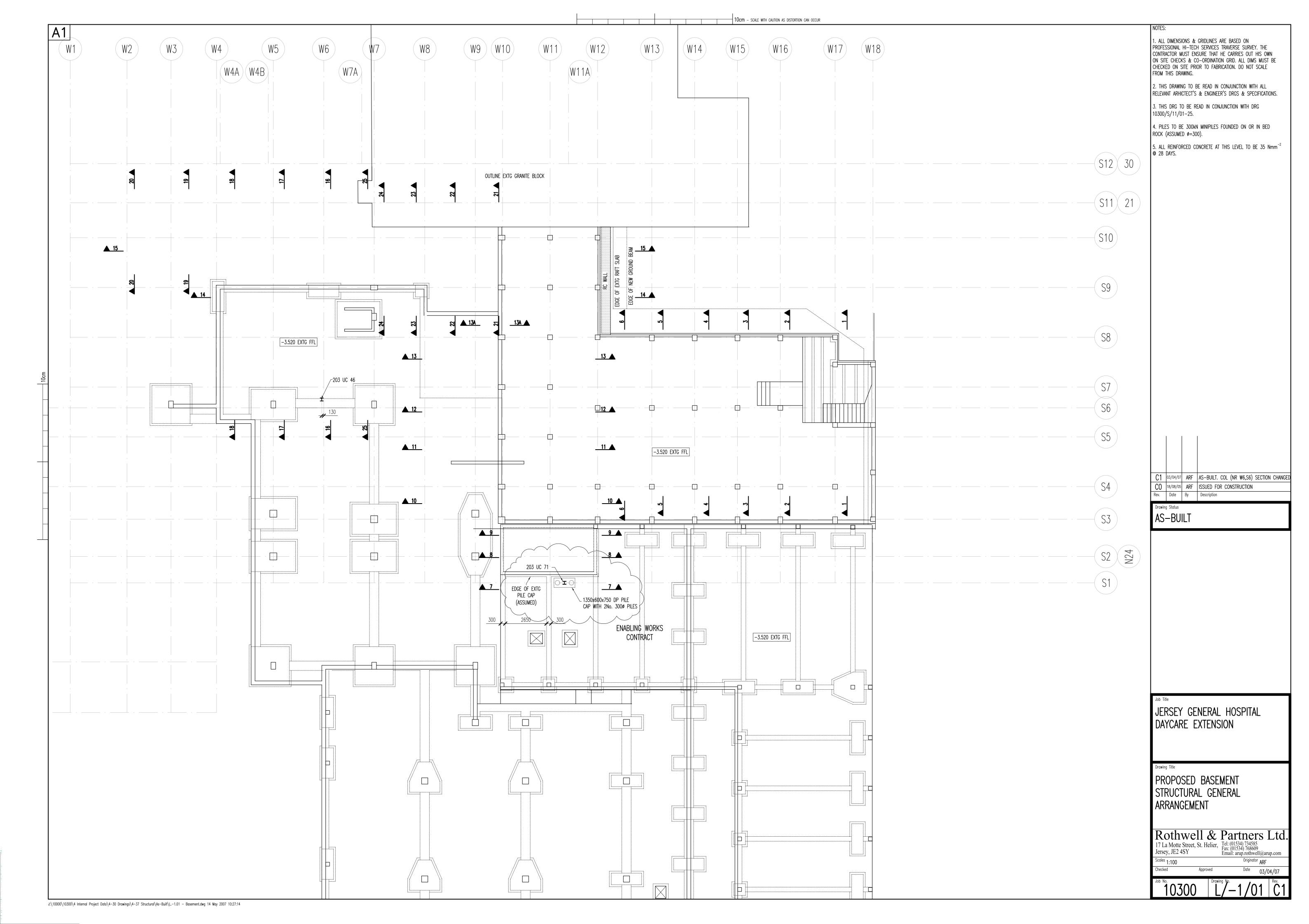
## Appendix E

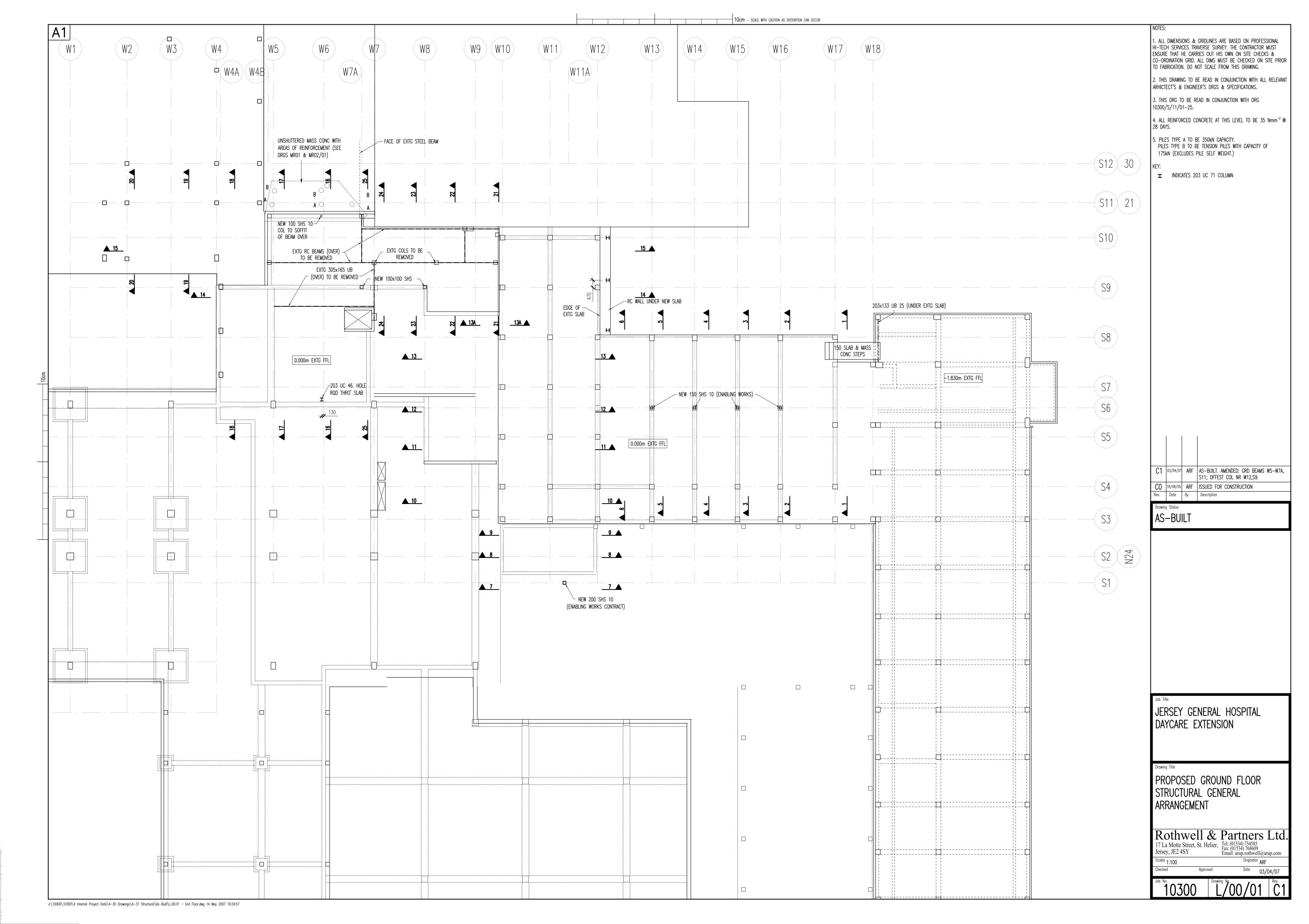
Available Construction Drawings

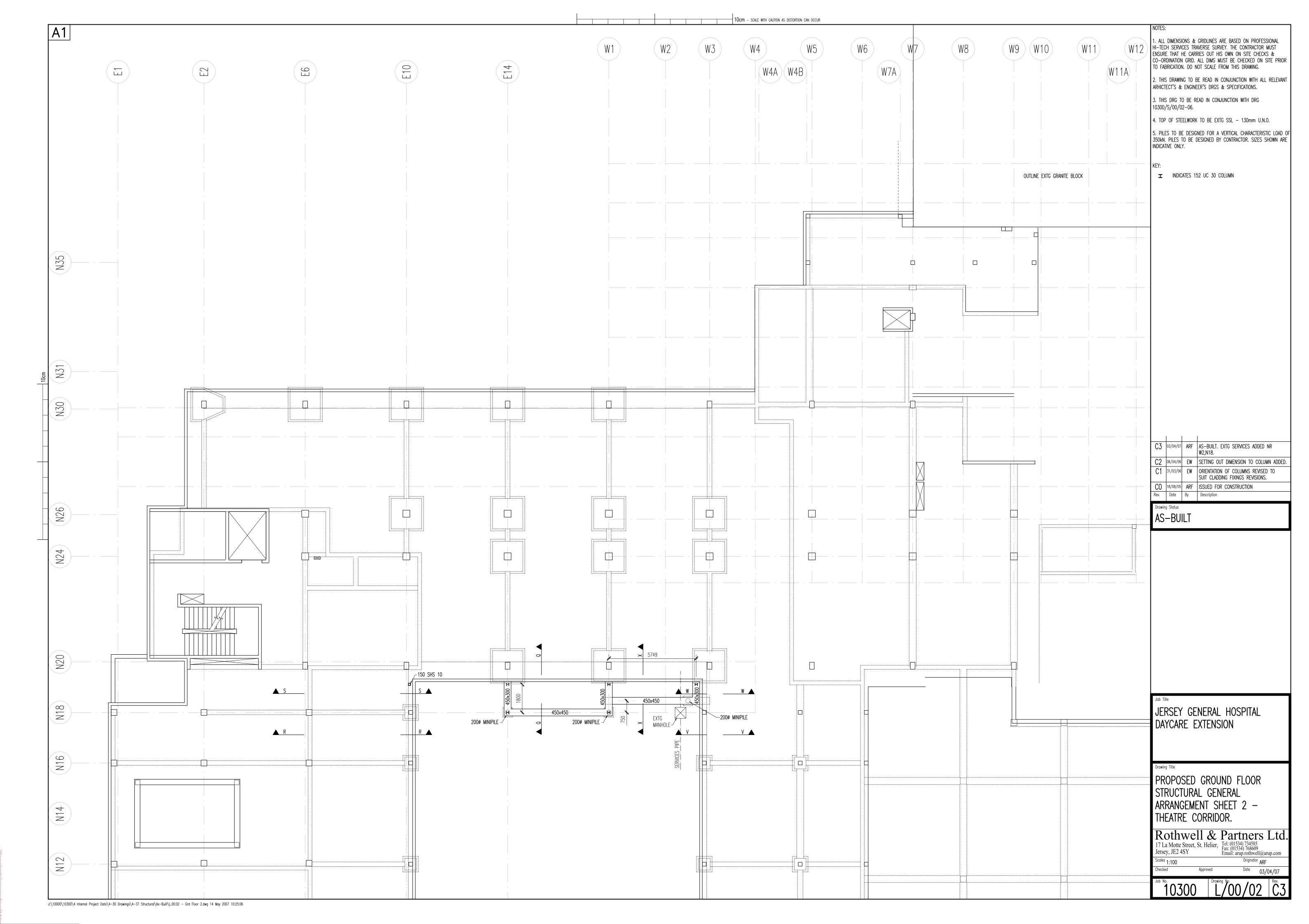
#### **Appendix E-1**

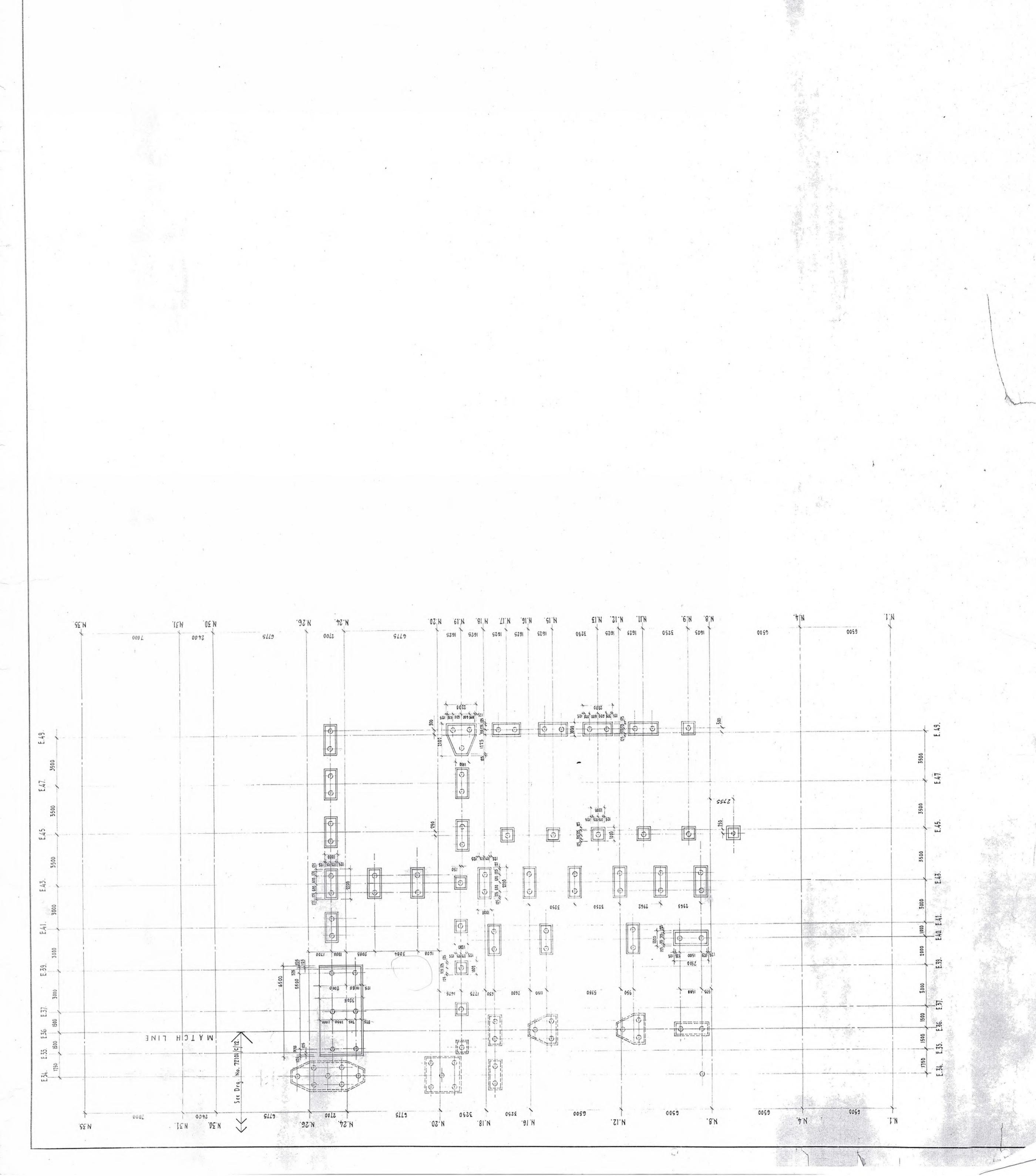
#### Available Construction Drawings – Jersey General Hospital

- Jersey General Hospital Daycare Extension, Proposed Basement Structural General Arrangement, Revision C1, Apr 2007
- Jersey General Hospital Daycare Extension, Proposed Ground Floor Structural General Arrangement, Revision C1, Apr 2007
- Jersey General Hospital Daycare Extension, Proposed Ground Floor Structural General Arrangement Sheet 2 – Theatre Corridor, Revision C3, Apr 2007
- Department of Public Building and Works States Offices, General Hospital Phase 1, General Arrangement Pile Caps Sheet 2, Revision D, Jun 1976
- Department of Public Building and Works States Offices, General Hospital, Jersey Phase One Redevelopment, Pile Layout Sheet 1, Feb 1975
- Department of Public Building and Works States Offices, General Hospital, Jersey Phase One Redevelopment, Pile Layout Sheet 2 – Revision D, Apr 1976
- Culvert Details, 6-14 Gloucester Street, St Helier, Jersey, Rothwell & Partners Ltd, Feb 2006
- Pile Layout, Jersey General Hospital, Phase 1B, Ove Arup & Partners Revision A, May 1980
- Existing Basement Plan, Jersey General Hospital, Health & Social Services, Jersey Property Holdings Design & Building Services, Drawing 001, Aug 2016
- Existing ground Floor Plan, Jersey General Hospital, Health & Social Services, Jersey Property Holdings Design & Building Services, Drawing 002, Aug 2016
- Phase 1A Engineering Department, Pile Layout, Sheet 1, Ove Arup & Partners, Working Drawing, September 1978
- Phase 1A Engineering Department, Pile Layout, Sheet 2. Ove Arup & Partners, Working Drawing, September 1978



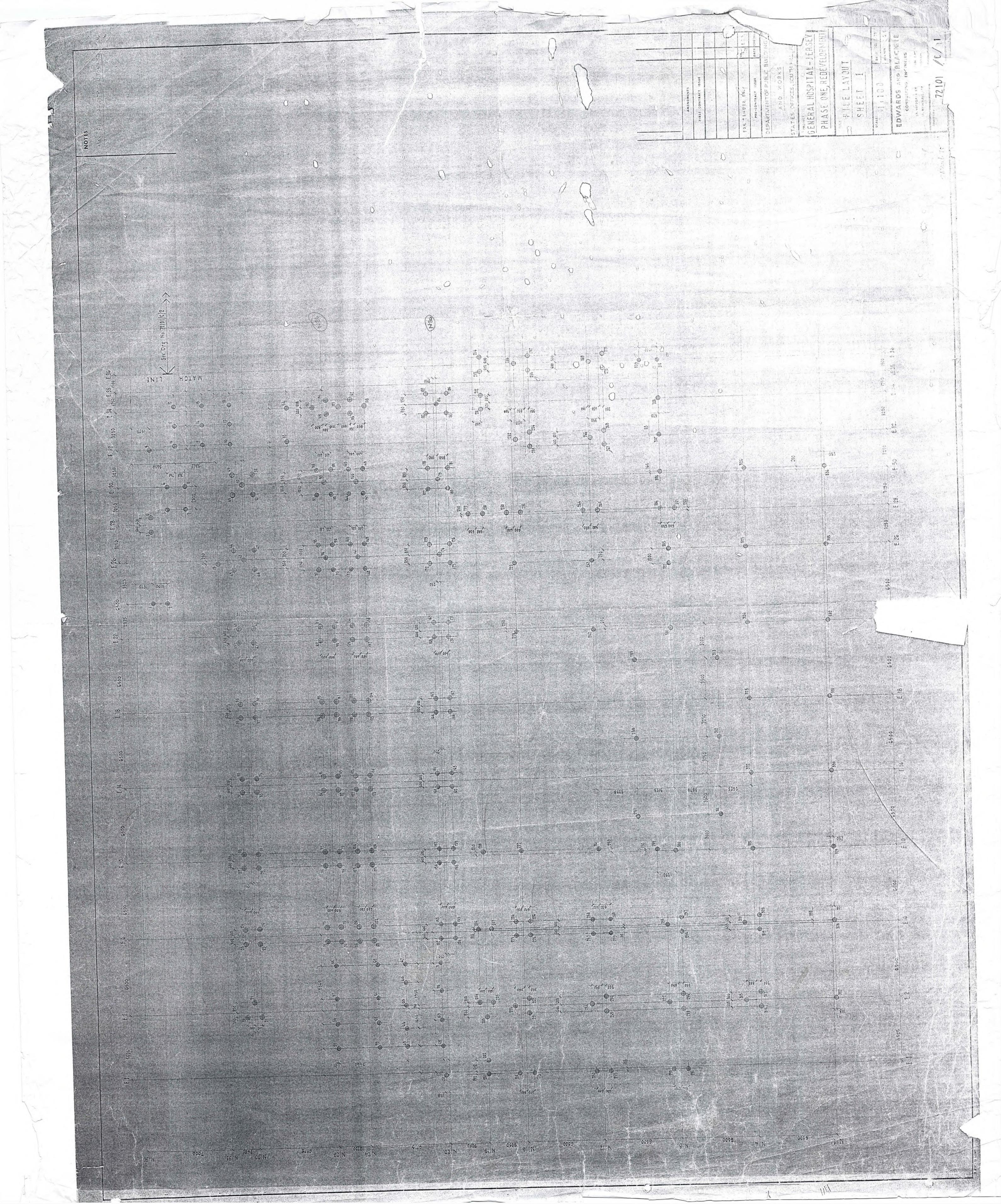






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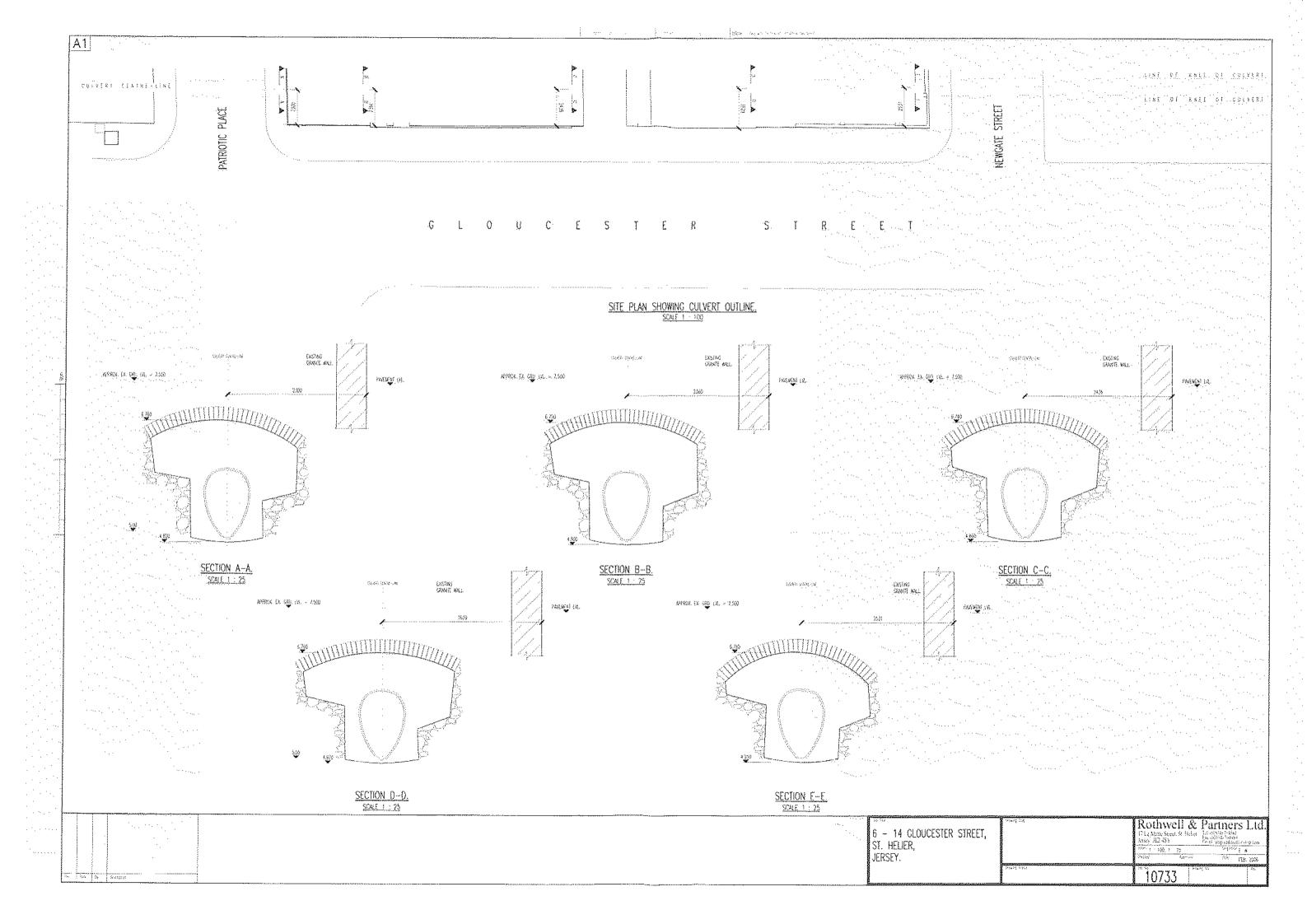
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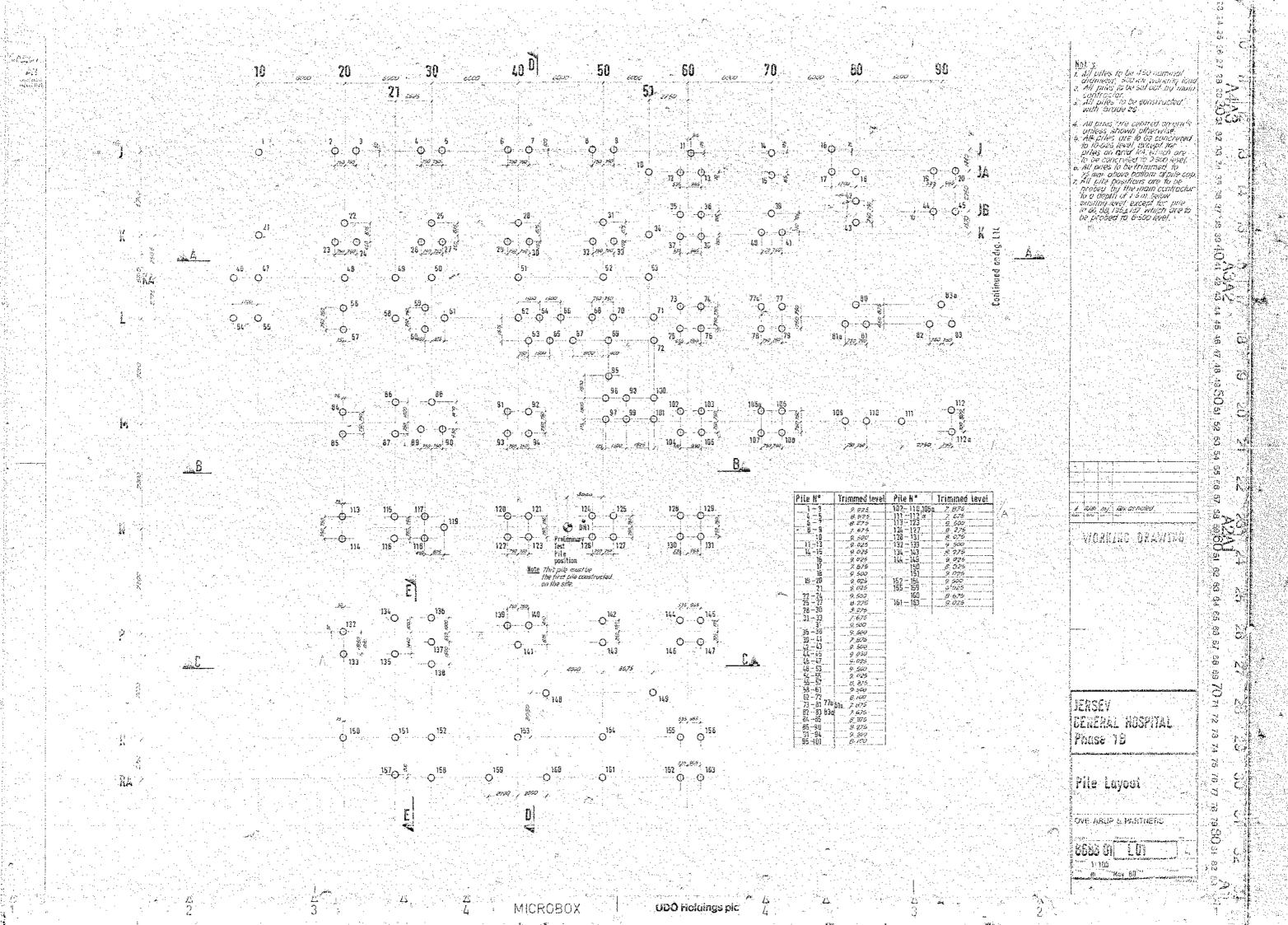
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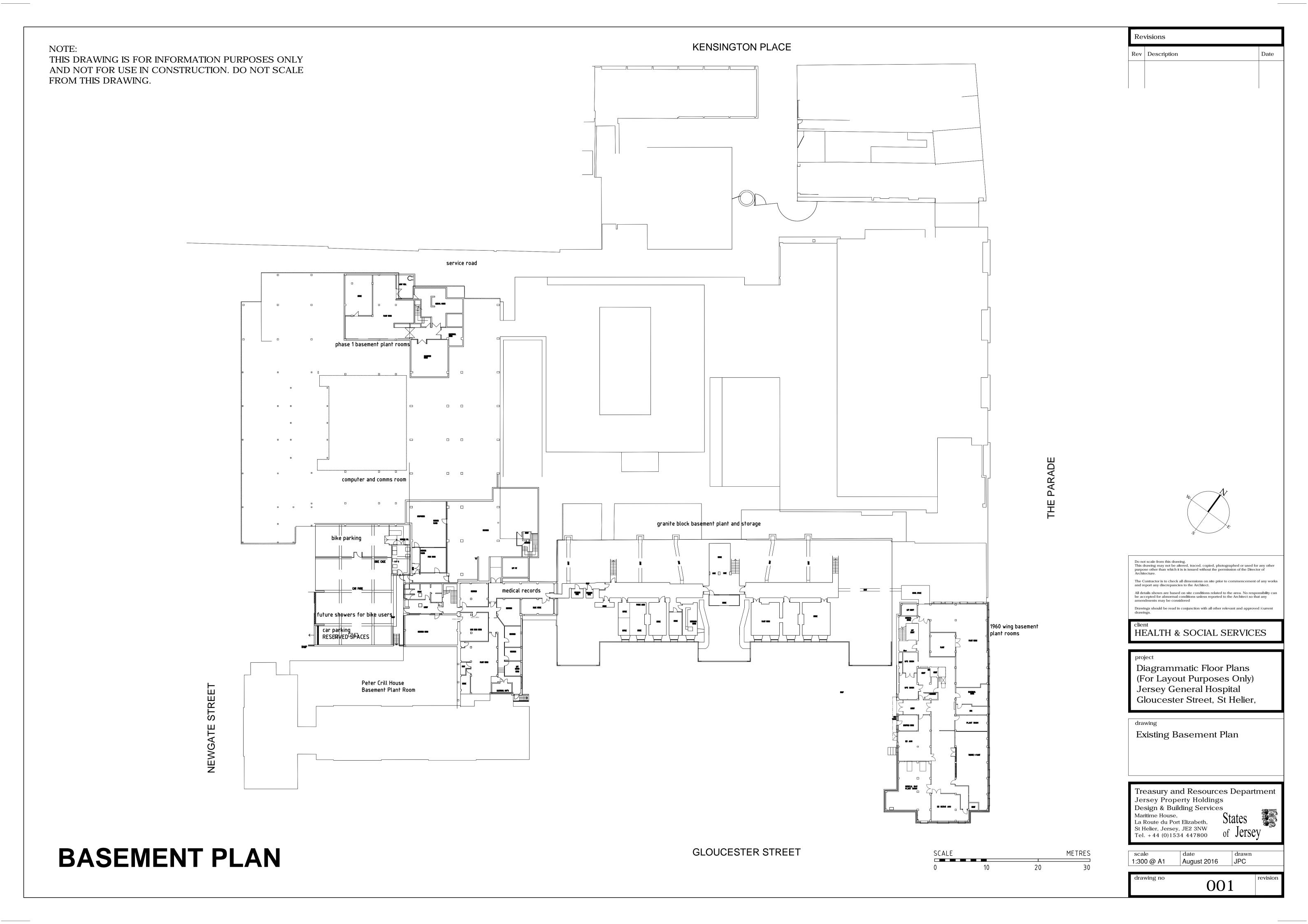
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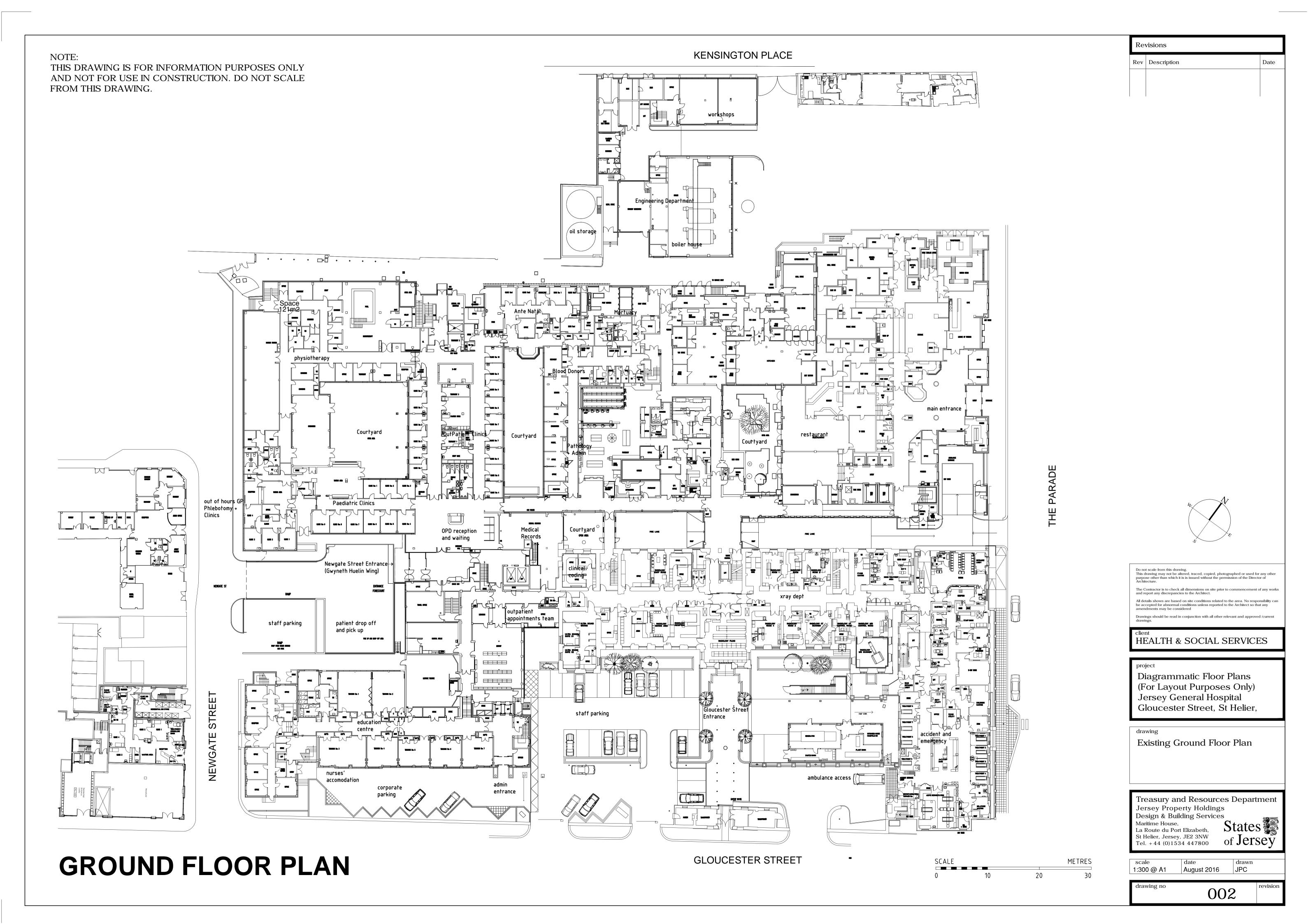


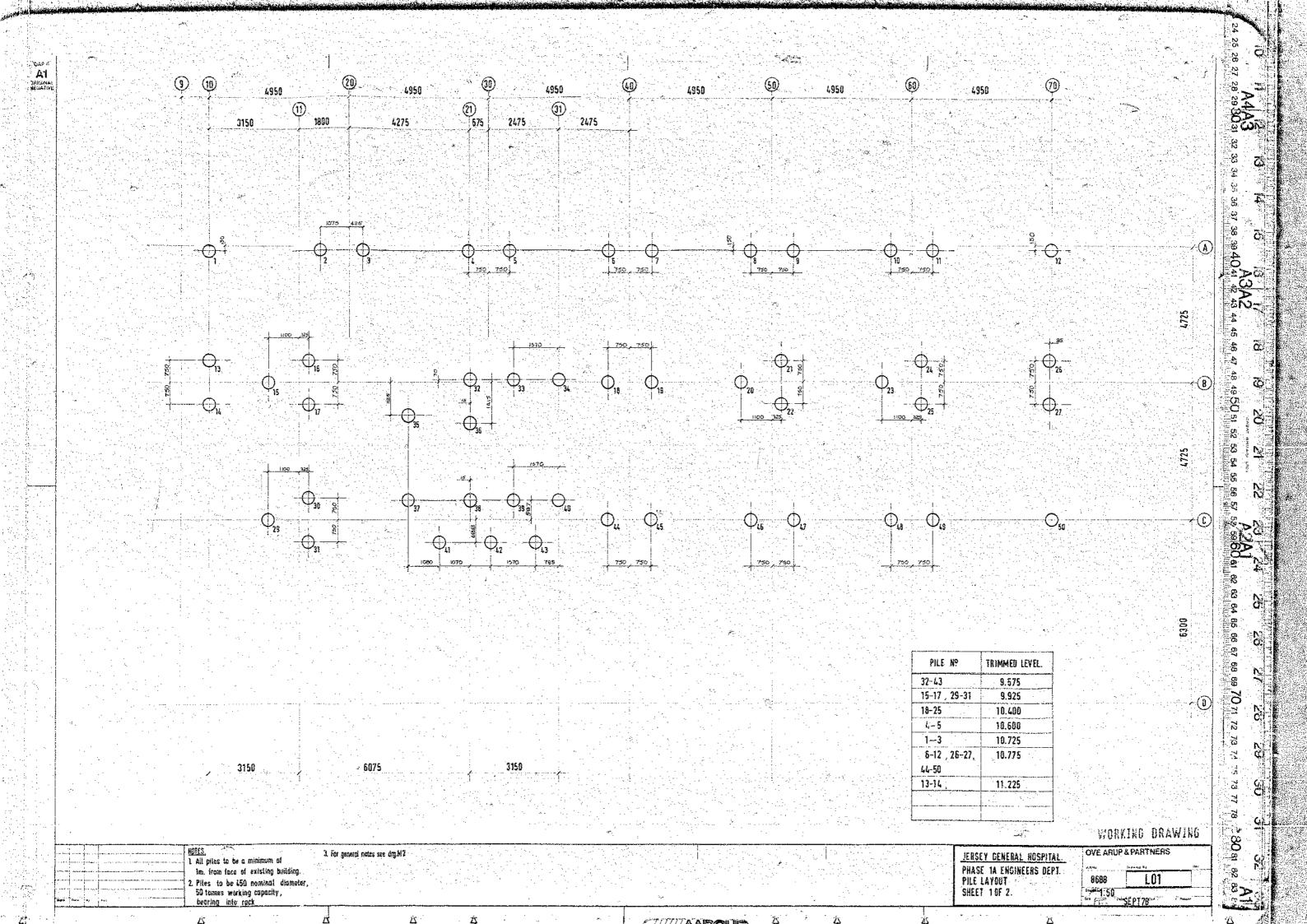


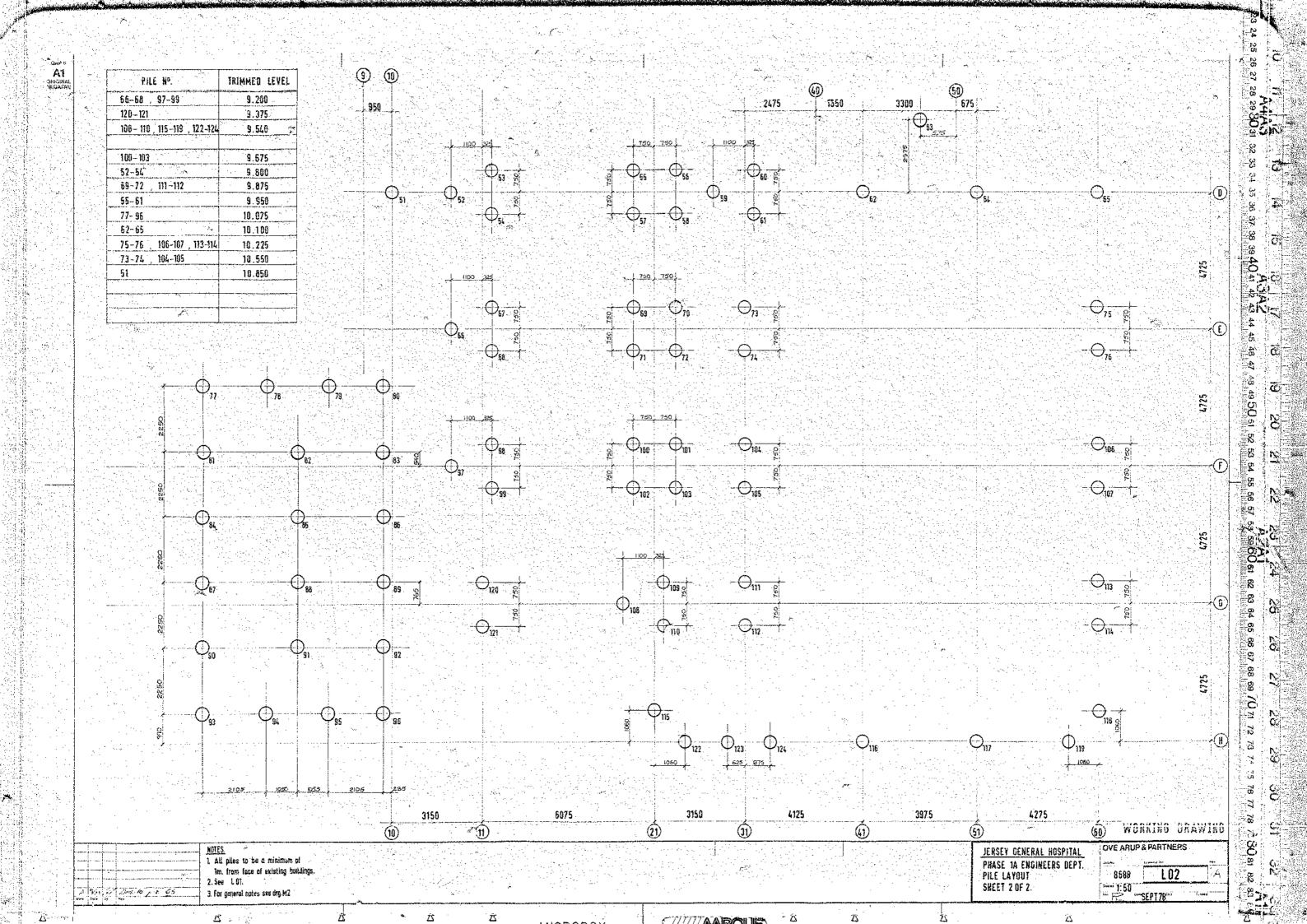
## **Appendix F-1**

Geotechnical Desk Study - Part 4





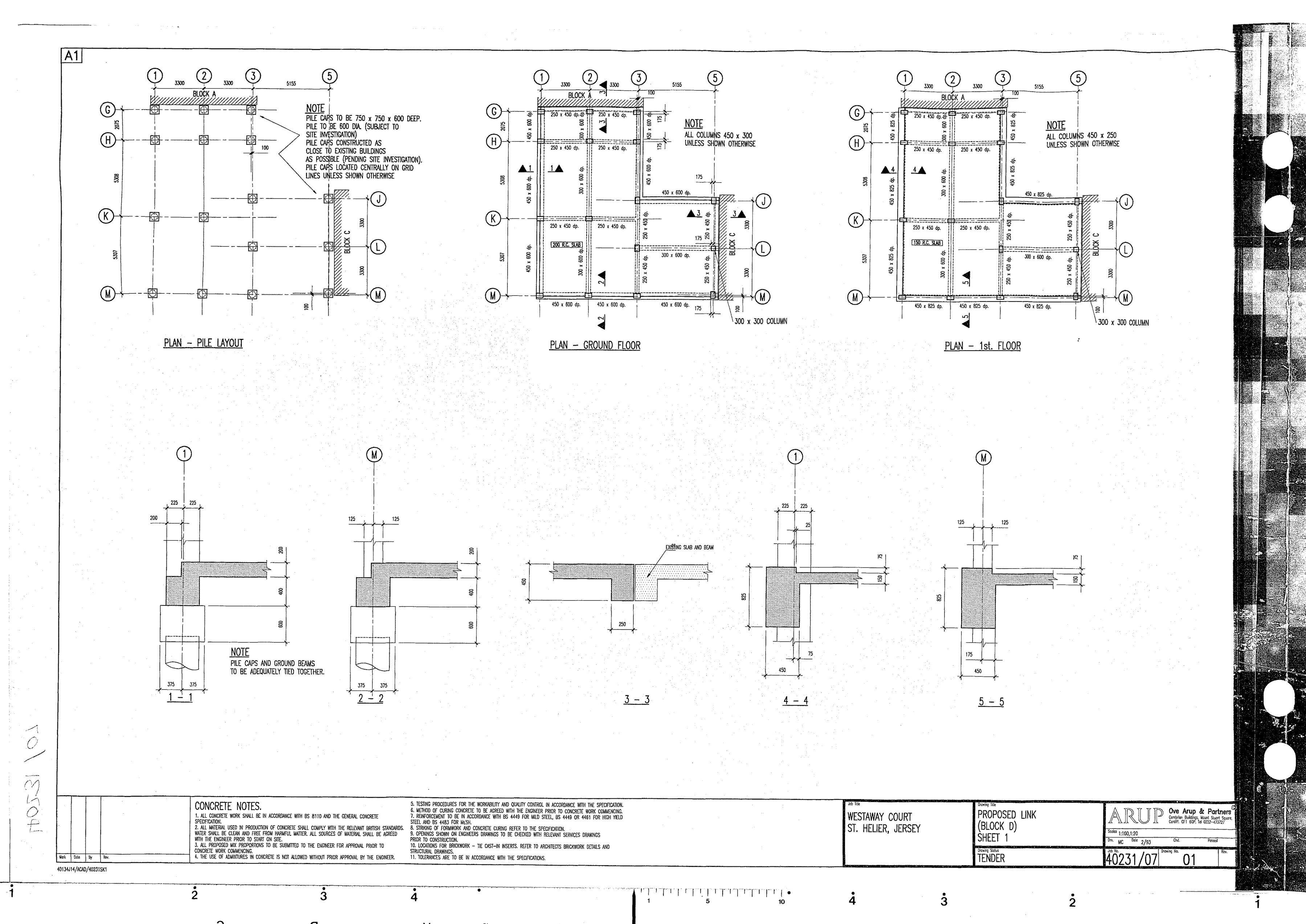




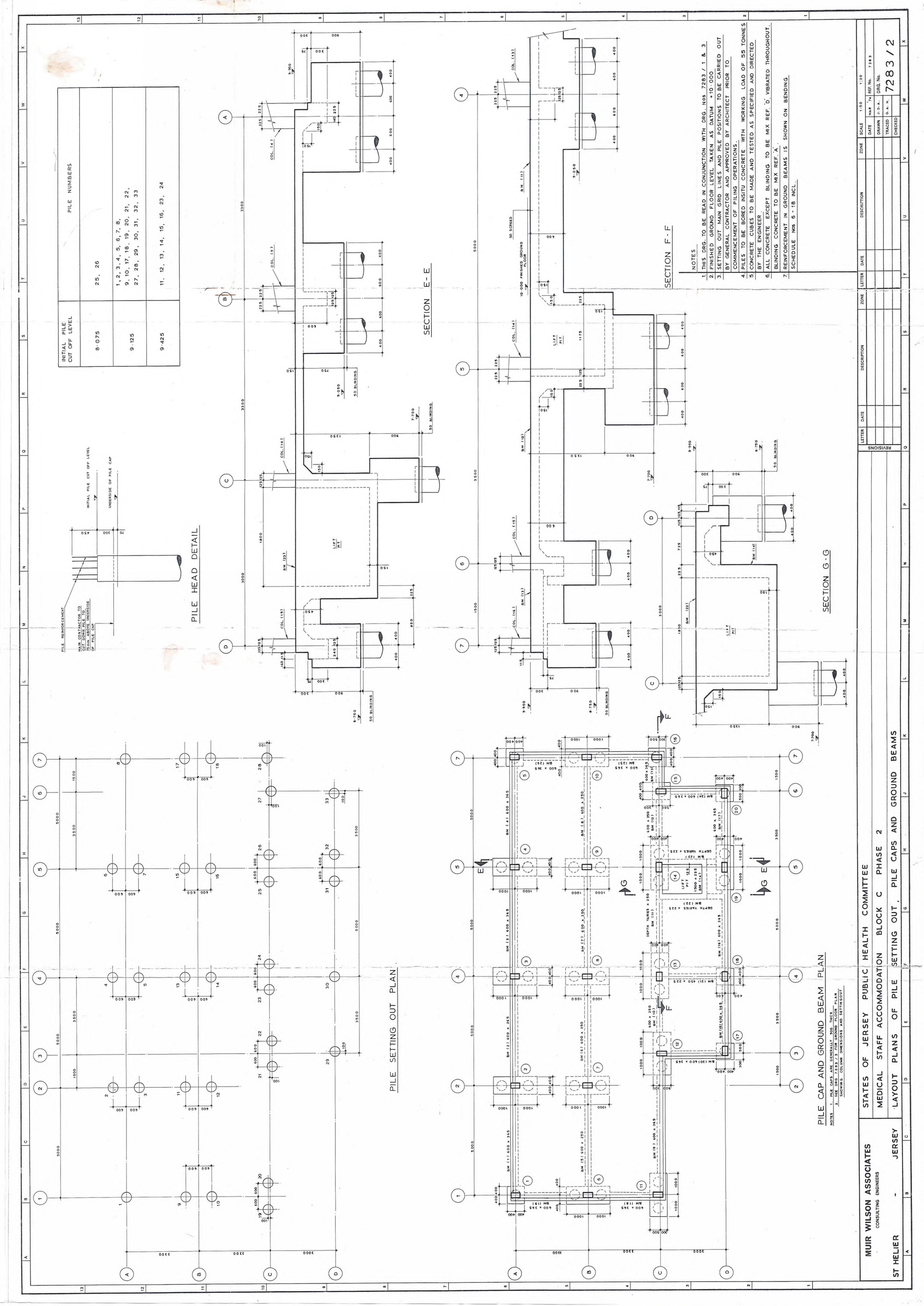
## **Appendix E-2**

Available Construction Drawings – Westaway Court

- Ove Arup and Partners, Westaway Court, Proposed Link (Block D) Sheet 1, (February 1993)
- Layout Plans of Pile setting out, Pile Caps and Ground Beams, Medical Staff Accommodation Block C Phase 2, Muir Wilson Associates, (March 1974)



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## **Appendix F-1**

Geotechnical Desk Study - Part 5

# Appendix F

Ground Risk Register (GRR)



Register referen
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Project	Jersey Future Hospitals & Westaway Court	Job number	237035-00
Package/Topic		Design stage	

Date (+ initials)	Area/Location of Risk Exposure	Description of Hazard and Risk Exposure	Mitigation of Risk (Potential or Achieved)	Α	R	С	Further Action	Ву	Status Active / Closed
15/09/16 (JC)	Jersey General Hospital	Anecdotal evidence of running sand under site area. Possibility of encountering more running sand and destabilising existing buildings.	Undertake ground investigation to determine extent and thickness of blown sand deposits and therefore potential for running sand.				Ground Investigation		Active
27/09/16 (JC)	Jersey General Hospital & Westaway Court	Sub-surface obstructions, such as existing piles, encountered during construction.	Use existing pile layout drawings to inform of current pile locations and where they will be encountered.						Active
27/09/16 (JC)	Jersey General Hospital	Damage caused to existing surface water culvert running parallel to Peter Crill house.	Undertake ground investigation to determine depth and location of culvert.				Ground Investigation		Active
27/09/16 (JC)	Westaway Court	Possible sub surface obstructions from previous building on site as indicated from historical mapping.	Undertake ground investigation to understand the extent and type of possible foundations				Ground Investigation		Active



Register referen
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Project	Jersey Future Hospitals & Westaway Court	Job number	237035-00
Package/Topic		Design stage	

Date	Area/Location of	Description of Hazard and	Mitigation of Risk	Α	R	С	Further Action	Ву	Status
(+ initials)	Risk Exposure	Risk Exposure	(Potential or Achieved)	^	IX		Tuttier Action	Бу	Active / Closed
			associated with historical building.						
27/09/16 (JC)	Jersey General Hospital & Westaway Court	Arisings classed as hazardous, suitable for hazardous waste disposal only.	Undertake ground investigation to confirm nature and classification of arisings through chemical testing.				Ground Investigation		Active
27/09/16 (JC)	Jersey General Hospital	Possible interaction with groundwater during basement development.	Undertake ground investigation and in combination with previous GI records determine groundwater level. Look at appropriate design options to mitigate against ground water incursion.				Ground Investigation		Active



Register reference
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Project	Jersey Future Hospitals & Westaway Court	Job number	237035-00
Package/Topic		Design stage	

Date	Area/Location of	Description of Hazard and	Mitigation of Risk	Α	R	С	Further Action	By	Status
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28/09/16 (JC)	Jersey General Hospital	Unknown extent of underground structure, identified in site photo 23 in <b>Appendix B-1</b> .	Further site investigation to determine the extent and nature of the structure shown on photo 23 in <b>Appendix B-1</b> .						Active
28/09/16 (JC)	Jersey General Hospital	Gas storage identified in site photos 6 and 7 in <b>Appendix B-1</b> could pose a risk to future ground investigation.	Gas bottles must be removed before any ground investigation is undertaken within the vicinity.				Temporary removal of gas storage		Active
30/09/16 (JC)	Jersey General Hospital & Westaway Court	Potential for artesian groundwater conditions.	Further investigation required for scope of the ground investigation works.				Ground Investigation		Active
30/09/16 (JC)	Jersey General Hospital	Possibility that the ground underneath site is impacted by saline intrusion.	Ground investigation is recommended to install tidal inducer monitoring to determine saline intrusion.				Ground Investigation		Active

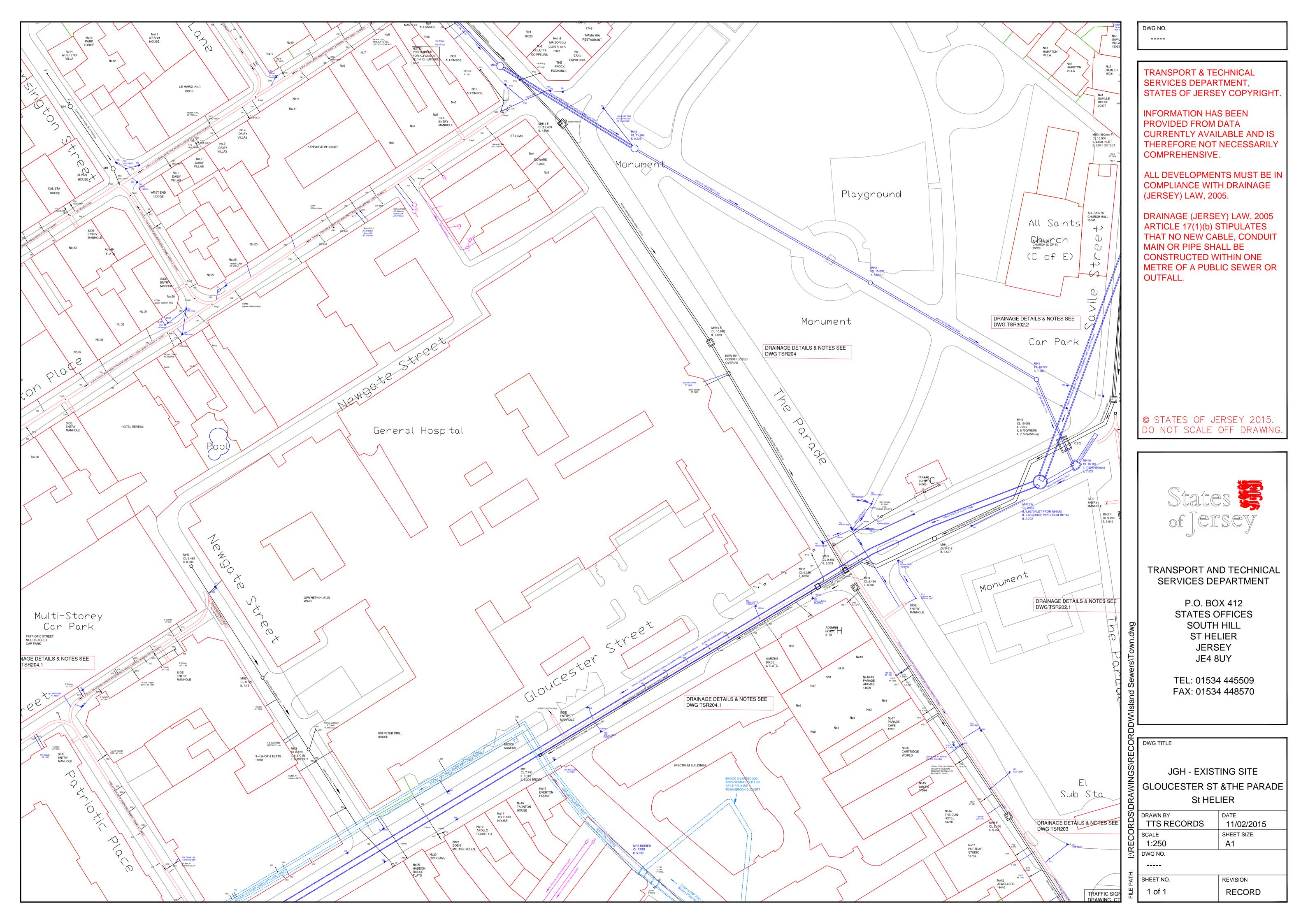


Project	Jersey Future Hospitals & Westaway Court	Job number	237035-00
Package/Topic		Design stage	

Date	Area/Location of	Description of Hazard and	Mitigation of Risk	Α	R	С	Further Action	Bv	Status
(+ initials)	Risk Exposure	Risk Exposure	(Potential or Achieved)					-7	Active / Closed
30/09/16 (JC)	Jersey General Hospital	Risk of buildings outside of building footprint will required demolition to accommodate the new proposed basement and building.	Careful consideration of demolition extent in particular between Blocks E and F and Block G and the existing hotel buildings.						Active
28/10/16 (JC)	Jersey General Hospital	'Le Faux Bie' stormwater culvert, parallel to Gloucester Street, may impact on foundation design requirements and temporary works	Accurately locate and position stormwater culvert. Accommodation of appropriate foundation design consideration at early stage.				Review of available culvert drawings and surveys (when complete) in relation to foundation design consideration.		<u>Active</u>

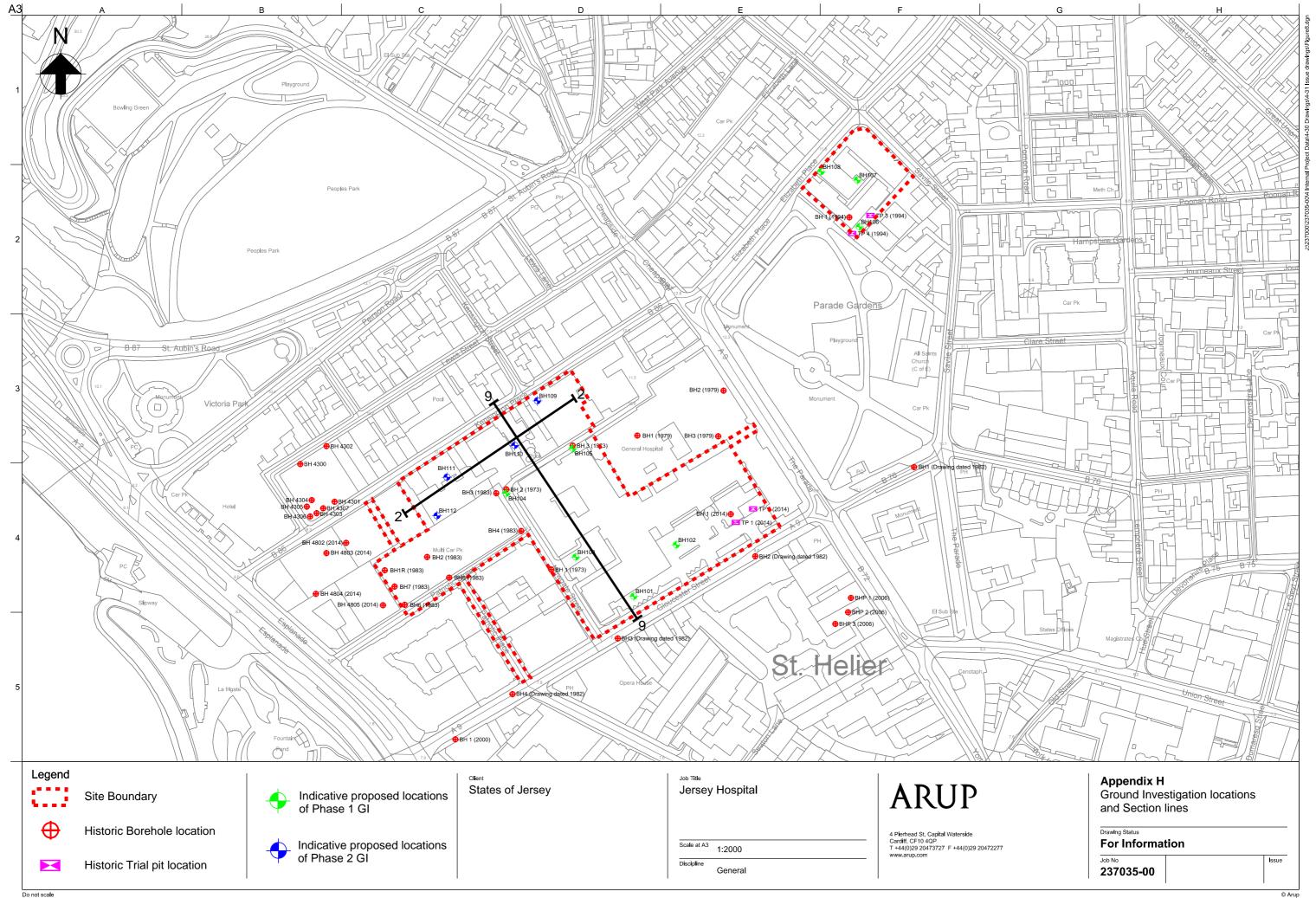
## **Appendix G**

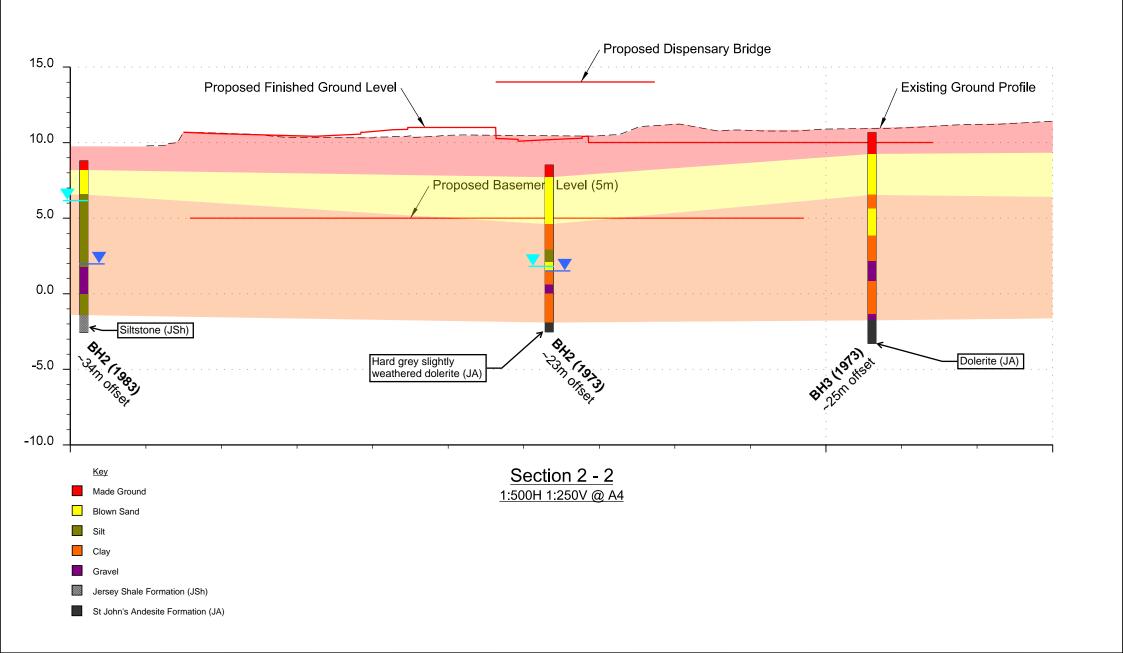
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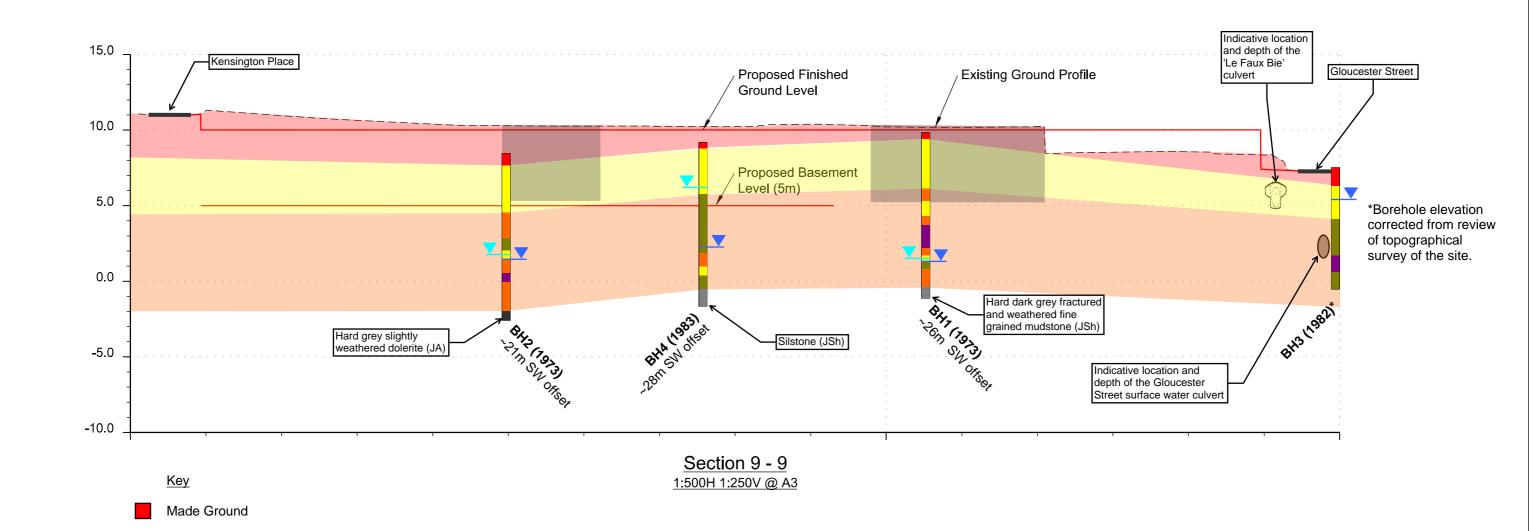


# Appendix H

Geological Section Drawings







Blown Sand

Gravel

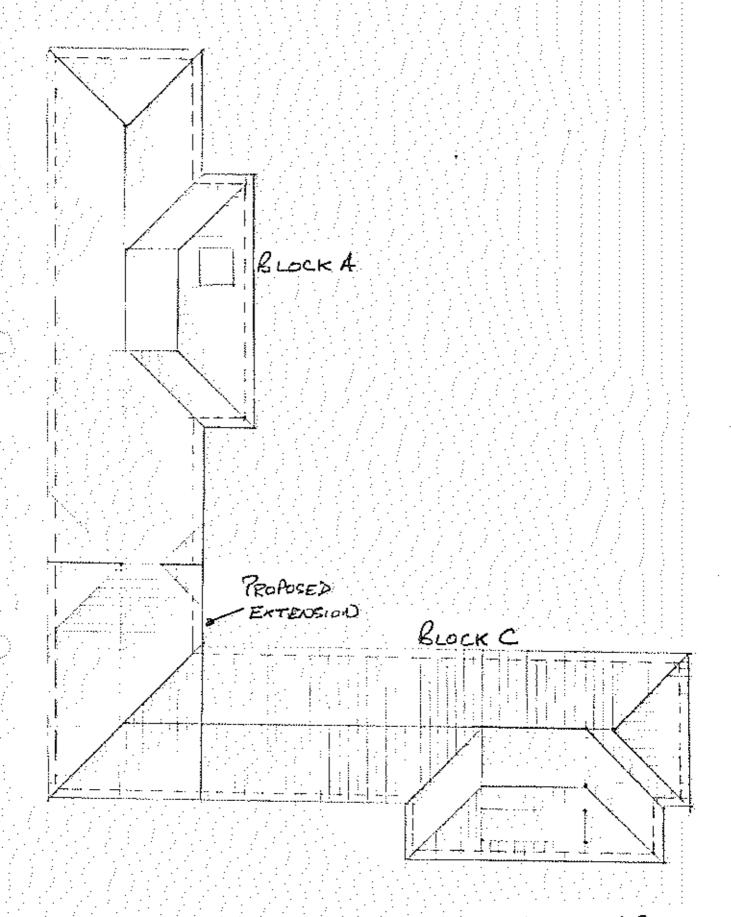
Jersey Shale Formation (JSh)

St John's Andesite Formation (JA)

## **Appendix I**

Extracts of Arup Calculations & Sketches - Westaway Court

# I1 Extracts of Arup Calculations & Sketches – Westaway



WESTAWAY COULT 40231/07 OVERALL PLAN OF PROPOSED PITCHED ROOFSCHENE SKA

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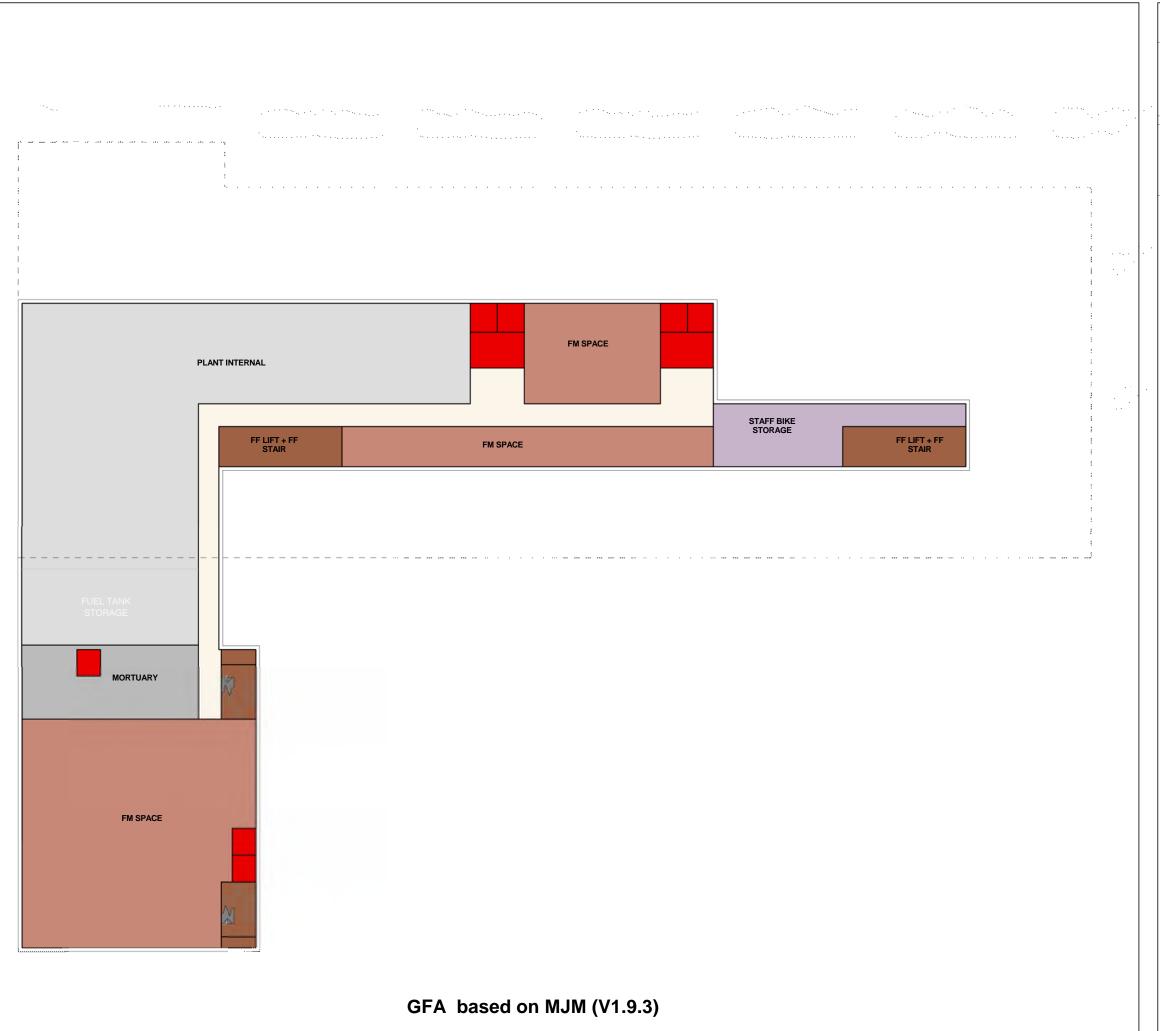
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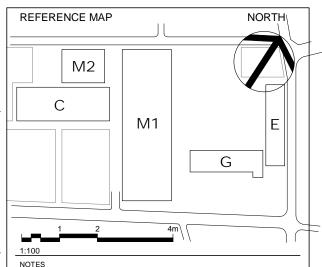
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# Appendix J

Indicative Project Proposals

# J1 Jersey General Hospital Indicative Proposals





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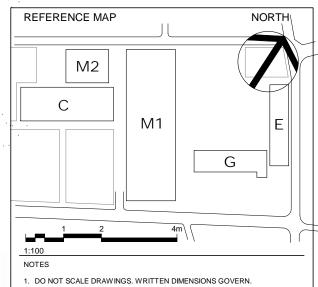
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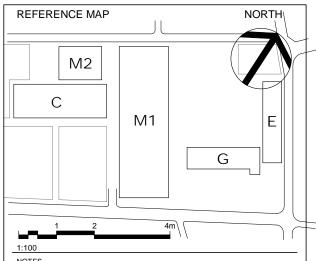
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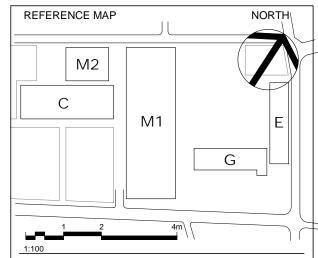
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JERSEY FUTURE HOSPITAL (JFH) - MAIN HOSPITAL SITE THE PARADE, ST HELIER, JERSEY JE1_3QS

DRAWING TITLE

#### L02 SECOND FLOOR -**DEPARTMENTS**

STATUS

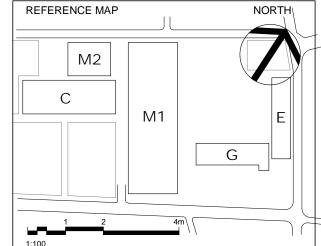
### **INFORMATION**

SCALE @ A3 ORIGINATOR PROJECT # REVIEWED APPROVED 012145 JB PROJECT# - ORIGIN. - ZONE - LEVEL - TYPE - ROLE - DRAWING# - STATUS+REV

JFH-HSL-M0-02-DR-A-1803-S2.P33



GFA based on MJM (V1.9.3)



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REV	DESCRIPTION	DATE
S2.P26	Functional Layout	07/04/17
S2.P29	Drawing Updated	26/04/17
S2.P30	Areas Updated	09/05/17
S2.P31	Areas Updated	15/05/17
S2.P32	Graphics Updated	16/05/17
S2.P33	Areas Updated	05/06/17

CONSULTANT

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DRAWING TITLE

### L03 THIRD FLOOR -**DEPARTMENTS**

STATUS

## **INFORMATION**

SCALE @ A3 ORIGINATOR PROJECT # REVIEWED APPROVED 012145 JB PROJECT# - ORIGIN. - ZONE - LEVEL - TYPE - ROLE - DRAWING# - STATUS+REV

JFH-HSL-M0-03-DR-A-1804-S2.P33

NORTH(

05/06/17

16/05/17

15/05/17

09/05/17

26/04/17

07/04/17

DATE

C:_Fevit Projects\JFH-HSL-M0-ZZ-M3-A-BUILD_PR_2_kiejm.rvt

S2.P26

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Areas Updated

Areas Updated

Areas Updated

Drawing Updated

Functional Layout

**DESCRIPTION** 

Graphics Updated

#### HASSELL

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#### STATES OF JERSEY

JERSEY FUTURE HOSPITAL (JFH) - MAIN HOSPITAL SITE THE PARADE, ST HELIER, JERSEY JE1_3QS

DRAWING TITLE

#### L04 FOURTH FLOOR -**DEPARTMENTS**

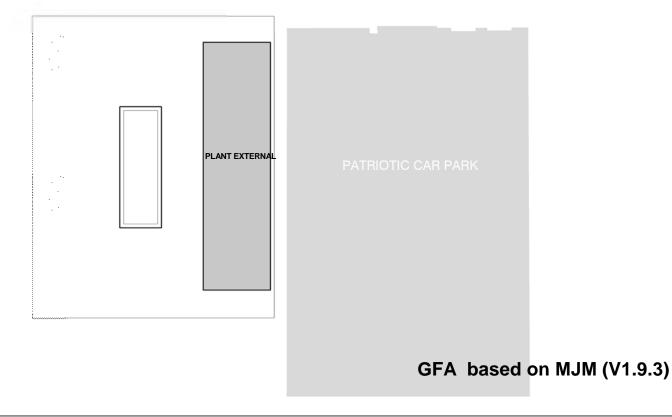
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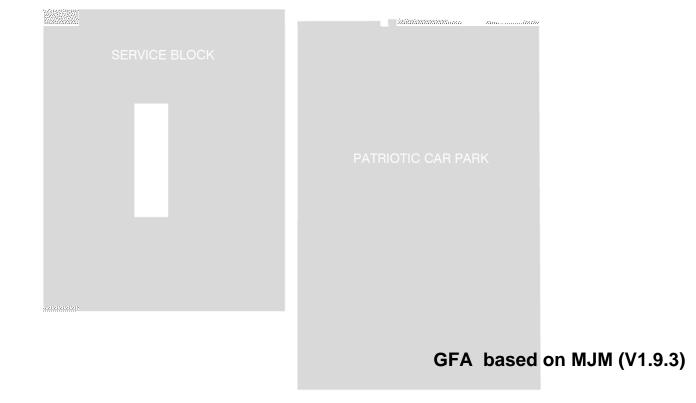
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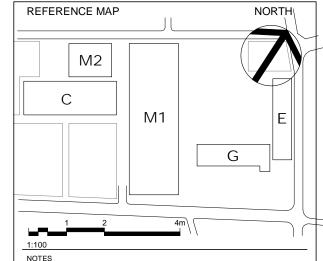
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JFH-HSL-M0-04-DR-A-1805-S2.P33









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S2.P31	Areas Updated	15/05/17
S2.P32	Graphics Updated	16/05/17
S2.P33	Areas Updated	05/06/17

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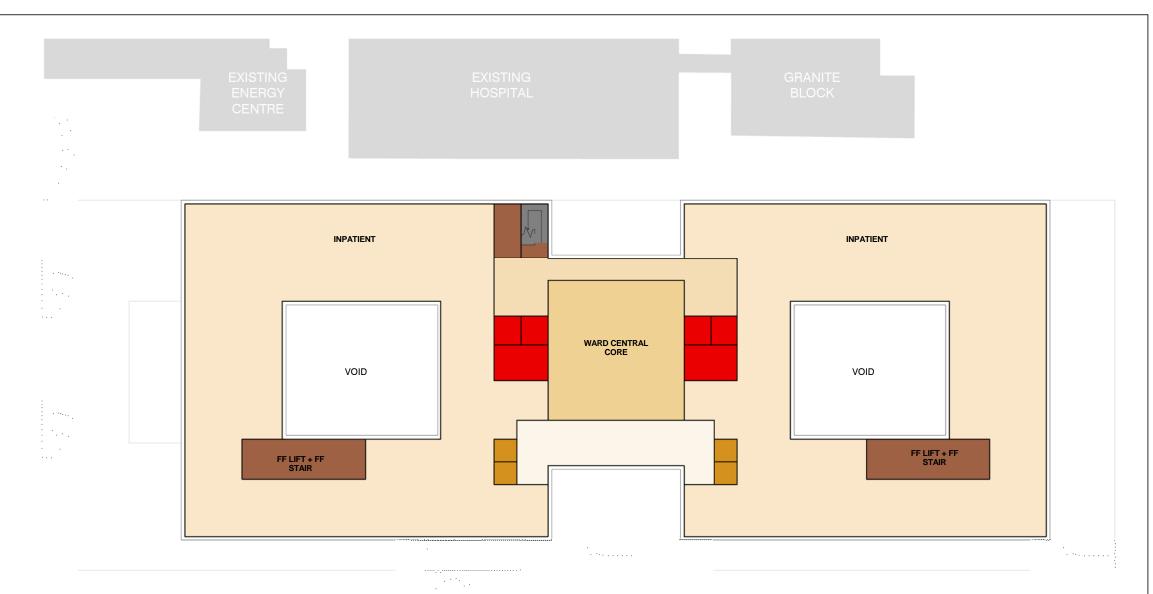
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### **INFORMATION**

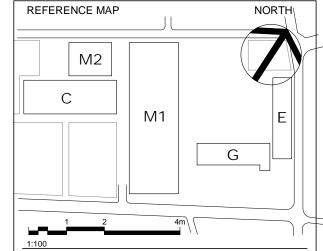
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JFH-HSL-M0-05-DR-A-1806-S2.P33

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REV	DESCRIPTION	DATE
S2.P27	Drawing Updated	21/04/17
S2.P29	Drawing Updated	26/04/17
S2.P30	Areas Updated	09/05/17
S2.P31	Areas Updated	15/05/17
S2.P32	Graphics Updated	16/05/17
S2.P33	Areas Updated	05/06/17

JERSEY FUTURE HOSPITAL (JFH) - MAIN HOSPITAL SITE THE PARADE, ST HELIER, JERSEY JE1_3QS

DRAWING TITLE

### L06 SIXTH FLOOR -**DEPARTMENTS**

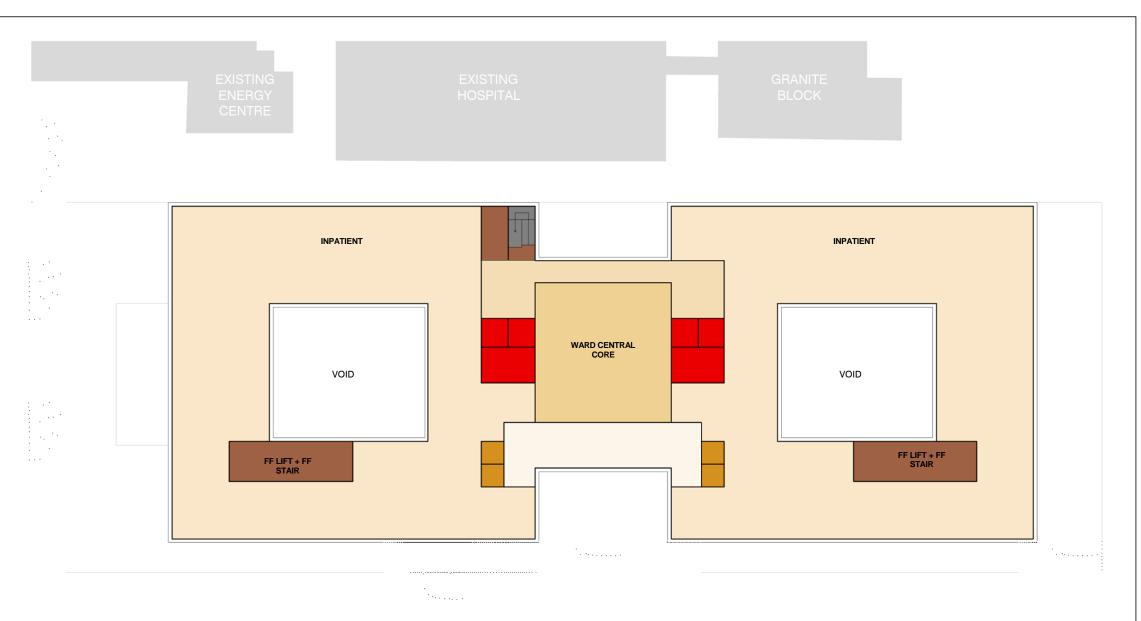
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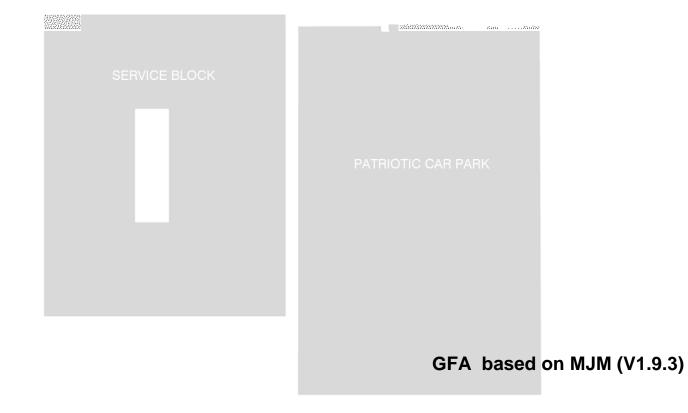
### **INFORMATION**

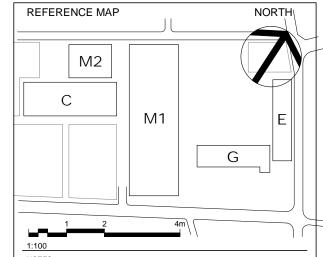
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JFH-HSL-M0-06-DR-A-1807-S2.P33

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S2.P29	Drawing Updated	26/04/17
S2.P30	Areas Updated	09/05/17
S2.P31	Areas Updated	15/05/17
S2.P32	Graphics Updated	16/05/17
S2.P33	Areas Updated	05/06/17

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DRAWING TITLE

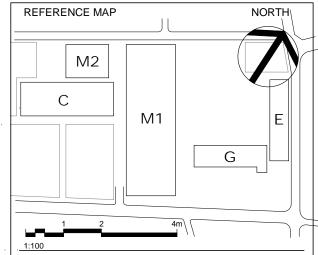
#### L07 SEVENTH FLOOR -**DEPARTMENTS**

STATUS

#### **INFORMATION**

SCALE @ A3 ORIGINATOR PROJECT # REVIEWED APPROVED 012145 JB PROJECT# - ORIGIN. - ZONE - LEVEL - TYPE - ROLE - DRAWING# - STATUS+REV

JFH-HSL-M0-07-DR-A-1808-S2.P33



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S2.P29	Drawing Updated	26/04/17
S2.P30	Areas Updated	09/05/17
S2.P31	Areas Updated	15/05/17
S2.P32	Graphics Updated	16/05/17
S2.P33	Areas Updated	05/06/17

CONSULTANT

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GREYFRIARS ROAD
CARDIFF CF10 3AF UNITED KINGDOM CARDIFF@HASSELLSTUDIO.COM T +44 29 2072 9071

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DRAWING TITLE

#### L08 EIGHTH FLOOR -**DEPARTMENTS**

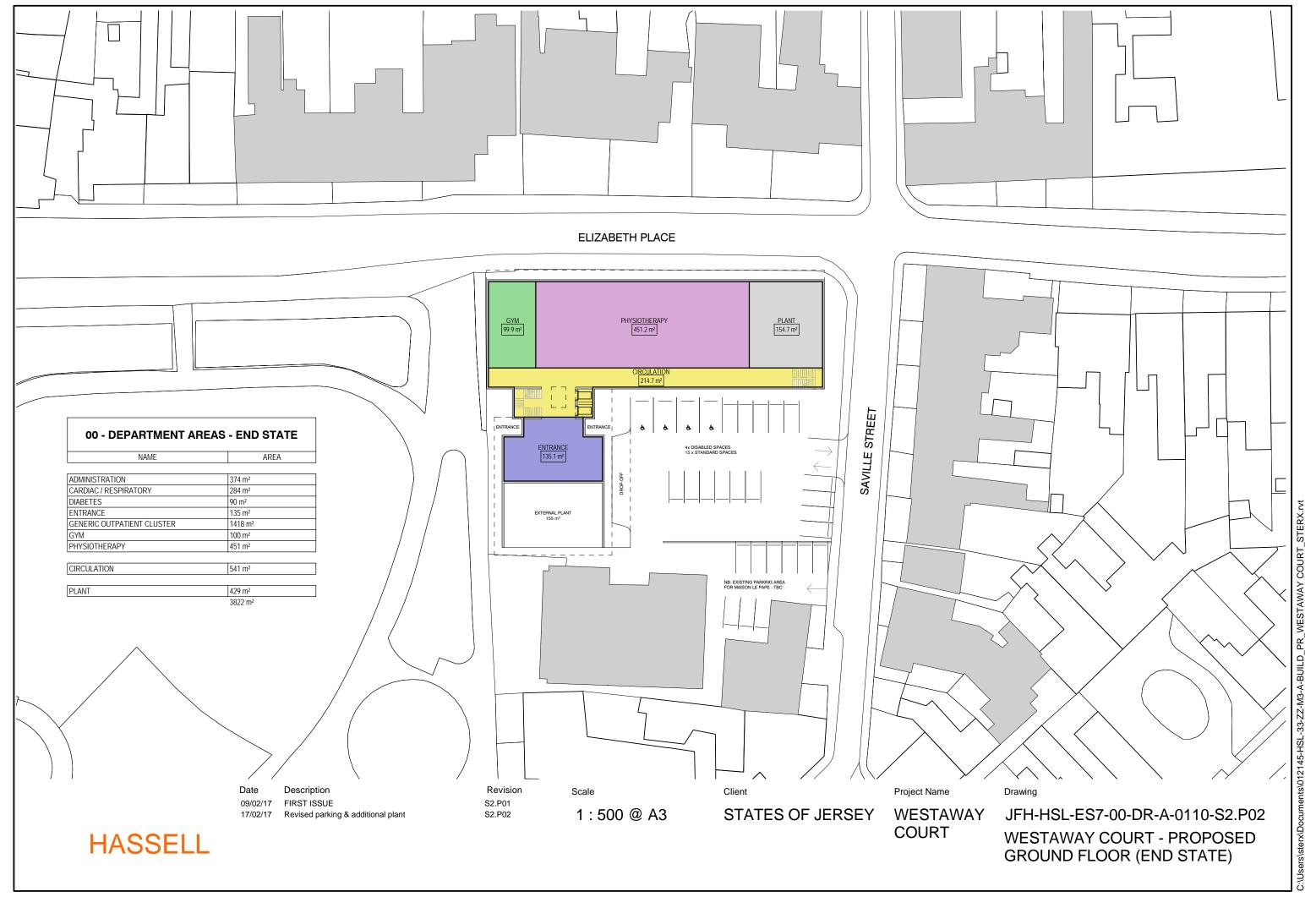
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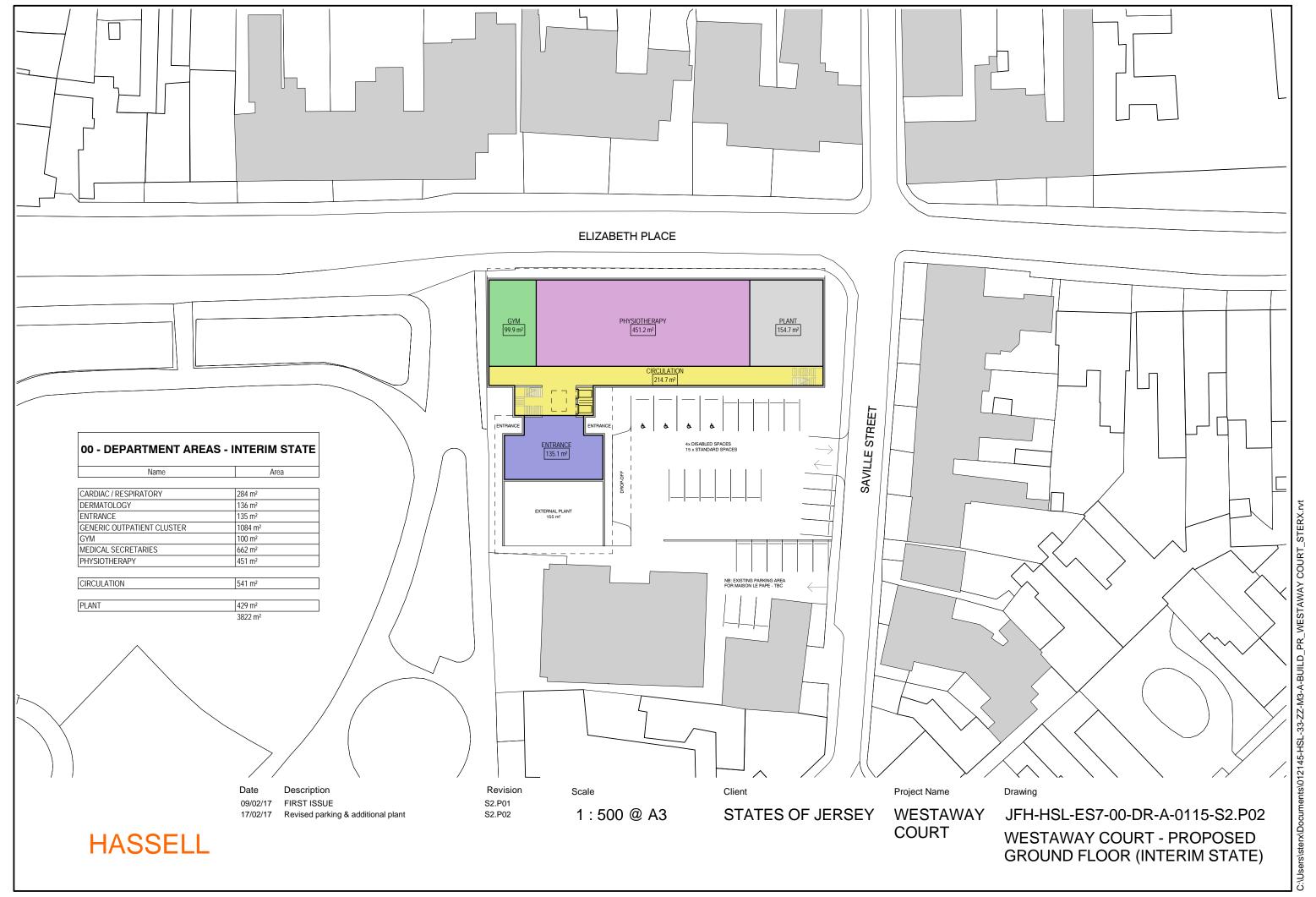
### **INFORMATION**

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JFH-HSL-M0-08-DR-A-1809-S2.P33

C:_Fevit Projects\JFH-HSL-M0-ZZ-M3-A-BUILD_PR_2_kiejm.rvt

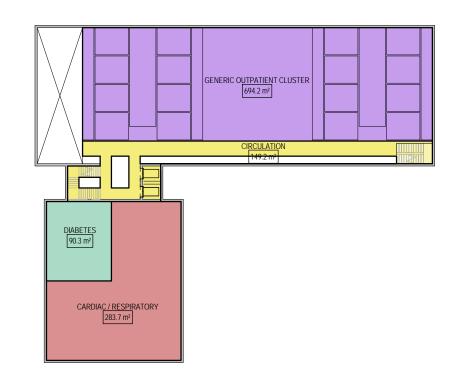






ADMINISTRATION	374 m²	
CARDIAC / RESPIRATORY	284 m²	
DIABETES	90 m ²	
ENTRANCE	135 m²	
GENERIC OUTPATIENT CLUSTER	1418 m²	
GYM	100 m ²	
PHYSIOTHERAPY	451 m ²	

CIRCULATION	541 m²
PLANT	429 m²
•	3822 m²



Date Description
09/02/17 FIRST ISSUE
17/02/17 Revised parking & additional plant

Revision S2.P01 Scale

Client

Project Name

Drawing

S2.P01 S2.P02

1:500 @ A3

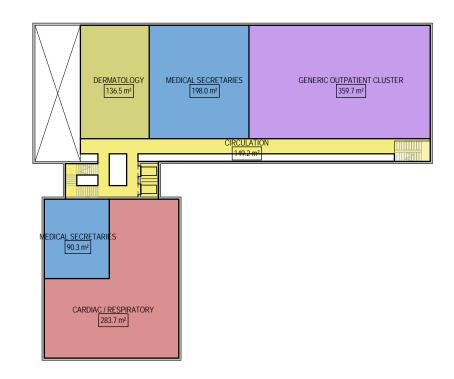
STATES OF JERSEY

WESTAWAY COURT JFH-HSL-ES7-01-DR-A-0111-S2.P02 WESTAWAY COURT - PROPOSED FIRST FLOOR (END STATE)



284 m²
136 m²
135 m²
1084 m²
100 m ²
662 m ²
451 m²

CIRCULATION	541 m ²
DI ANT	120 m²



Date Description
09/02/17 FIRST ISSUE
17/02/17 Revised parking & additional plant

Revision S2.P01 S2.P02 Scale

1:500 @ A3

Client

STATES OF JERSEY

Project Name

WESTAWAY COURT JFH-HSL-ES7-01-DR-A-0116-S2.P02

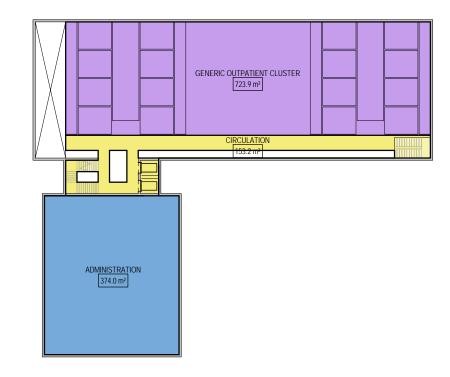
WESTAWAY COURT - PROPOSED FIRST FLOOR (INTERIM STATE)



ADMINISTRATION	374 m²
CARDIAC / RESPIRATORY	284 m²
DIABETES	90 m²
ENTRANCE	135 m²
GENERIC OUTPATIENT CLUSTER	1418 m²
GYM	100 m ²
PHYSIOTHERAPY	451 m ²

CIRCULATION	541 m ²
PLANT	429 m ²

3822 m²



Date Description
09/02/17 FIRST ISSUE
17/02/17 Revised parking & additional plant

Revision S2.P01 Scale

Client

Project Name

Drawing

S2.P01 S2.P02

1:500 @ A3

STATES OF JERSEY

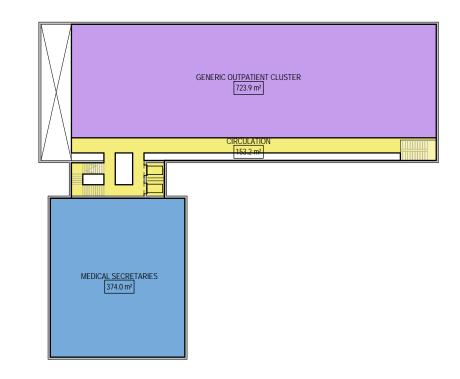
WESTAWAY COURT JFH-HSL-ES7-02-DR-A-0112-S2.P02 WESTAWAY COURT - PROPOSED SECOND FLOOR (END STATE)



CARDIAC / RESPIRATORY	284 m²
DERMATOLOGY	136 m ²
ENTRANCE	135 m²
GENERIC OUTPATIENT CLUSTER	1084 m ²
GYM	100 m ²
MEDICAL SECRETARIES	662 m ²
PHYSIOTHERAPY	451 m ²

CIRCULATION	541 m ²
PLANT	429 m ²

3822 m²



Description 09/02/17 FIRST ISSUE

Revision S2.P01 S2.P02

Scale

Project Name

17/02/17 Revised parking & additional plant

1:500 @ A3

STATES OF JERSEY

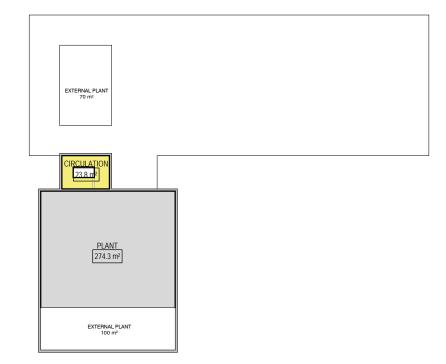
WESTAWAY COURT

JFH-HSL-ES7-02-DR-A-0117-S2.P02 WESTAWAY COURT - PROPOSED SECOND FLOOR (INTERIM STATE)



374 m²
284 m ²
90 m²
135 m ²
1418 m²
100 m ²
451 m ²

CIRCULATION	541 m²
PLANT	429 m²



Date Description
09/02/17 FIRST ISSUE
17/02/17 Revised parking & additional plant

Revision S2.P01 S2.P02 Scale

Client

Project Name

Drawing

1:500

1:500 @ A3

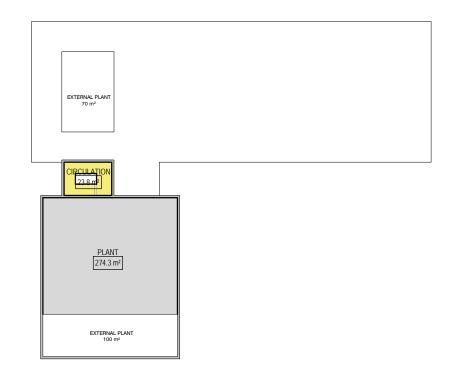
STATES OF JERSEY

WESTAWAY COURT JFH-HSL-ES7-03-DR-A-0113-S2.P02 WESTAWAY COURT - PROPOSED THIRD FLOOR (END STATE)



CARDIAC / RESPIRATORY	284 m²
DERMATOLOGY	136 m²
ENTRANCE	135 m²
GENERIC OUTPATIENT CLUSTER	1084 m²
GYM	100 m ²
MEDICAL SECRETARIES	662 m²
PHYSIOTHERAPY	451 m²

CIRCULATION	541 m²
PI ANT	429 m²
FLAINT	3822 m ²



Date Description
09/02/17 FIRST ISSUE
17/02/17 Revised parking & additional plant

Revision S2.P01 Scale

Client

Project Name

Drawing

S2.P01 S2.P02 **1** 

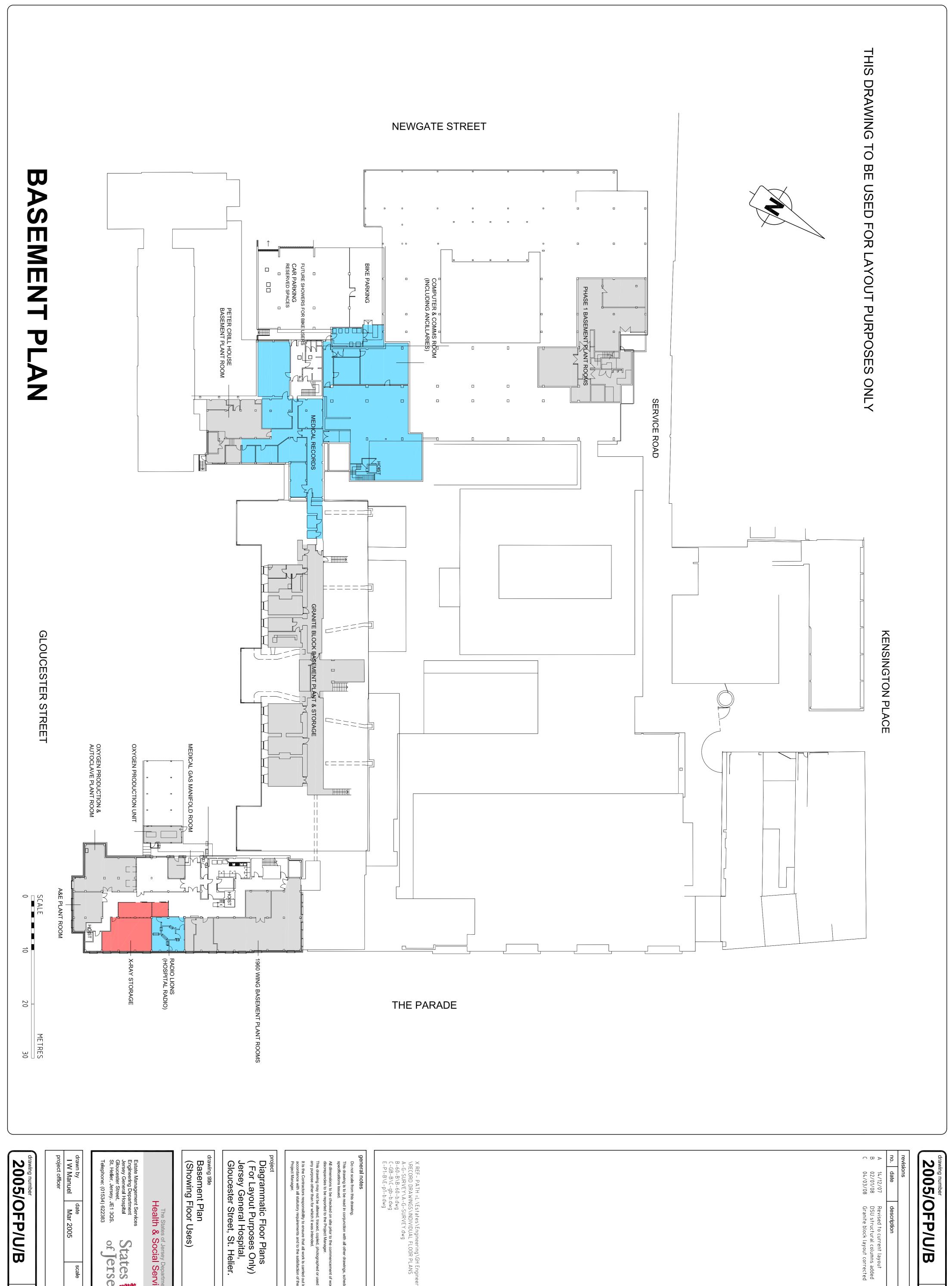
1:500 @ A3

STATES OF JERSEY

WESTAWAY COURT JFH-HSL-ES7-03-DR-A-0118-S2.P02 WESTAWAY COURT - PROPOSED THIRD FLOOR (INTERIM STATE)

# **Appendix K**

Detailed Existing Basement Drawing - Jersey General Hospital



2005/OFP/U/B

States sof Jersey

Diagrammatic Floor Plans (For Layout Purposes Only) Jersey General Hospital, Gloucester Street, St. Helier. All dimensions to be checked on site prior to the commencement of work, any discrepancies to be reported to the Project Manager.

This drawing may not be altered, traced, copied, photographed or used for any purpose other than for which it was intended.

It is the Contractors responsibility to ensure that all work is carried out in accordance with all statutory requirements and to the satisfaction of the Project Manager. Basement Plan
(Showing Floor Uses) Health & Social Services

revision

# **Appendix L**

Jersey Environmental Health Radon Protection From: Alan Irving <a.irving@health.gov.je>

**Sent:** 10 November 2014 11:42

To: Katherine Iles

Subject: Radon

Health and Social Services Department

Environmental Health, Public Health Department Maison Le Pape, The Parade St Helier, Jersey, JE2

3PU

Tel: +44 (0)1534 443712 Fax: +44 (0)1534 445773 Email: eh@health.gov.je

Dear Katherine

Re: Radon queries

Thank you for the email. The following website also should assist you:

www.ukradon.org

All of Jersey is considered a Radon affected area and we refer any queries relating to testing to the Public Health England (formerly the Health Protection Agency). Building Control are considering introducing radon protection measures for commercial building as part of changes to the Building Byelaws. The new hospital I understand will be fitted with Radon protection measures. The Environmental Scrutiny panel have produced a report considering Radon in Jersey which is available at <a href="http://www.statesassembly.gov.je/ScrutinyReports/2014/Report%20-%20Radon%20-%20Adviser%20-%208%20September%202014.pdf">http://www.statesassembly.gov.je/ScrutinyReports/2014/Report%20-%20Radon%20-%20Adviser%20-%208%20September%202014.pdf</a>

I hope this is helpful. Please contact me should you have any queries. Yours sincerely

Mr A M Irving Chartered Environmental Health Officer BSc (Hons) MSc

Direct Dial: 01534 445811

Please note my days of work are Monday - Thursday 9.30am - 2.30pm

Think of the environment...do you need to print this e-mail?

Good morning Environmental Health,
Please review and respond to email received from Katherine Iles.
Kind regards,
Environmental Protection
Department of the Environment
Environmental Protection, Howard Davis Farm, La Route de la Trinité, Trinity, Jersey. JE3 5JP

T: +44(0)1534 441600 | F: +44(0)1534 441601 | E:

EnvProtection@gov.je<mailto:EnvProtection@gov.je> | W: Error! Hyperlink reference not valid.> |

Twitter: follow<http://twitter.com/StatesofJersey>

WORKING FOR A BETTER ENVIRONMENT

Be ECO-ACTIVE, please don't print this e-mail unless you really need to

From: Katherine Iles [mailto:katherine.iles@arup.com]

Sent: 04 November 2014 13:49
To: Environmental protection
Subject: Re: Radon in new buildings

To whom it may concern,

I'm preparing a desk study report for proposed new buildings and from the geology understand radon protection measures may be required in new buildings.

The Radon section on your website states the following for new homes.....

'What about new houses?

All new houses built in Jersey must now be protected against radon, however it is still recommended that they are tested to check that the protection is adequate.'

Do you have a radon affected areas map / have a any specifics with regards to new buildings such as hospitals?

Your earliest response would be much appreciated.

Many Thanks

Katherine

Katherine Iles

Geologist / Scientist | Geotechnics

BSc (Hons) FGS MIES CSci.

Arup

4 Pierhead Street Capital Waterside Cardiff CF10 4QP United Kingdom t +44 29 2047 3727 d +44 29 2026 6548 f +44 29 2047 2277 m +44 7841 249655 Error! Hyperlink reference not valid.>

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# **Appendix M**

Indicative Location of Tower Crane Piled Base



Photo 1 (Day Care Extension to Block H) – around 2007



Photo 2 (Day Care Extension to Block H) – around 2007

The above photographs provide an indicative location of a piled base for a tower crane within the Gloucester Street car park in front of the Granite Block (Block C) at the Jersey General site.

# **Appendix N**

Gloucester St. Surface Water Outfall Plan & Section of Tunnel and Sewer

Prop. Invert Ex. Invert Chainage.(m) Levels Levels 13 124 13 017 13 082 13 237 12-900 13-028 50.000 13-073 13-136 Patriotic Place BH.4 13 - 212 110-000 13 - 165 120.000 Newgate Street Firm to stiff morange brown with traces of 130.000 13-066 The dimensions i

. = Ground

e information 0 13 029 140-000  $\Box$ 150.000 BH.3 [11] 170-000 PLAN B.H. 2 LONGITUDINAL S 180-000 13-198 190-000 13-281 m 200-000 ъ 500  $\mathcal{R}$ Asphait crushed Ex. Culvert SECTION 10 - 995 13-642 210-000 surfacing rock fill 11 - 275 | 13 - 768 220-000 230.000 13-982 240.000 7.679 14-172 S  $\leq \Xi$ 250-000 14-366 <u>BH.2</u> ਰ ਰ 14-567 260-000 ឧឧ 270.000 14-700 Parade Place 15-082 300-000 12-098 15-257 Tangent Point No. 2 303 - 378 525 6 Foul Sewer 310-000 15-523 330-000 15 528 Tangent Point No. 1 340-000 15-617 350-000 15.732 15-822 365·000 8·500 367·000 12·800 15-915 380-000 390 000 12 973 450 mm. dia G.V.C. pipe at 1 in 4.772 Contract N° 120.

DRAWN BY: M.R.

CHECKED BY: 88.

SCALE: 1 to 50/500.

REG. DRG. N° T.S. 693. STATES RESOURCES RE Plan & Section of Turnel and Sewer.

701 Beach Outfall, Plan & Section.

702 Details of M.H.No.J - Drop M.H.

703 Details of M.H.No.Z - Tide Flap/Access M.H.

704 Location Plan

1 ypical Details. Gloucester Street
Surface Water Outfall BARTLEY, B.Sc.(Eng.); C.Eng; M.I.C.E; F.I.Mun.E; M.I.W.E.S. Plan 81 B.B. CURVES INCREASED TO 200m RADIUS
2 B.B. WORKING AREA IN PARK AMENDED.
2 B.B. Level of Connel at MH2 altered
and gradient MH2 to Ch.240.009
existing sewer details added.

BETAILS

BETAILS Tunnel 8 % 1A & 1B have recently been sunk piezometers installed. And NOTES RECOVERY BO. related DIRECTOR L.B.38 S.O. And Sewer TRACED BY: M.R. Section Of F.B. **BOARD** 1981. |**X**|**X**|**C** 0 ○ JEPST

# **Appendix F-2**

Previous GI Reports

### RECORD OF BOREHOLE No:___

JERSEY ST HELIER HOSPITAL

cation : ST HELIER HOSP ntract No. : CF 669 /1121 H

be of Boring: Shell and Auger

te (started) : 12: 3:73

Borehole Dia : 8 6 6 6 Casing : 6 to 33 6

Ground Level : 32 1 ft OD.

Sheet 1 of 1

10 f 31	.u. scaj	. 12 3 13				20	ieet	1 01 1
epth	Water	SAMP	LES		2.	TRATA		DESCRIPTION OF STRATA
of axing	Fevel	Depth	Тура	No.	Legend	Depth	Thickness	
				· · · · · · · · ·	333333	G.Z.	/* a*	MADE GROUND-Tormach
		1. 5."	ם .	1 .	/	" a"	****	2" overlying compacted
								sandelone.
	٠							Medium dense light brown
				_			7: 3"	fine billy SAND with pebbles
		(N·20) 5'- 0"	۵	2		• : '	, —	below 7-6
		· ·						
		7:6.	Φ	, <b>3</b>	000	71.		
		8. 6"	٥	4	2	. 6		Loose light brown/gray
. • 1. •		(N.5) 10:00	۵	<b>5</b>			3-6.	silly SAND.
						240		
		12'. 0"-13'. 1"	U	Ø		~ ~	2:0	Firm light brown sondy very
` · · `		/3.6"	ط	7		4:0"	1	silly CLAY.
		14:0	Δ,	8		* *****		•
		(N.23) 15:0°	Q.	7			4:0.	Medium dense brown silty
		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s				. , .		dayey f.m. SAND.
		18'-0"	0	10		g: o *	2:0"	Firm to stiff grey silly CLAY
		19-0-20-2"	U	//		20-0"		11 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		20'-0"	٥	12	000			
		(N. 24) 22' 0"			200		5:0	Medium dense sandy
		22' 6"	0	/3	200			GRAVEL ( / m.e.)
					0°0	. , ,		
		25'- 0"	0	14		25: <i>o"</i>	1.6	Firm grey cilly CLAY.
		25' 6 - 26' 8"	U	15	2	26-6	1	Medium dense dork grey
		26.6	0			28'.0'		silly fine SAND.
3.0"	5'8'	28'- 0"	Φ	/7	*		1-6"	Firm grey clayey lominated
· '' ·		29:6"	D	1	` <b>\`</b> \`\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	29 . 6		SILT
		30-0-31-0"	Ü	19			1:0	Still grey slightly willy CLAY
		52' 6"	0	20				with fine grovel - below 32:6"
. •		33.6	1	2/		'6 ' ڈڈ		brown and without gravel.
		۵۰۰۵					2 0	
33' G	· /o': 5	(MAS 35'- 6"	۵	22	€.0.8	35 ' 6	"	slightly weathered very fine grained MUDSTONE.
i at of	8' 3	. Initial 2").	W					grames - 102-10 -
:							-	
		į,						
		<u> </u>		<u></u>	_11			<u> </u>

S: Chibel used for 2 hours 30-6" + 35-6" to prove bedrock.

Water added to assist in shelling, and to prevent sond and gravel from blowing.

### RECORD OF BOREHOLE No:

JERSEY :ST. HELIER HOSPITAL . Location

Contract No. : CF 669 / 1121H

Type of Boring : Shell and Auger

Date (started) : 10: 3:73

8 to 20 0, 6 to 34 0 Borehole Dia

Casing

Ground Level : 27.9 ft OD.

Sheet 1 of 1

o e		Water	SAM	PLES		T	STRATA		DESCRIPTION OF STRATA
lime	Carroa	Level	Depth	Туре	No.	Legend	Depth	Thickness	
D 3:		1				SUSSE	G.L.		MADE GROUND: 3" formes
								2:6	over 3" roadelone overlying
ļ					]		2'- 6"		granile boulders and slabs.
1			3-0"	ص ا	/	×			
٠.			(N.17) 5:0°	٥	2				Medium dense light brown .
. 1 .						×			slightly silly fim. SAND.
			7-0	٥	3			10-0"	Horizon is sark brown and
						× ×.	٠.		very wilty 7'0 10'0"
.					١,,	*			
			N. 22 10. 0°	0	4				
			12: 6	D	5		12'6"		
					'				
			15' 0'-16' 3"	U	6		**.		Soft to firm brown sandy
.]							1	6:0"	silly CLAY
.	]		16-6"	Ø	7	<b>=</b>			
			18'-6	0	В		18:6	-	Soll to firm brown/grey bondy
1000	20:0	5.6			. –	<u>×_×</u> =×			SILT. with some clay.
3.73	4	_	20:0:21:2"	U	9	I			
	20.0	6'3."	21.0	D	10		21:0		Medium dense light grey/ brown
			, ,		,,	****	23:01	2.0	sulty f.m. SAND.
•			23' 0"	<i>D</i>	11		23.0		
			25.0":26: 4"	U	12			3.0	Firm green/brown/grey CLAY.
			26: 0	0	/.5		26:0	1	
			20-0			500		2:0"	Medium dense sondy GRAVEL
			28: 0	0	14		28'. 0"		with some green/grey day bind
		.							Province
٠.		. [	30: 0 - 3/: 3"	U	15		-	4.6	Soft to firm grey   brown
			3/2 0	ص	16			1	Billy CLAY
			331 - "		17		32'6		Stiff brown billy CLAY with
			32'- 6"	О	''			1'. 6'	traces of graves.
			34' 0"	ے ہے	18		34'.0"	_ ,	. [
			N1591 35: 0"			心影	1	2 0	Hard grey elightly weathered
<del></del>			Vinitial 1/2)		j,	£.0.B	36-0"		porphydia DOLERITE
				W				-	broken with clay smears.
			1	}	*				
				İ					
			L	<u> </u>				<u> </u>	

REMARKS: ground and 1/2 hrs. 34 0"

**JERSEY** 

Location

: ST HELIER HOSPITAL

Contract No.

: CF 669 /1121 H

Type of Boring: Shell and Auger and Rotary Core
Date (started): 6:3:73

RECORD OF BOREHOLE No:

Borehole Dia

Casing

8" 6" HX

8" to 20'-6" 6 to 40'-6"

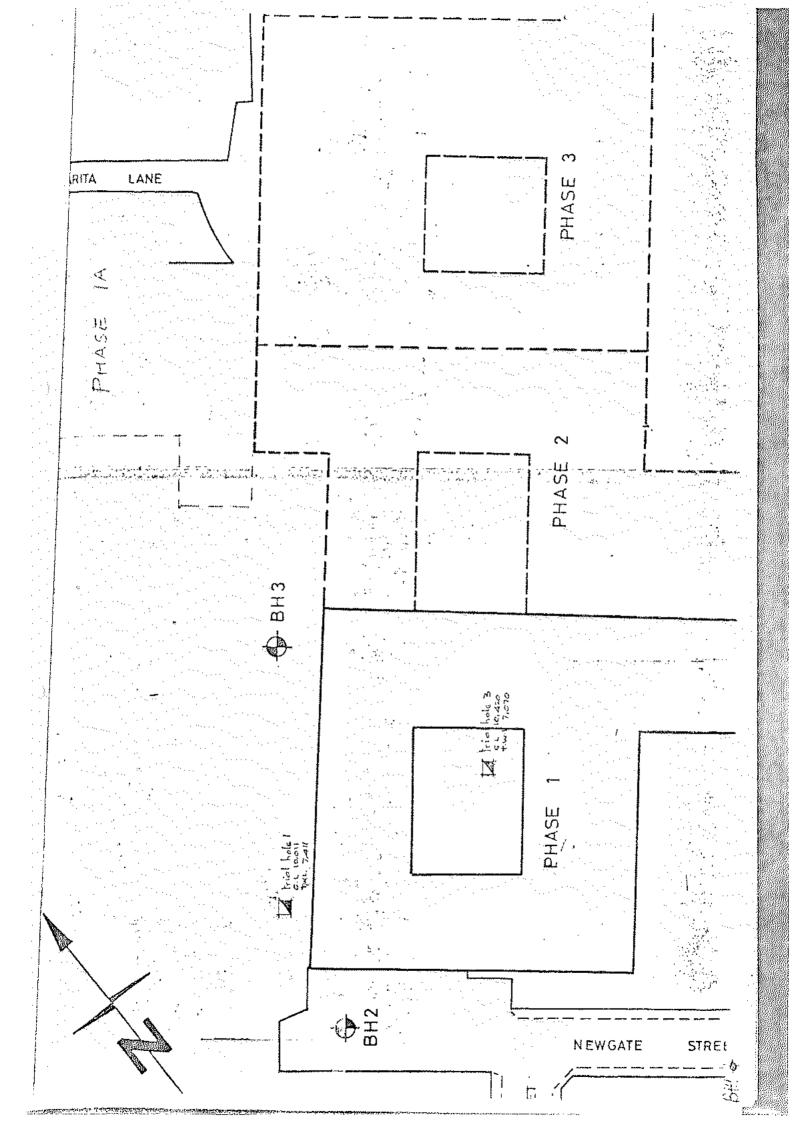
Ground Level: 34.8 ft 0.D. (10166 m 00)

Sheet 1 of 2

ĺ									
e d	Depth	Water	SAME	LES	····		STRATA		DESCRIPTION OF STRATA
Te e	Casing	Level	Depth	Туре	No.	Legend	Depth	Thickness	
د7 ،			/\a	Δ.			0.L.	/: a*	MADE GROUND: concrete ducting.
:								3' 3"	MADE GROUND: Brown band with groves and brick
	. •		A: 6' (MAI) 5'-0	о Д	2 3		4:6:		
								4'.6"	Dense light brown slightly willy fim SAND
	· . ·		9:0"	۵	4	×	91-01		
			(~.19) 10:0	D	5	×		4.7.	Medium dense dark brown cloyey silly SAND with
	•					V.		7 60	some organic maller.
			13' 6"	Ð	6	×	13:6'		
			15'0"-16'0"	υ	7			3.0	Firm brown yellow sondy CLAY
	· .		16'6	Δ.	8		16 6"		
						*		φ: <u>α</u> "	Medium dense brown/grey
			(N. 22) 20° 0°	0	9	*			silly for SAND
-	•		22' 6"	۵	10		22'6"		
			25' a"- 26': a"	Ų	"		٠	5 6	Firm to stiff light grey sondy willy CLAY
			-			y	28°0"		
			28: 0*	Д	12	3.0			Medium dense sondy  GRAVEL (I.m.c.)
			[w·23] 30' 0"			, 0,0 0,°<		A ( 0 )	GRAVEL (f.m.a)
			52% o	ص	د.⁄	200	32:0"		,
				W		<b>34</b> -		5' 0"	CLAY.
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8510-361 /	U	14	<b>X</b>		.	
		7	37. 0"	٥	/ <u>\$</u>		37.0	2' &"	Still grey/green / brown CLAY.
_			39' 6"	0	16		39 : 6 40 : 0")	r'. o ·	Dense GRANEL and cabbles.

EMARKS: Water odded to assist

> Three Trial pite dug to locate of them.



### DOREHOLE LOG

CLIENT STATES OF JERSEY

DEPT. OF PUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL

DATE 12-14 JULY 1979 GROUND LEVEL 10-30M. AOD.

BOREHOLE No 1 (Sheet 10 + 2)

SCALE 1:50

رن	propress and	casing record	de renption	SP1/	core	o <del>c</del> pth	Here'	
	12 JULY	. !						
			Made Ground and with some gravel and brick.		٠			
			y ard was rice.					
				1		-1.98	9.30	2
		rui	Mading daying broading looser	Ñ . (17)		1.17	• • • •	
			Medium dense becoming looser with increasing depth, while fine		o			,
• .		•	SAND	. <del>,</del>	3			
					grilling.	2.00	. •	
		kii		4. (10)		2.17		
	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		becoming pale grey fine and medium. SAND See Remarks 2.	1				
			SAND See REMORES 2.	!				-
	j			1			<u> </u>	1
	Smick water	rui.		H= (6)		3.17		-
	at 4 00m.		•	1		1		
	lievel ofter			1				
	isinking 4 ox	• •		4		4.17	6-30	-
	Botore waite	nil '	Medium dense orange proximising	₩ •(e)				
	HUSK 4-00		fire Sand	1	1	4.50		
	) 			-	12 7	4.80		Į.
· · .	PM After Husting in			·į	8	.]		1
	casing -at	Ì	_	T		5.51		ľ
	surface	5.15 P.M.5-G	5-80-5-85m. band of sity fine 500	n -(16	)			10
	13 JOLY		with the grave.		1		1	
	A.M. J-45	S	6.25-6.30m. band of party	:		. <b>j</b> . '{	<u> </u>	
. •			cemented silty fine sand	_		_6-30	4-00	-
			Medium dense orange mortled grey			6.65		
		6.49	fine soudy Silt with some iron-	· (12	)	0 63		
		1	situited partices. Lamitated from	*		-1		17.
			6.30-6.50m. and 7.45-7.50m. A little clayey below 7.50m.	1	† 	1		1,
		. 4	To make condend town to make	1		7 67	į	1
		7.51	1	ी भै ÷(a;	) <u>2</u> 7	ţ	1	ڒڒٳ
· . ·			Madure days a could amore walked	-	Δ.	1	2.30	1
		1	Medium dense grey green motified orange silly fine Sano and fine	, <del>ب</del>		6.30	2.00	<b>\</b>
		1	GRAYEL.	1,		5 60	$\mathbf{p}_{\mathbf{j}}^{\dagger}$	10
		8.44		4	)	. ]		[·
			Dense grey silly fine SAND and fine and mealum CIRAVEL	_		l l		10
		1		ļ			:	1 0
		_	See Remarks 2.		<u> </u>	_ = > 6	0.70	
			Continued in different strotum on Sheet	2.				
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## REHOLE LOG

STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS JERSEY GENERAL HOSPITAL 12-14 JULY 1979 GROUND LEVEL 10-30M AOD. BOREHOLE No 1 (Sheet 2 of 2)

SCALE 1:50

propress and	COSIMA		SPT/	core.	<u> </u>		<u></u>
y water level		Ge kChpt-on	RPT	sample	depth	he we!	•
	<del>!</del>	<u> </u>		1	1		<u>.                                    </u>
1	1	1		i i			i E
·   — —	·				9.60	0.70	! }
13 JULY	9.50	First gray bounded fine savay SILT	J. Can	T	9 67	0.70	6,20
		with pase grey time sand landmations,	(20) : <del>إ</del>				· .
	1	dark grey clayey silt bands, some		<b>9</b>			, ,
	<u>ج</u>	brown staining and black organic		وساانه			, , ,
	₹	inclusions. Occasional rounded fine	:	ક			
1	ن ا	oravel amond 9-60M. Becoming	1 .		10.71	-	* _ ~
	) है। <b>०</b> -इड	. Slighty clayey or increasing depth.	1.(15)	N .	$H \cdot DO$	-0.70	
	<b>F</b>	Shiff and Taminated below to 95m.	•	§ 5			
	•			Ü		*. *	·
	11-29	Very stiff grey mottled yellow grzy	- - - - - - - - - - - - - - - - - - -		11.45		
		clayey sardy SILT with strong and lyghy weathered iron-stowned	ا جيءَ يا				
	[	highly weathered iron-shirted		준			*
	i: ▼ 1つ.ラ∡	. Iraaments of meta-sillstones.	į	4	12.20	-1.90	· •
	12:24	CONTRACTOR VINE TO THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERT	, #	g 5	12.36	ĺ	7×
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		1 Hunting week near that the significant is the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the significant to the sig		drilling Zank, pio	-12.75	-2:45	
	d i3-002	fragments of META-SILTSTONES,	l	27.			つー
	ন্ত	friable below approx to este	ļ	5 17	1	.	× ×
	į	Constant	]		ĵ	į	7/
	Ĵ 13·35	Completely weathered very weak		dianord an.	- 1	1	سرد
	<i>b</i>	pale grew fine grained gravel		올ի성	i	ļ	v ,
		META-SILISTONE Programments		-इ । ब	-	Ì	~
		in a silfy clay matrix.	ļ	HÝL	_14-20	-3· <del>2</del> 0	<u> </u>
M 2-60	3.35	Moderately weathered very strong pale	ł	Nater-Fluste	į		
- JULY	AM14 55	greensh grey lightly metamorphosea	į	三 <b>「</b> ¹ ¹	1	· ·	
M 1 45	į	Chiorite rich MUDSTONE WITH COLCINE	ľ	2	Ī	į	
fore pulling		crystals, occasional pyrite and	- 1	\$	15.20	_ / 50	
अरुग मित्रस्थ	LCOACLEY	numerous calcite veins.	i		رسم ددا۔	-4-90	
P. M. 1.45							
16-19JOLY	. ]	End of boretole.		1			·
1.45	· . [	2					٠.
		Remarks		1			
		. Starter pir excavated to 0-75% depth.				1	٠.
	<b>j</b>	8.90-9.50m.	1				
	[	5. SPT records.	1	· . į	1	-	****
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		2.01 = (3) X 0 0 2 0 2 (2) A 4 (2)		. 1		i	
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		3-01-(2), 1, 2, 2, 1 9.50-(16), 7, 4, 4, 5					
		3-01 - (2), 1, 2, 2, 1 9-50 - (16), 7, 4, 4, 5 4-00 - (2), 1, 2, 1, 2 10-55-(5), 3, 3, 4, 5	وارونيات د واست		-		
		3-01 - (2), 1, 2, 2, 1 9.50 - (16), 7, 4, 4, 5 4-00 - (2), 1, 2, 1, 2 10.55 - (5), 3, 3, 4, 5 5-15 - (5), 4, 4, 4, 4 11.29 - (16), 9, 9, 8, 14		paragui ferben verrenam Lel	***************************************	deployment of territoria errowa	
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32		e add trace necessaria in contractor	***************************************		
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	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32			TYPE I MAN TO ANALYSIS OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE		
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
	100 m m m m m m m m m m m m m m m m m m	3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					
		3-01 - (2), 1, 2, 2, 1 4-00 - (2), 1, 2, 1, 2 5-15 - (5), 4, 4, 4 6-49 - (4), 3, 3, 3, 3 12-20 - (24), 32					

# BOREHOLE LOG

BOREHOLE No 2 (Sheer 1 of 2)

CLIENT STATES OF JERSEY

DEPT. OF PUBLIC BUILDING AND WORKS

DATE 14-17 JULY 1979 GROUND LEVEL 11-60M. ADD. SCALE 1:50

+C10034	progress and		de rection of	SPY/ RPT	core. sample	depth	bevel.	
	14 JULY							
			MADE GROUND - sand with					
			some gravel and brick fragments.					
				. •				
						1.20	10-40	
		Г					10 , -	
			MADE GROUND -yellow brown very			•		192
			silly fine sand with some poorly		ā	L 1.BO	7.50	77.
			cemented pairthes.	Å·67)	=	1.99	٠.	
		rui	MADE GROUND-pale yellow grey	선 177)	ਤ	İ		///
	ļ		and brown mothed fine and			1		$\times \times$
	Dawy below	1	medium sand.			200	ಕ.ಕಂ	XX
• •	3.30m.	ļ <b>-</b>				1	ļ	7.5.
	Smock water	rul	Loose pale yellow fine SAND.	Ψ • <del>(2</del> )		3.04		
	ar 3.97	141		TW		<del> </del> 3.30	8.30	-
	level after		Medium dense yellow and brown				<u> </u>	
	striking 3-97		mediom and fine SAND.			3.77	•	
, .					<b>A</b>	4 00	7.60	-
٠.	P. M. 3.97	nil	Loose brown silly medium to fine SAND.	N (5)			•	
	! .		TRANSITIONAL	7 50		4.50	7.10	
٠. ٠	16 JULY	[	Mad days provide oral is pieces					1
	A.M. 3.94	1 1	Med dense greenisk grey in places mortizd orange poorly laminated fine					٠ <u>-</u>
·. ·		nil	SOUNDER CHANGE BOOK GLEST	l Alimenta	1	5.02		** X
	}	10.	lammations and bands of claye,					
		1	silf. Some from nodules and			5.57		Y
٠.	1	i iin	staining.	<del>- (</del>	1			7
						6.00		~ * * *
		5.86	Becoming less sandy with increasing	4			}	YX
			depth.	1	•	6.56		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
		5.86	TRANSITIONAL	1.(12)	民,	6:56	4.90	)    -  -  -
٠.			Blue arey mottled yellow poorly		- 0	7.00	,	Y , ,
			laminated fine sandy SILT with	1				* *
		6-86	some from staining along borninations.	İ	i	1		
			Clayey between 7.40 k and B. 20m.	J		7.5€	1	,
٠.		6.86	Band of yellow cemented silty fine	4-(12)	4	İ		21.
· .			sard at 7.90m.	ì		8.04	1	¥. ±
		7.56	·		1			
					4	L8:50	3-10	-
<del>-</del>			Continued in different stratum on Sheet 2.		1	1 .	1	
			Prince Hills Westerney and a sender and an an employee and active security and granted	1				-
					1			i i
		1			-			1 .
427						1	1	
2								
100		. مذراء						
			ه د د موسید ده د	. Company	1 3 3 3 Y	·	],	
W-15,00	A COMPANY	All Control of the Control	e, open-drive or prepared from drill core		CEL	IOB No.	FIG	• • • • •

## SOREHOLE LOG

CLIENT STATES OF JERSEY
DEPT. OF RUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL S.TE

DATE 14-17 JULY 1979 GROUND LEVEL 11-60M. AOD. SCALE 1:50

BOREHOLE No 2 (Sheet 2 of 2)

оюду	progress and	٠ .	aes⊂nptio∩	SPT/	core.	depth	Se vei	
						_ B 50	3 10	202
	16 JULY	7.86		14 (41)			j	
		1.00	Dense yellow silly fine SAND	1				$\triangle \mathbb{Z}$
	, a trace t		and fine and measure suppregular		<b>₽</b>		. 1	<u></u>
			GRAVEL WITH a little subrounded		drilling 0-	9.40	. į	,
			gravel.		हे ह	9.80	į	250
						9.95	į	7
		7.79		N (35)		10.20	1.40	1000
			The Comments					
		·	Firm pale grey silly fine SAND		8		į	
. ·			with arey hine sandy sill laminations becoming time sandy		· •	10.72		
		10-72	SILT with some sandy laminations,					
	1	انا	with occasional organic patches.	1	1	11:15	O-45	¥
		D 10-72	TRANSITIONAL	₩·(Œ)	[	11.60		
· .	Before water	, ,	T IKWADII IDAWT	1	준.	11.75	•	
	Hush - Dry	153	Firm grey laminated very silly fine	*	1	12.15		200
		12.01	Spardy (LAY WITH OCCASIDAD)	-r <u>v</u> =(100)	! !	12.20	-0-60	* * * ×
	<u> </u>	12.30	ordanic patches. A little rine	_ ` '		12,30		2
	Ì		aravel below 11-80m. Becoming		drilling			· •
	P. M. 3.64	P.M. 12:45	a greenisk grey sandy SILT		₹ ₹			2
	17 JULY				8			<b> </b>
· · · .	A.M.3-60	12.95	· · ·		dumond core	S		
			Shong moderately weathered grey to greenish grey META-SILTSTONE.		12 17	3	٠.	¥
	Before pulling		from -starred along most		1 2 1			y
	CORING 3-94	? [	discretifuities. 3 joint sets	}	3	4		
			recognisable, one vertical, one	Ì	1 . <b>1</b>			۲
	İ		60° dip. loirly separation approx		2			\ \v
			lorunt, one 75 aip, joint separation.	· •	à			1
	P.M. 5-7	8	approx. 40 mm.		Water-flush			) ×
		122-22	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	1	1	TE-01	-3.4	
	18-21 July	Y TECHNOLOGY	A little clay snearing or joints			1		
	B-17		above 13 som. Some joints open				1	
		1	to 2 mm. or calcite infilled,	•				1
			penerally < 1 mm.					
			Numerous calcille veins.	1				
			End of borehole.		•			}
			Remarks.  II. Sharter pit excavated to 1-00m depth.		. ]			
			2. SPT records.					
			1.83-(5),5,44,4 7.40-(5),4,5,4;					
			288 - (4), 2322 8.44 - (6), 9,10,10,1		. }			
			3.97-(2),1,1,2,1 9.79-(5),9,12,B,1					
•	The second		5.42-(4) 3,4,4,3 11-12-(6),3,3,4,					
			6.40 - (5) 4,3,4,4 12.00 - (6),24,26	-[				
			3. Piezometer installed: tip at B.Gom. response zone B.10 - 9.10m.	-			1	{
			trakuse roug and - Sugar		1			
				<u>_l</u>			<u> </u>	<u></u>
September 1	CONTRACTOR OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE	shed same	ole, open-drive or prepared from drill core	;	,	JOB.No.	FIG	

### BOREHOLE LOG

CLIENT STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS

SITE

JERSEY GENERAL HOSPITAL

DATE 18-20 JULY 1979 GROUND LEVEL 10:00M. AOD

BOREHOLE NO 3 (Sheer lof 2)

SCALE 1:50

⊋≠0 <b>/</b> 00	progress and water level		σεεςτώτι <del>ο</del> υ	SPT/ RPT	core, sample	<b>G</b> epih	Sevet	
	المال الكا				<u> </u>			
			MADE GROUND - Sand with some					
	i		gravel.	. *.				
			<u> </u>					160
				<u> </u>				K
						-125	6.75	
				T		1.42		-
		rùl	tat at a material language	r (15)				•
			Medium dense pale yellow grey		5			12.60
			fine Sand becoming white below 1-60m.		drilling grant		٠.	' . '
			pack t-point.		8	2.49		13.5
		rú(		+ (2)				
1		1970  		1			<b>-</b>	
1			Loose white fine and medium SAND.			• •	7.∞	1
	Dough below					3.20		
	3-20FL	[	Loose brown fine and medium Sand	! ! T		3.49		> -
		.5·20	with occasional dark brown silly	H = (6)				
			patthes.			4.00	6.00	
			Crompe brown silly medium to fine		•			1
			T SAND.			- 4·25	5.75	TV.
			TRANSITIONAL J					÷ .
		4.28	Medium dense blue group poorly	į	8 1	4.80	5.20	* -
			laminated very silky fine Sans.	<u> </u>	8			l'v
			TRANSITIONAL	{ !				Ţ,
Ì		4.28	<u> </u>	4 : ((5)		5.36		, v
		•	Firm blue arey mothed uslow laminated hine sandy SILT with	I				z " w
		į	some iron-stational along levels.			ေသ		* * ·
		6.00	5-60 -5-80m. Wer sill pour his		•	w. W		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
			extensive iron-staining.					1540
				1,	-	6.56	٠.	Į,×,
		6.00		r =(13)				1. Y
			Breakly war blue and clause from	*				J
		7:36	Becoming more blue and clayey from 7.10-7.20m.		_	ļ	i I	J = 1
		/ 26	7-10-7-2016.		<u>Z</u> .	7-36		Y.
				<u> </u>				Ĭ,
			The same of the Control of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the Same of the		. *	77.78	3:33	
	Smick water	1	Dense yellow silly fine SAND with some fine gravel.	4.(35)	A	+6:36		FO
	or 8.26 Level after	7.36	Some time graves.	T		8.25		10
	striking 6-00	1	Dense to medium dense grey becoming	[	Ø	<b>6</b> ∙65	İ	15.0
	1 2 2		brown silly Sand and him and		<b>!</b>	0 03	<u> </u>	c ?
L	_1		medium subrounded to subangular			9.00	1.00	
Γ-		T	GRAVEL, strongly ironstained at	1		[		
	Andrea 1		8-60 m. Occasionally subrounded					]
			coarse gravel.					
								l
	The second of		Continued in different stratum on Sheet 2.					
	J • 1				1			1
*				-	-		Ì	
Total .	4 E	] ;-	•				ļ	
		Bar.	•	1			ļ ·	
A. O.L.	and the Philipper to seem	aprobational de la companya de la companya de la companya de la companya de la companya de la companya de la c	el open-drive or prepared from drill core	<del> </del>	-	OB No.	FIG	<u> </u>

## OREHOLE LOG

LENT STATES OF JERSEY
DEPT. OF PUBLIC BUILDING AND WORKS

JERSEY GENERAL HOSPITAL

18-20 JULY 1979 GROUND LEVEL 10-00M AOD.

BOREHOLE No 3 (Sheat 2 of 2)

SCALE 1 50

<b>-</b> ФБУ	progress and water level		de #chation	SPT/ RPT	core eample	depin	level	
	WAIG! HEVE	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			<del></del>		1	
1	İ							
	:						i	
	•						-	
- 1				.		1900	1.00	I STATE OF THE
	18 JULY	9.00	Firm orange orawn silky fine SAND	3, 120		9.16	1	Sec.
	P.M. 3-26	PM.9 20	(100mm) becoming blue grey laminated	4.62	· <u>ह</u> '			
	דיוער פו		slightly clayey fine sandy SILT with		<u> </u>	9 55	1	
	A.M. 3:40		more than one includes and		י ש	9.75	į	_1 _2
			black organic inclusions,		ω <b>I</b>	10.00	Ì	
		9.20	9.75-9 BSM. very wer sill bound,		203		- 40	٧ - ٧ - ١
			_ becoming very silly fine SAND _ r	-ţ	· .	10.40	-0.40	<u>,`</u> =`:=`:
٠.		15	between 10 00 and 10 20 m.	N: - (14)	_	10.55		<del>-</del>
		F 3-20	TRANSITIONAL /	4,000	ρīg	10.80	i	
•		£ 11-∞	Shiff blue grey laminalted very silty	┪	<b>5</b> 1	11.00	- 1.00	~ *
		K)	CLAY WITH OCCOSIONAL SUPPOUNDED		drilling			,,,,,,,
		K.	Fire gravel		के हैं			 سر با _ا سر
	j		1		2 1			مست مرار دا
	ļ		Highly weathered rock fragments in		8			, x
		*	a silfy CLAY.		ā			
	P. M. 3.60	PMIZO	Highly weathered strong dark grey,		chomorto		Ì	x '
	20 JULY	1	in places laminated, lightly		S			1
	A.M. 3-60	•	metamorphosed MUDSTONES with			<u>.</u>		ļ. Ÿ.,
	Before posting		class smeather on some wint haces.		3 .	] [		
			Becoming grey META-SILTSTONE.		7			X
	meng 3-60	1	moderately weathered and massive		Mer. Aust			
	P.M. POC	12-01	1 1 .		31	13.50	-3· <i>5</i> 0	*
<del></del> :	1	TECOVERE	most wint surfaces Seaton sets				٠.	
٠.,			of high angled joints. Average					
			separation 200-300 mm.					·
			Becoming dark grey and more					} ·
			fine grained below 13 00m.					
			Laminated in places with				•	
			occasional banas including					] .
			pyrite crystals.				· ·	
			!   " " "					1
			Bedding approx.10° dip.		1 .			
	**********		<u> </u>	.		· [ - · · · i		
	***************************************		End of borehole.					
٠.	1		Remarks.					
٠. `			1. Starter pit excavated to 0 7Em depth.			.		
			2. SPT records.			·		
			1.33 - (5),4,4,4,3 6.40 - (4),3,3,3,4					1
	1		2-33 - (4), 2, 2, 3, 2 7.60 - (8), 9, 8, 8, 10					
	January States		3-33-(2),1,2,1,2 9.00-(6),8,9,4,4					1
		•	5.20 - (4), 3,4,4,4 10.40 - (6), 3,4,4,2	5				
			3. Piezometer installed: Yip at 13 com.					1
			response zone 12.50 -13.50m.					}
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-000		20 Que -	le open-drive or prepared from drill core	- K-356/65	<del></del>	JOB No.	<del> </del>	URE

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PHASE IB - GENERAL HOSPITAL - JEF EY C.I.

Geomarine Borehole No. Les Ruettes, La Grande Route de **Borehole Log** St Jean, St John, Jersey, JE3 4FN Tel: 01534 856566 GEOMARINE BH₁ Email: enqueries@geomarine.je Sheet 1 of 2 Project No. Hole Type Jersey General Hospital, Main Project Name: Co-ords: 564726.84 - 5448673.17 Theatres Upgrade SI CN 1343 ВН Scale Location: St Helier Level: 13.00 1:50 Logged By 07/03/2014 - 08/03/2014 Client: **Property Holdings** Dates: **KMS** Samples and In Situ Testing Water Depth Level Well Legend Stratum Description Strikes (m) (m) Depth (m) Type TARMAC 0.10 12.90 DRILLERS DESCRIPTION: TYPE 1 (MADE 0.30 12.70 GROUND) 0.50 12.50 DRILLERS DESCRIPTION: FILL comprising bricks, concrete, etc. (MADE GROUND)
DRILLERS DESCRIPTION: Orange coarse 0.80 12.20 SAND. (BEACH DEPOSITS?) Orange brown gravelly SILT. (BEACH DEPOSITS?) 1.20 N=6 (1,1/1,2,1,2) 1.20 - 1.65 SPTL 1.45 11.55 Grey-white fine SAND. (BLOWN SAND) 2 2 40 10.60 Grey brown laminated sandy SILT. (ALLUVIUM) 2.70 N=10 (2,2/2,3,3,2) 2 80 10 20 SPTL 2.70 - 3.15Grey mottled brown silty SAND. (ALLUVIUM) 3 3.25 9.75 Green grey sandy SILT. (ALLUVIUM) 3 55 9 45 Green grey laminated SILT. (ALLUVIUM) 4 4.05 N=13 (3,3/4,2,3,4) SPTL 4.05 - 4.50 5 5.45 N=9 (2,1/2,2,3,2) 5.45 - 5.90 SPTL 6 7 7.15 N=16 (3,4/4,4,4,4) SPTL 7.15 - 7.60 8 8.69 N=22 (4,6/6,5,4,7) 8.75 4.25 Grey silty cobbly GRAVEL. Gravel is medium to SPTL 8.69 - 9.14 coarse, sub-rounded Cobbles are rounded. S 9 Gravel is of mixed lithology becoming a weathered Jersey Shale with depth. (ALLUVIUM)

Remarks

Ground level is arbitrary level. Water strike at 4.05m rising to ground level after 30 minutes. Borehole backfilled with grout on completion.



Continued on next sheet

10

Geomarine Borehole No. Les Ruettes, La Grande Route de **Borehole Log** St Jean, St John, Jersey, JE3 4FN Tel: 01534 856566 GEOMARINE **BH1** Email: enqueries@geomarine.je Sheet 2 of 2 Project No. Hole Type Jersey General Hospital, Main 564726.84 - 5448673.17 Project Name: Co-ords: Theatres Upgrade SI CN 1343 ВН Scale St Helier 13.00 Location: Level: 1:50 Logged By Client: 07/03/2014 - 08/03/2014 **Property Holdings** Dates: **KMS** Samples and In Situ Testing Water Depth Level Well Legend Stratum Description Strikes (m) (m) Depth (m) Туре Results 10.10 N=47 (6,9/8,9,11,19) 10.21 2.79 Grey blue rock recovered as medium to coarse 10.10 - 10.55 SPTL angular gravel of rock. 11 12 12.67 0.33 End of borehole at 12.67 m 13 14 15 16 17 18 19 20

Remarks

Ground level is arbitrary level. Water strike at 4.05m rising to ground level after 30 minutes. Borehole backfilled with grout on completion.



GEO	MARINE S	St Jean, S el: 01534	es, La Grande Route de t John, Jersey, JE3 4FN			Tri	al Pit Log	Trialpit No <b>TP1</b>
Desis			Hospital, Main Theatre	- Projec	nt No		Co-ords: 564730.80 - 5448668.93	Sheet 1 of 1 Date
Project Name	: Jersey (	e SI	nospitai, iviairi Trieatre	CN 13	343		Level: 13.00	08/03/2014
				10			Dimensions 0.4	Scale
Locati	on: St Helie	r					(m):	1:25
Client:		/ Holding			ı		Depth 0.50	Logged GW
Water Strike	Sample Depth	Type	n Situ Testing Results	Depth (m)	Level (m)	Legend	Stratum Description	
> 0)	200	.,,,,	. toodito				TARMAC	
				0.10	12.90		BACKFILL - TYPE 1	
				0.25	12.75	*********	CONCRETE FOOTING	
							@ 0.25m Concrete footing protrudes 250mm from the v	vall.
				0.50	12.50		End of pit at 0.50 m	
							·	
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Remarks: Trial pit to identify foundation of retaining wall. Ground level is arbitrary level.

Stability: Good



		Geomarine Les Ruettes	s, La Grande Route de							Trialpit N	No
GEON	MARINE	St Jean, St Tel: 01534 8	John, Jersey, JE3 4FN			Tr	ial P	it Log		TP2	
				ļ						Sheet 1 c	of 1
Project Name:	Jersey Upgrad	General H	ospital, Main Theatre	S Project	t No.			64743.02 - 5448	676.87	Date	
ivaille.				CN 13	343		Level: 1 Dimensions	3.00	0.4	08/03/20 Scale	
Location	n: St Heli	er					(m):		0.4	1:25	
Client:	Proper	ty Holdings	3				Depth 1.20	0.5		Logged GW	d
e a	Samp	les and In	Situ Testing	Depth	Level			_		ı	
Water Strike	Depth	Туре	Results	(m)	(m)	Legend		Stratum D	escription		
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				0.10	12.90		BACKFIL	L - TYPE 1			
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				0.95	12.05		<u> </u>				-
				0.93	12.03		CONCRE@ 0.95 Cd	TE FOOTING	es 250mm from wall.		1 -
				1.20	11.80						-
				1.20	11.00			End of pit	at 1.20 m		-
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Remarks: Trial pit to identify foundation of retaining wall. Ground level is arbitrary level.

Stability: Good

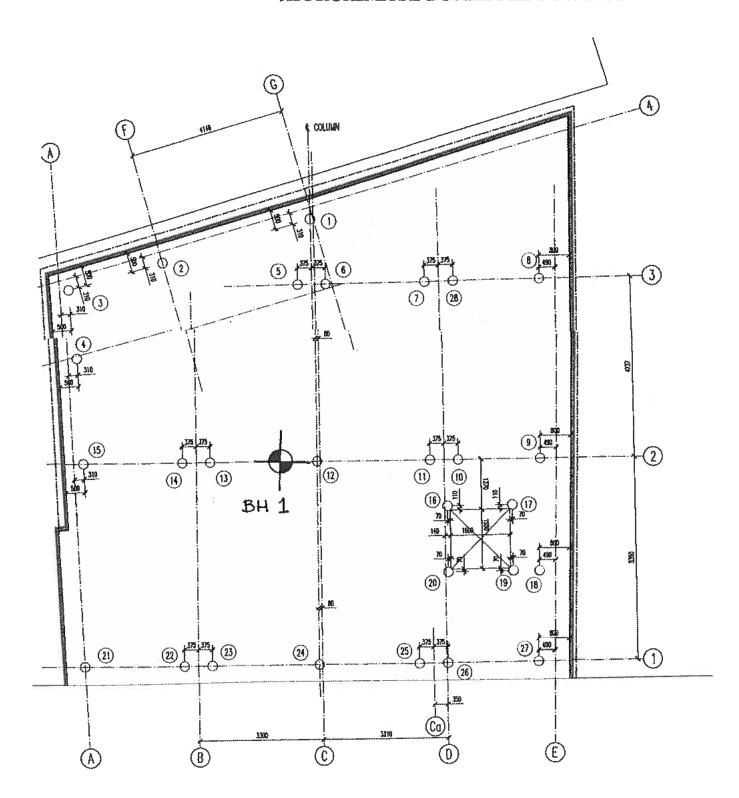




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#### APPROXIMATE BOREHOLE POSITION



PILE LAYOUT.

Amplus Ltd Foundation and Geotechnical Specialists

Boring Method Twintech TD308	Casing Diameter		Ground	Level (mOD)	Cilent Tillyard for 18 the Parade Limited	Job Number 0948
	Location as site plan	· .	Dates 11	1/09/2006	Engineer Beaumont Structural Consultants	Sheet 1/1
Depth (m) Sample / Tests	Casing Water Depth Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend
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randas robe hole drilled using a Twintech robe hole drilled using 110mm au 0.46m Refusal: presumed weathe to ground water strike using this m	1308 drilling rig gers to refusal at 10 red rock head and r	).46m bgl end of probe hole			Scale (approx)	Logged By GW

·····	1PLU	·	·····		Specialist		Site 15-16 The Parade, St Haller, Jersey	Borehole Number P2
Boring Met Twinlech Ti		1 '	Diamete Omm cas	r ed to 9.90m	Ground	Level (mOD)	Client Triyord for 18 the Parade Limited	Job Number 0948
		Location es	n site plan		Dates 11	1/09/2006	Engineer Beaumont Structural Consultants	Sheet
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (th) (Thickness)	Description	Legend &
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emarks obe hole dri	lied using a Twintech	308 drillin	g rig		F***		Scale (approx)	Logged By
oe noje dri 10m Refusai ground wat	lled using a Twintech lled using 110mm au i: presumed weathere ler strike using lbis m	gers to refu ed rock hea ethod of b	usal at 9.: ad and er oring.	90m bgi nd af probe hole	· .		(approx)	GW GW
			-				Figure No.	
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Location as site plan  Design Confidence Structural Consultants  Find Records  Design Confidence Structural Consultants  Find Records  Design Confidence Structural Consultants  Find Records  Design Confidence Structural Consultants  Description  Laged  Description  Laged  Description  Laged  Description  Laged  Description  Laged  Description  Laged  Description  Laged  Description  Description  Laged  Description  Description  Description  Laged  Description  Description  Description  Description  Laged  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  Description  D	AM	IPLUS	SLT	Poundati	on & Geo Specialist	otechnica) s	Site 15-16 The Parade, St Heller, Jersey	Boreho Number P3
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Accept the design of the motion and grey sandy CLAY/SILT  7.00  Firm to still brown gravely CLAY  (1.00)  3.00  Soft to firm occurs and grey singly sandy CLAY  (1.00)  7.00  Firm to still brown gravely CLAY  (1.70)  9.70  Complete at 6.70m  Scale (Approx)  Scale (Approx)  Scale (Approx)  Scale (Approx)  Scale (Approx)  Figure No.	Depth (m)	Sample / Tests	Casing Water Depth Dopth (m) (m)	Field Records	Level (mOD)	Dapth (33) (Thickness)	Description	Legend
obe hole drilled using a Twintech 308 drilling rig obe hole drilled using 110mm augers to refusal at 9.70m bgt 70m Refusal: presumed weathered rock head and end of probe hole oground water strike using this method of boring.  Figure No.						(0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0.50) (0	Made Ground  Loose medium dense light brown SAND  Soft to firm brown and grey sandy CLAY/SILT  Firm to stiff brown gravelly CLAY  Firm to stiff brown and grey slightly sandy CLAY	Legerd
obe hole drilled using a Twintech 308 drilling rig obe hole drilled using 110mm augers to refusal at 9.70m bgt 70m Refusal: presumed weathered rock head and end of probe hole oground water strike using this method of boring.  Figure No.	THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P				TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TATAL TA			
Figura No.	Remarks robe hole di robe hole di 70m Refusi o ground wa	rified using a Twintech rified using 110mm au at: presumed weathen ater strike using this w	a 308 drilling rig gers to refusal at 9 ed rock head and setbod of boring	9.70m bgt end of probe hole				
0948.F3	л даацло wa	ow suike using Mis n	reindo of boring.		:		Figura No	<b>9.</b>

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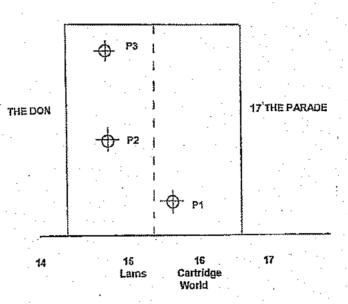
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SPECTRUM



THE PARADE

Amplus Ltd
Foundation and Geotechnical Specialists



Boring Met Fraste PL R			Diamete			evel (mOD)			Job Numbe	
Fraste PL K	19	11	3mm cas	ed to 8.90m	9	9.80	Regal Construction (Jersey) Ltd		0762	
		Locatio	n site plan			01/2007- 01/2007	Engineer Peter Brett Associates		Sheet 1/2	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	(mOD)	Depth (m) (Thidkness)	Description		Legend	
					99.56	(0.04)	CONCRETE		Trimbia.	
					99.40	(0.16)	Hardcore		160	
							Very loose to loose brown fine to medium SAND ar gravel	nd little		
20-1.70	X 0.22			12/01/2007:0.00m		(1.80)				
20-1.65	SPT N=4		DRY	13/01/2007:DRY 2.1/21.1						
70-2.00	X 0.00		DIVI	-, 114, 1, 1						
00-2.23	X 0.00				97.60	2.00	Soft dark brown sandy SILT			
23-2.50	X 0.76					(0.40)	Soli dan arown sandy SICT		3.0	
50-2.95	SPT N=10	1.90	DRY	2,2/3,2,2,3	97.20	2.40	Soft to firm brown slightly sandy SILT			
50-3.50	X 0.53					(0.60)				
					96.60	3.00	Soft to firm blue grey slightly sandy CLAY/SILT		222	
									-	
50-3.95 50-4.00	SPT N=3	3.40	DRY	1/,1,2		-			-	
.50-4.00	X 0.50	4.00								
00-4.40	U 0.40 X 0.55	4.31	2.83	12 blows		-				
						(3.30)			200	
						,,				
00-5.45	SPT N=5 X 0.50	4.31 5.92	3.95	1,1/1,1,2,1		-				
					1					
5.64					Ė					
.00-6.50	X 0.74									
	en# 11.05				93.30	6.30	Dense blue grey very clayey fine to coarse GRAVE	L	-	
.50-6.95 .50-7.12	SPT N=36 X 0.62	6.20 6.75	3.06	1,2/5,9,10,12	1					
					1	/1 600				
12-7.67	X 0.00				1	(1.50)			-	
					-				-	
67-7.75 75-7.76	X 0.00 X 0.00	7.30		13/01/2007:3.27m	91.80	7.80				
76-7.80	X 0.60			131011200113.27111		_	Very dense brown clayey sandy fine to medium GR	AVEL		
Remarks tarter pit ex xploratory h	cavated by hand from note drilled using the om 1.20m - 9.13m	n ground le Fraste PI i	evel to 1. Rig	20m bgl				Scale (approx)	Logged By	
ry drilling frock core dr 70 drilling f	om 1.20m - 9.13m illing with water flush rom 4.00m - 4.40m -	from 9.13	m - 10.23	7m				1:40	MRW	
round level	s are not Ordnance	Datum						Figure N	0.	

AIV	B & Evad	ه هسته ده	الكنبت الكنبت	stri 18 - 44	حسم	Specialists Specialists Site Kensington Gate Car Park, St Helier, Jersey					
Boring Met			i	Diamete 3mm cas	r ed to 8.90m	Ground i	Level (c 99 60	nOD)	Client Regal Construction (Jersey) Ltd	Jo N:	
			Locatio	n site plan		Dates 12/ 15/	/01/200 /01/200	7- 7	Engineer Peter Brett Associates	Si	
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mQD)	Der (m (Thick	oth i) ness)	Description	Leg	
7.80-8.22 7.80-8.25	X 0.00 SPT N=	:52	7.80	4.90	3,4/7,15,12,16		- (	0.50)	Stratum as above		
9,22-8,33 9,33-8,38 9,38-9,13	X 0.11 X 0.50 X 0.75		8.00 8.11 8.90			91.30		8.30 0.80)	Soft to firm brown sandy StLT		
	TCR	SCR	RQD	 		90.50		9.10			
l.11 l.13 l. 14	100	90	âū	6	tere tra _{nd} an	90.50		5.10	Moderately strong grey slightly weathered ANDESITE, iron-stained joints		
l. <b>79</b>					1,6,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1		- (	1.17)			
	100	75	25	10		20.00	<u>-</u> 			+ + + + + + + + + + + + + + + + + + +	
0.27				   	15/01/2007:3.21m	89.33	[:-  -  -	10.27	0	-	
· ·.							E. 		Consplete at 10,27m		
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							רדיריין				
Remarks			· . · ·						Scale (approx	t) E	
		7		1	Marie Company			71.00			



Boring Meth		Casing				evel (mOD)	P. T. Salar, M. A. Salar, S. S. Salar, S. S. Salar, S. S. Salar, S. S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar, S. Salar	Job	
Fraste PL Ri	9	113	3mm cas	ed to 8.30m	9	9.40	Regal Construction (Jersey) Ltd	Number 0762	
		Location	n site plan		Dates 16/1 18/1	01/2007- 01/2007	Engineer Peter Brett Associates		Sheet 1/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legeno	instr
					99.30	(0.10) 0.10 (0.90)	CONCRETE  Layers of concrete and sand	_ 40048	
0.80-1.20	X 0.35				98.40	1.00			
1.20-2.00	X 0.57						CONCRETE		
2.00-2.73	X 0.73					(2.80)			
2.73-3.67	X 0.30			16/01/2007 17/01/2007:2.24m					
3.67-3.82 3.82-4.27 3.82-4.73	X 0.10 SPT N=0 X 0.38		2.00	i .	95.60	3.80	Very soft to firm grey/brown slightly sandy CLAY with a little fine gravel		
1.73-5.00	X 0.45				100				
.00-5.45 .00-6.00	SPT N=5 X 0.52	4.80	2.00	1/_2,3		(3.00)			
00-6.45 00-6.60	SPT N=11 X 0.52	4.80 6.42	2.14	1,1/2,2,3,4					
.60-7.00	X 0.50				92.60	6.80	*		
00-7.45 00-7.35	SPT N=31 X 0.35	6.42 7.25	3.06	3,44,7,10,10			Firm to stiff orange/brown sandy CLAY with a little fine to medium gravel		
35-7.62 62-8.13	X 0.27 X 0.00								
Remarks tarter pit exc xploratory h	cavated by hand from ole drilled using a From 3.82m - 9.24m	n ground le	evel to 1.	20m bgl				Scale (approx)	Logged By
ry drilling fro	om 3.82m - 9.24m illing with water flush excometer with tip insi s are not Ordnance I	from 0.80	m - 3.82r	m. 9.24m - 10.47m				1:40	MRF

Boring N Fraste Pl		q		i	Diameter 3nım cası	ed to 8.30m	Ground t	L <b>eve</b> l 99 40	(MOD)	Client Regal Construction (Jersey) Ltd		i N	ob umb: 076:
				Location as	n site plan		Dates 16/ 18/	/01/20 /01/20	)07- )07	Engineer Peter Brett Associates		S	heet 2/2
Depth (m)		Sample	/ Tests	Casing Depth (m)	Water Depth (m)	field Records	Level (mOD)	D _i (Thic	epth  m) :kness)	Description	Legen	o. Water	ins
8.13-8.60	3	X 0.00		8.30		17/01/2007 18/01/2007:2.90m							
8.63-9.00	3	X 0.23				· ·			(2,40)	· ·			3.1
9.00-9.24 9.00-9.3	4	X 0.40 CPT 80/	155 SCR	8.30 RQD	2.23 FI	2,3/5,25,,50	50.00	}_ 		Stratum as above			
9.24	٠. إ	TCR 15	0	KUD			90.20		9,20	Moderately weak grey slightly weathered ANDESITE, very closely jointed	*****		
9.50		100	0					 - -		the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			
9.66		100	0						(1.27)				
9.93		100	10	0	10+			<u></u>					
10.47	.			<u> </u>	ļ 	18/01/2007.2.99m	88.93	-	10.47		******		TA.
	٠.		٠. ٠							Complete at 10.47m			
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Remar	ks	٠		<u> </u>	<u>.i</u>	<u> </u>		-		. · ·	Scale (approx	;   x}	ogg By



Installation			Dimensi	_TD For	Specialis	19	_	Kensington	Gale C	ai Paik,	K FIGHER,	70:30y		_	BH2
Standpipe		ter						Client Regal Con	struction	(Jersey)	Ltd				Job Number 0762
			Location as site		Ground t	evel (m/		ngineer Peter Brett	Associa	tes					Sheet 1/1
egend 🖁	Instr (A)	Level (mOD)	Depth (m)	Description				Gr	oundwa	ter Strik	s Durin	g Dritting			
					Date	Time	Depth Struck (m)	Casing Depth (m)	Inflo	w Rate	5 min	Read 10 min	Ings 15 min	20 min	Depth Seale (m)
		98.20	1.20	Bentonite Seal			(14)	, , , , , , , , , , , , , , , , , , ,							0.00
								Gre	oundwat	er Obser	vations	During D	rilling		
							_	Start of St					end of SI		
					Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Wate Leve (mOD
					16/01/07 17/01/07 16/01/07	am am am	2.73 8.13	8.30	2.24 2.90	97.16 96.50	pm pm pm	2.73 8.13 10.47	7.25 8.30	2.99	96.4
								Instru	ment Gr	roundwa	er Obse	rvations			
				Gravel Filter	Inst.	A] Type	: Stand	pipe Piezo	meter						
						Inst	trument	[A]							
		- 1			Date	Time	Depth (m)	Level (mOD)				Remi	ins		
					18/01/07 06/02/07	14:42	3.07 2.64	96.33 96.76		- 2					
		89.20 89.00	10.20 10.40	Piezometer Tip											



Boring Meth Fraste PL Ri			Diameter	r ed to 9.21m	Lot come of	evel (mOD)	Client Regal Construction (Jersey) Ltd	Job Numb	13 ber
	•	Locatio			Dates		Engineer	Sheet	
		1	site plan		08/	01/2007- 01/2007	Peter Brett Associates	1/2	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legen	d
					100.03	(0.07)	CONCRETE	1000	
							Loose light brown fine to medium SAND		
						(4.42)			
						(1.43)			
20-1.50	X 0.00								
1.50-1.60 1.60-1.67	X 0.00 X 0.47	1.65	DRY		98.60	1.50	Very soft red brown sandy SILT becoming firm with depth		
1.67-2.12 1.67-2.30	SPT N=11 X 0.00	1.65	1.46	2,2/2,3,3,3					
2.30-2.50	X 0.52			08/01/2007:1.46m					
2.50-2.92 2.50-2.95	X 0.15 SPT N=10	2.85 1.65	DRY	09/01/2007:DRY 1,2/2,3,3,2					
2.92-3.50	X 0.32								
3.50-3.95 3.50-4.50	SPT N=0 X 0.90	2.85	2.00	1/ .					
						(5.50)			
4.50-4.95	SPT N=11	4.40	2.22	1,1/2,3,3,3		(0.50)		88	
4.50-5.50	X 0.50	1.40	-44	1, 112,0,0,0					
	-								
5.50-5.95 5.50-6.10	SPT N=13 X 0.60	4.40 5.83	2.85	1,1/2,3,4,4					
3.10-6.50	X 0.40			09/01/2007:GLm					
6.50-6.90	U 0.28			11/01/2007:1.37m					
5.50-7.14	X 0.57								
7.14-7.50	X 0.00				93.10	7.00	Dense grey and brown clayey very sandy fine to coarse GRAVEL with occasional cobbles	200	
							GRAVEL With occasional cobbles	1300	
7.50-7.52 7.52-7.67 7.67-7.87	X 0.00 X 0.00 X 0.00	7.30				(1.50)			
7.87-7.93	X 0.00					(1.50)			
Remarks Starter pit ex Exploratory h	cavated by hand from	m ground i	level to 1.	20m bgl			Scale (approx	Logge	ıd
Dry drilling for Rock core dr	cavated by hand from note drilled using a From 1.20m - 9.42m, 5 filling with water flush	9.64m - 9.6 n from 9.42	9m 2m - 9.64	m, 9.69m - 10.97m			1:40	MFW	
uro aniling n	rom 6.50m - 6.90m is are not Ordnance						Figure	No.	

Boring Met	hod		Casing	Diameter	-	Ground L	.evel (mOD)	Client	Job
Fraste PL R			i		ed to 9 21m	ŧ .	00.10	Regal Construction (Jersey) Ltd	Nun 0
			Locatio	n site plan	W1374444	Dates 06/ 12/	01/2007- 01/2007	Engineer Peter Brett Associates	She
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Lege
7.93-8.33	X 0.00		8.10						
8.33-8.46 8.46-9.26 8.46-8.91	X 0.50 X 1.20 CPT N=	40	9.21 8.10	3.22	A 7/7 11 14 12	91.60	(1.50)	Stratum as above	
0.40-0.91	CI-1 N-	40	0.10	3.24	4,717,13,14,16		<del>.</del>  	Firm to stiff brown sandy SILT with occasional grey fine to medium gravel	
						. <u> </u>	(1.10)		
9.42-9.64 9.28-9.40 9.40-9.42 9.64-9.69	X 0.00 X 0.00 X 0 12	***		<i>p</i> .,	11/01/2007:3.07m		<u>-</u>  		
9.69	TCR	SCR	RQD	FI	12/01/2007:2.14m X 0.27	90,50	9.60	Moderately strong light grey slightly weathered ANDESITE, iron stained planar discontinuities	
							- 		
	95	90	75	5			<u>(1,37)</u>		
							- - - -		
10.97					12/01/2007:3.40m	89.13	10.97		
							<u>-</u>	Complete at 10.97m	
	·								
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· **	}	٠.					<u> </u>		
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	'''								
					Section 2	·	- - - -		240000000000000000000000000000000000000
	AAR-ACOUNT CO								
Remarks	***************************************	11.4.1	<del></del>	· . · · · .			en en en en en en en en en en en en en e	Scale (approx)	Log
			٠. ٠		V.,		**	1:40	MI

G=	OMARINE				La Por St Sav JE2 7h	arine (Jer te, Rue D four, Jers HT geomarine	u Pont 54303	Borehole N  1  Sheet 1 of
Projec	ct Name			Р	roject N			Hole Type
(ensi	ngton Place				49		Co-ords: -	WLS
ocati	ion: Kensin	gton Pl	ace					Scale
							Level: -	1:50
Client:			uction (Jersey	) Limited	i		Dates: 21/07/2009	Logged By NH
	fikes Depth (m)	Type	Situ Testing Results	Depth (m)	(m AOD)	Legend	Stratum Description	
	0.00-0.55	D					Brown very gravelly soily fine to medium grained to coarse, sub-angular. Occasional cobbles. Slight hydrocarbon smell. (MADE GROUND)	SAND. Gravel is fine
	0.55-0.81	D		0.55			Brown soily gravelly fine to medium grained SAN	D. Gravel is fine to
4	0.81-0.98	D		0.81		30.00	coarse , sub-angular, Layer of pale brown/ white sand, (MADE GROUN	
100	0.98-1.16	D		1.16		100	Brown soily gravelly fine to medium grained SAN	
	1.16-1.40	D		1.40			Layer of pale brown/ white sand. (MADE GROUN	D) //
						====	Light brown gravelly fine to medium grained SAN coarse.	D. Gravel is fine to
	0.62 5/20						Increased sand content. (MADE GROUND)	
	1.40-2.90	D					Pale brown/white slightly gravelly fine to medium is fine to coarse, sub-rounded. Coarse cobbles pe	grained SAND. Gravel / resent. (MADE GROUND)
							Greyf tan sandy CLAY. Strong hydrocarbon smell Sand is fine grained with angular fine to coars occasional brick fragments at 1.40m.	I. (HEAD DEPOSITS)
	2.90-4.40	D		2.90			Grey CLAY. Contains calcareous shells. Strong hydrocarbon smell. (HEAD DEPOSITS)Sub-angular coarse gravel fragments at 2.90n	n.
	4.40-5.90	D		4,40			Grey slightly sandy CLAY. Rare gravel fragments sub-arigular. Hydrocarbon smell. (HEAD DEPOS	, fine to coarse, (TS)
				5.90			Tan slightly sandy gravelly CLAY. Gravel is fine to	
	5.90-6.70	D					sub-angular. (HEAD DEPOSITS)	coarse,
				6.70			Reddish colour, highly gravelly at 6.60m.	
							End of Borehole at 6.80 m	
emark		Type	Results				lain well from 1.80m to ground level w	

Remarks: Slotted well from 6.80m to 1.80m with gravel pack. Plain well from 1.80m to ground level with bentonity surround. Well cover flush at surface.

AGS

	Name toл Place	~~	.,	- 7	roject N 49	eomarine lo.	e Sheet 1 c	уp
cation		gton P	lace	l			Level: - Scale 1:50	e 
ent:	Regal	 Constr	uction (Jersey) I	imited	 		Dates: 17/07/2009 Logged	
Wate	er Sampl	es & In	Situ Testing	Depth	Lavel		NH NH	
Strike	95 Depth (m)	Туре	Results	(m)	(m AOO)	Legend	Stratum Description	
	0.00-1,40	D					Dark brown very gravelly ctayey fine grained SAND. Frequent cobbles. Gravels are fine to coarse, sub-angular, cohesive. Brick fragments and rootlets present. (MADE GROUND)  Clay texture at 0.40m	
							Tan/ brown CLAY at 0.80m	
	4-11-100-11-11-11-11-11-11-11-11-11-11-11			1.40			Grey slightly gravelly CLAY. Gravel is fine to coarse. Hydrocarbon smells. (HEAD DEPOSiTS)	
	1.40-2.90	. و		٠				
				2,90			Yellow/ tan slightly gravetry CLAY. Gravel is fine to coarse, sub-rounded. Slightly stained from hydorcarbon. (HEAD DEPOSITS)  No recovery from 2.90- 5.90m	<del>-</del> .
							No recovery from 2.90- 5.90m	٠.
	5.90-6,80	D		• •			I magazina ang panggan ang Mitting ang military ang military ang military ang military ang military ang militar Military ang military ang military ang military ang military ang military ang military ang military ang military Military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang military ang m	
				6.80	3-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1		Reddish slightly sandy gravelly CLAY from 6.65- 6.80m	
	6.80-7.30	D.			·		End of Bosehole at 7.40 m	
			T TO THE TOTAL THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF THE TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF TAXABLE PARTY OF		. !			
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			1 + 1 1 + 1 1 + 1	3				

surround. Well cover flush at surface.

GEO	MARINE				La Por St Savi JE2 7H	irine (Jers te, Rue D our, Jers iT eomarine	u Pont S 4305	Borehole N 3 Sheet 1 of
Project N	lame			P	roject N			Hole Type
Kensingt	on Place			7-	49		Co-ords: -	WLS
_ocation:	Kensin	gton Pla	ce				Level: -	Scale 1:50
Client:			ction (Jersey				Dates: 19/07/2009-20/07/2009	Logged By NH
ell Water Strikes	Depth (m)	Type Type	itu Testing Results	Depth (m)	(m AOD)	Legend	Stratum Description	
	0.00-0.51	D		0.51			Brown very gravelly fine to medium grained SAND, Gra- coarse, sub-angular. Contains sile fragments, granite (MADE GROUND)	wel is fine to and cobbles.
	0.51-0.89	D		0.89			Brown very gravelly clayey fine to medium grained SAN to coarse, sub-angular. Contains tile fragments, (MADE	D. Gravel is fine ! GORUND)
	0.89-1.36	D					Brown very Gravelly fine to medium clayey SAND. Gravel is fine to coarse, sub-angular. (HEAD DEPOSIT	S)
	1.36-2.80	D		1.38			Tan slightly Sandy CLAY. Contains tiny calcareous she fine. (HEAD DEPOSITS)	ills. Gravel is
	2.80-4.70	2.80 2.80 D 8.45		Tan/ grey CLAY. Occasional fine gravel. (HEAD DEPO	SITS)			
	6.25-6.45 6.45-7.25						Red/ brown very gravelly fine to medium grained SAND. coarse, sub-angular. (HEAD DEPOSITS) Tan very gravelly SAND/ CLAY at 6,45m Gravel is fine to medium, sub- rounded.	Gravel is fine to
				1.63			End of Borehole at 7.25 m	
				*				
	-	Type	Regulto	1				

GEON	MARINE				La Por St Savi JE2 7h	arine (Jers te, Rue Di lour, Jerse IT eomarine.	S 4306	Borehole N 4 Sheet 1 of
Project N	ame			P	roject N			Hole Type
Kensingto	on Place			7.	49		Co-ords: -	WLS
ocation:	Kensin	gton P	Place				Level: -	Scale 1:50
Client:	Regal	Constr	uction (Jersey)	Limited			Dates: 20/07/2009	Logged By NH
Mater Strikes	Sampl Depth (m)			Depth (m)	Level (m AOD)	Legend	Stratum Description	n
	0.00-0.65	D	(Victoria)	0.65			Brown soily very gravelly medium grained SAND Gravel is fine to coarse, sub-angular, cobbles, ( Brown very gravelly fine to medium grained SAN	D. Occasional rooflets. (MADE GROUND)
	0.79-1.43	D		0.79			fragments. Gravel is fine to coarse, sub-angula Brown very gravelly fine to medium grained SAN Gravel is fine to coarse, sub-angular. Concrete	r. (MADE GROUND)
	1.43-2.90	D	Type Results (m) (m AOD) C  D  D  0.65 0.79  D  1.43		GROUND) Tan sandy CLAY. Hydrocarbon smell. (HEAD C Brown very gravelly SAND at 1.55m	sular. Concrete powder observed. (MADI smell. (HEAD DEPOSITS) 1.55m		
	2.90-4.40	D					Brown/ grey very slightly sandy CLAY. Rare ang hydrocarbon smell, dark grey lines running through the sand sand sand sand sand sand sand sand	igh. (HEAD DEPOSITS)
	4.40-5.90	D					Brown/ grey CLAY. Rare fine gravel. Hydrocarb	on smell (MADE GROUN
	5.90-6.35	D					Brown gravelly CLAY. Gravel is fine to medium, GROUND) Reddish very gravelly SAND at 6.30m  End of Borehole at 6.55 m	sub-angular, (MADE
		Тура	Results					F

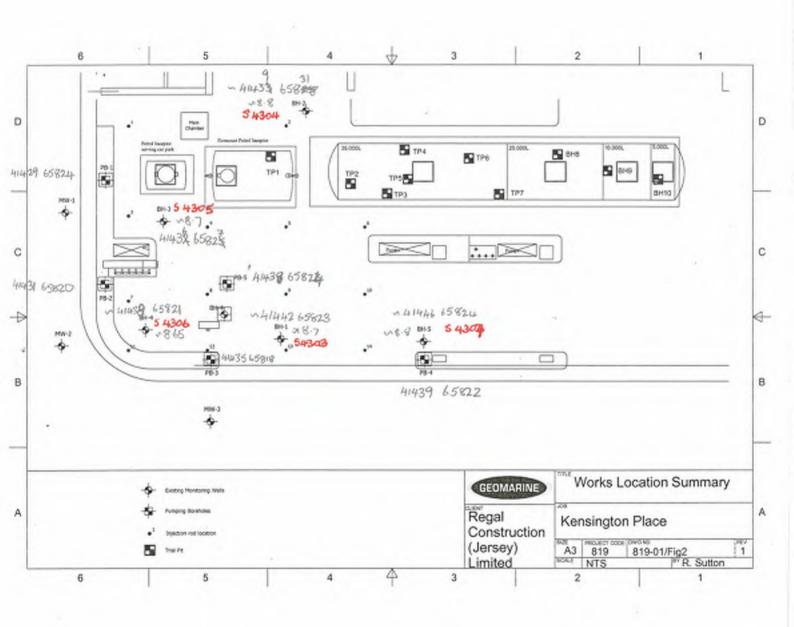
Remarks: Slotted well from 6.55m to 2.00m with gravel pack. Plain well from 2.00m to ground level with bentonite surround. Well cover flush at surface.



1	EON	ARINE	•				te, Rue Di our, Jerse		Borehole I
-	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	Service Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the C				JE2 7H		5 40-7	Sheet 1 of
ro	ject Na	ame			Р	roject N	with an industry publication		Hole Typ
		n Place			100	49	711	Co-ords: -	WLS
oc	ation:	Kensin	gton P	lace					Scale
								Level: -	1:50
'Ea	nt:	Pagal	Conote	votice ( lessev)		,		5.1	Logged B
alle	TH.			uction (Jersey)	Limited			Dates: 16/07/2009	NH
I	Water Strikes	Depth (m)	es & In	Situ Testing Results	Depth (m)	Level (m AOD)	Legend	Stratum Description	
		0.00-0.50	D					Dark brown gravelly clayey fine grained SAND. Grav sub-angular. Cobbles, brick fragments and rootlets.	el. fine to coarse. (MADE GROUND)
					0.50			Tan fine to medium grained SAND. (MADE GROUN	D)
					0.80		12.55	Dark brown gravelly clayey SAND. Gravel, fine to co	arse.
		0.95-1.25	D		1.40			sub-angular. Occasional cobbles, brick fragments as Interbedded tan sand. (MADE GROUND)	nd rootlets.
					1.00		35.55	Dark brown gravelty clayey fine grained SAND. Gravel is fine to coarse, sub-rounded. (HEAD DEPO	SITS
							20.25	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
		1.40-2.90	D						
							32-85/1		
							200		
		2.90-3.10	D		2.90		10000	Dark brown clayey fine grained SAND. (HEAD DEPC	NOTED V
		2.0.10			3,10		77.75	Grey very slightly gravelly CLAY. Fine gravel, sub-ro	
								hydrocarbon smell. (HEAD DEPOSITS) Black/ grey clayey SAND at 3.10m	oroco. Fami
								Hydrocarbon smell. Layer of black hydrocarbon- stained CLAY at 3.30	
		3.10-4.60	D			1		Early of State Hydrocardon Statistic CEAT 813.30	JITI J
							3.5		
ı							拉記		
					4.60		77	Greyl brown slightly gravelly CLAY. Fine gravel, sub-	rounded, cohesive.
							TE	(HEAD DEPOSITS)  No recovery at 4.60m to 6.10m	
							THE R		
							목됩		
							13.5		
						1			
1							목됩		
		6.10-6.90	D				1		
					6.80			Reddish/ brown very gravelly clayey fine grained SAN	D. Ground in fina
		6.90-7.50	D		0.80			to medium, sub-angular. (HEAD DEPOSITS)	/
		VIII-1190			7.50			Brown/ grey very gravelly fine to medium grained SAN to coarse, sub-angular, Rare cobbles present, Faint (HEAD DEPOSITS)	ID. Gravel is fine hydrocarbon smell.
						-	EE.	Grey brown slightly gravelly CLAY. Gravel is fine to	coarse,
		7.50-8.40	D			1		sub-angular. Rare cobbles present. Hydrocarbon sm Very gravelly CLAY at 7.50m	ell. (HEAD DEPOSIT:
					8.40		TEN.	End of Bovehole at 8.40 m	
								CHU U COMPOR IL G.40 M	
1			Type	Results					
w	ovivo:	No inetall-	ation (	Backfill to surfa	100				

Remarks: No installation. Backfill to surface.





115mm cased to 7.00m	Boring Meth	IPLU:	,	Diamete		Specialist:	Level (mOD)	66-72 Esplanade, St Helier Client			BH1
Depth   Sample   Tests   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canadara   Canada	Inspection pi	it to 0.90m	1			o.ou.io	as res (silve)			No	umber
1,00-1,00			-		plan	21	/03/2014- /03/2014			Job Num 15 She	
MADE GROUND - Convented   Mapper   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Convented   Mapper GROUND - Conve	Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water	Instr
Remarks ispection pit excavated by hand on 21.03.14 to 0.9m, dry and stable, backfilled before drilling light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bogged light from 1.20 - 7.00m   Bo	0.00-1.00 1.00-2.00 2.00-3.00 3.00-4.00 4.00-5.00	X 0.75  X 0.78  X 1.00  X 1.00	1.00 2.00 3.00 4.00 5.00 7.00	DRY DRY DRY	28/03/2014:3.75m		0.10 (8.158) (0.30) (0.30) (0.30) (0.30) (0.30) (0.30) (0.30) (1.10) (1.00) (1.00) (1.00) (1.00)	MADE GROUND - Sity sand MADE GROUND - Gravel (Hoggin) Sity brown CLAY Light yellow SAND Brown CLAY with fine to medium gravel  Light brown sity SAND with fine to medium gravel  Light brown Sity SAND  Brown sandy SILT  Yellow brown sandy SILT  Light brown sity sandy CLAY with fine to medium gravels		A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PAR	
spection pit excavated by hand on 21.03.14 to 0.9m, dry and stable, backfilled before drilling Vindow sampling from 1.20 - 7.00m	Domeste										
1:50 MFW	Remarks Inspection pit Window same	t excavated by hand pling from 1.20 - 7.0	on 21.03. 0m	14 to 0.9	m, dry and stable, bed	ckfilled befo	ore drilling		Scale (approx)	B)	gged
		F-19 11311 120 - 170							1:50		MFW

	MP	LU			ation & Ge Specialis		ical	Site 66-72 Esp	olanadę,	St Helier					Borehol Number BH1
Installat Single l	tion Type Installation		Dimensi Intern	ions al Diameter of Tube [A] = 50 n	ทยา			Client Dandara	Jersey Lt	(ci					Job Number 1503
			Location as per	r site plan	Ground	Levei (m	OD)	<b>Engineer</b> Dandara							Sheet 1/1
egend	ਜ਼ੇ ਗਿstr ⊗ (A)	Level (mOD)	Depth (ni)	Description					roundw	ater Strik	es Durin	a Drittin	a		***************************************
iggeno iggi:	<u> </u>	(ISIOD)	(111)		<u>!</u>			7	i		<u> </u>		dings		~
				Cement/Bentonite Grout	Date	Time	Depth Struck (m)	Casing Depth (In)	Inflo	w Rate	5 min		15 min	20 min	Depth Seale (m)
			0.70												
			4.00	Gravel Filter						*.					· .
			1.00											***************************************	
						<u>:</u>	<u>!</u>	Gr	กมาสพล	ter Obse	rvations	During f	) Villina	<u> </u>	<u></u>
			٠.								1				
					Date	Time	Depti Hole	Start of S Casing Deptil		Water Level (mOD)	Time	Depth Hole (m)	End of Si Casing Depth (m)		Water Level (mOD
					27/03/14 28/03/14			5,00	(m) 3.75	(mOD)	17.00 17.00	5.00	5.00 7.00	(m) DRY 3.90	(mOD)
					Longon	05.00		0.00			17,55	7.50	7.50	0.80	
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				Slotted Standpipe	înst.			d Standpip	e			Lechdocienes			
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Source No: 4803

	Inspection pi	t to 1.20m	-	Diamete 3mm cas	r ed to 6.18m	Ground	Level (mOD)	Client Dandara Jersey Ltd	Job Number 1503
0.00-1.13	Praste PL Ri		TAGE OF		plan	21			Sheet 1/2
0.00-1.13	Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (rh)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend
1.13-1.28	0.00-1.13	X 0.50					E (6°15)	MADE GROUND - Concrete	
1.15.1-28							E '0.25		1923
1.05-1.90				12			(0.95)	Clayey gravelly SAND with cobble sized stones becoming light yellow sand	
1.05-3.06	1.13-1.28	X 0.40	1.18		-		1.20	Lanca and Lanca CAMB and Service	
1.90-3.05		101717					E	Loose yellow and brown SAND with line gravel	
1.05-3.50	1.55-1.90	X 0.00					(0.70)		
1.05-3.50 SPT N=2 2.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.05-3.51 X 0.10 3.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-5.04 X 0.41 5.04 Substitute (0.69) Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sa	1.90-3.05	X 0.20					1.90	Loose brown fine SAND	120022 120022
1.05-3.50 SPT N=2 2.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.05-3.51 X 0.10 3.16 DRY 0.00.0.1.1 3.05 Very soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-4.10 X 0.95 (1.58) Soft brown and grey sandy SiLT 3.51-5.04 X 0.41 5.04 Substitute (0.69) Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown and grey sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-5.52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sandy SiLT 3.51-52 Soft brown sa					-		Ē		1000
3.05-3.51 X 0.10 X 0.95	-				-		(1.15)		
1.05-3.51							E		
1.05-3.51   X 0.10   X 0.95   X 0.53   X 0.53   X 0.53   X 0.53   X 0.54   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41   X 0.41	0.05-3.50	SPT N=2	2.16	DRY	0.0/0.0.1.1		3.05	Non-ord house and OH V	999
1.10-4.63						-		very sort brown sandy SIL1	
.10-4.63	.51-4.10	X 0.95	-				-		
83-5.08   SPT N=5   X 0.41   S.04   St.   0.1/1.0.2.2   Soft brown and grey sandy SILT	1						(1.58)		(VE)
83-5.08   SPT N=5   X 0.41   S.04   St.   0.1/1.0.2.2   Soft brown and grey sandy SILT									883 -
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	1.10-4.63	X 0.53	4.16				Ē	- 1	333
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	20 5 00	ODT N. S		~			4.63		323
1.04-6.28			5.04	GL	0,1/1,0,2,2	*	=	Soft brown and grey sandy SILI	
1.58-6.96	i.04-5.28	X 0.22					(0.65)		
98-8.41 SPT N=33	.28-5.58	X 0.30					5.28	Soft brown sandy CLAY	
1,986-8,41 SPT N=33	5.58-5.96	X 0.38					(0.68)		
1.386-8.41 SPT N=33 SPT N=33 SPT N=33 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=14 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 SPT N=26 S							5.96		
1.82-6.95	i.96-6.41 i.96-6.43		6.18		2,5/6,8,9,10		E		
1.92-6.95	.43-6.65	X 0.22			-		E		
95-7.24	.65-6.92	X 0.00					Ė		
33-7-57 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.88 X 0.00 7.8			0.00		02/04/2014/24/2		h	14	3.2
337-57   X 0.00   7.88   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0.00   X 0			0.00				Ē.		
1.28-8.94	.33-7.78	SPT N=26		2.35	5,3/6,7,7,6		Ē.		
1.28-8.94	.57-7.68	X 0.00	1.00				7.78	Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination of the Combination o	200
1.94-9.39 SPT N=14 (.94-9.38 X 0.00 Stiff grey sandy CLAY Siff grey sandy CLAY (0.77) Stiff grey sandy CLAY (0.77) Seale (approx) By drilling from GL to 10.46m								Firm brown sandy sity CLAY with little firm to medium gravel	1
1.94-9.39 SPT N=14	28-8.94	X 0.66	8.68				E		
94-9.39 SPT N=14		V-S-MI					(1.62)		
.94-9.38	*						- (1.02)		
.38-9.63 X 0.65 9.18 9.40 Stiff grey sandy CLAY .63-9.85 X 0.22 (0.77) .85-10.17 X 0.32 (0.77)  Remarks respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling rey drilling from GL to 10.48m					4,3/2,3,4,5		E		
.63-9.85 X 0.22 (0.77)  Remarks respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling rry drilling from GL to 10.46m			0.40				0.40		
.85-10.17 X 0.32 (0.77)  Remarks specifion pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the following type of the f			9.18				9.40	Stiff grey sandy CLAY	3
Remarks Inspection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling Introduction pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before dr							(0.77)		
respection pit excavated to 1.20m on 21.03.14 dry & stable, backfilled before drilling larger GL to 10.46m By		A V.36					<u> </u>		
they coming of 1.50 M	repection pit by drilling fro	om GL to 10.46m	on 21.03	.14 dry 8	stable, backfilled bef	ore drilling		Scale (approx)	Logged By

oring Methorspection pit raste PL Rig	to 1.20m	1	Diamete 3mm ças	r ed to 6.18m	Ground	Levo	i (mOD)	Client Danidara Jersey Ltd	Job Num 15(	ber
THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P		Locatio as	n per site :	plan	Dates 21	1/03/2 1/04/2	2014 2014	<b>Engineer</b> Dandara	Shee 2/	 et :/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	(Th	Depth (m) Ickness)	. Description	Legen	id j
0.17-10.46	X 0.29						10.17	as previous		
ĺ		:					(0.29) 10.46	Stiff grey CLAY with fragments of rock		
0.46-10.53 0.53-10.90	C 0.00 C 0.45							Weak grey slightly weathered Jersey Shale Formation with fron stained close bedding (no solid core recovery)		
0.90-11,55	C 0.65					E	(1.09)			
						<u> </u>	()			
			 	04/04/7054/4 4400		=	11.55			
*				04/04/2014;1.44m		=		Complete at 11.55m		
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temarks	excavated to 1.20m	an 21 03	.14 dru 8	stable, hackfilleri hefe	ore driffing	F	·	Scale (approx)	Logg By	jed
y drilling fro	m Gi. to 10.46m	antie 1700	⊬ i⊸ mily o	stable, backfilled befo	nie miniti			(approx)	By	
Mark Politics	עניוו טו								;	

Insta	llatio	п Туре		Dimensi	ons				Client			····				BH2
						·			Dandara .	Jersey Lte	d 	<del> </del>		·····	<u>}</u>	Number 1503
				Location as per	t site plan	Ground	Level (m		Engineer Dandara							Sheet 1/3
egen	y y	instr (A)	Level (mOD)	Depth (m)	Description				G	roundwa	nter Strik	es Durin	g Drillin	9		
						Date	Time	Depth Struck (m)	Casing Depth (m)	inflo	w Rate	5 min		dings 15 min	20 min	Depth Seale (m)
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															-	
									Gr	oundwai	er Obsei	vations	Burina D	) rilling	·	-
																/4.1
						Date			Start of S	,,	,			End of S		
						Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
						03/04/14 04/04/14	08.00		6.18	1.95		17.00 17.00	6.95 11.55	6.18 9.18	2.40	(1100)
						04/04/14	04.00	0.00	0.10	1.50		17.00	11.00	9.16	1.44	
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									Instr	ument Gr	oundwa	ter Obsei	rvations			
						Inst.	[А] Туре	:					**************************************	^^!!-		
	}		j				ins	trument	[A]							
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AMPLUS I Borehole Foundation & Geotechnical Number Specialists 66-72 Esplanade, St Heller ВН3 Casing Diameter Ground Level (mOD) Client Job Number Inspection pit to 1.20m Competitor Rig 115mm cased to 7.00m Dandara Jersey Ltd 1503 Dates Location Engineer Sheet 25/03/2014-26/03/2014 as per site plan Dandara 171 Casing Depth (rh) Water Depth (m) Depth (m) (Thickness) Depth (m) Water (mOD) Sample / Tests Field Records Description Legend Instr 0.00-1.00 WS 0.17 1.00 (8,13) MADE GROUND - Concrete (0.32)MADE GROUND - Gravel, metal sheet 0.45 (0.25) 0.70 (0.20) 0.90 MADE GROUND - Dark grey gravelly sit Light grey silty CLAY Light yellow SAND 1.00-1.45 1.00 1.00-2.00 SPT N=23 (0.30)DRY 1.3/4.5.6.8 1.20 Stiff brown sandy CLAY with fine to medium gravels WS 1.00 2.00 (0.80)2.00 2.00-2.45 2.00 2.00-2.70 SPT N=68 DRY 8,9/12,17,17,22 Dense light brown fine to coarse SAND with fine to medium gravels WS 1.00 2.70 (1.45)WS 0.30 2.70-3.00 3.00 3.00-3.45 SPT N=31 2.85 8,12/10,8,7,6 3.00 WS 1.00 4.00 Firm brown and grey sandy SILT (0.55)4.00 4.00-4.45 4.00 4.00-4.70 SPT N=2 3.84 0,0/0,0,0,2 Soft brown sandy clayey SILT WS 1.00 4.70 (1.00)WS .30 4.70-5.00 5.00 5.00 5.00-5.45 SPT N=12 4.92 1.2/2.2.4.4 Firm brown sandy SILT 5.00 5.00-5.72 WS 1.00 5.72 (1.00)5.72-6.00 WS 0.20 6.00 6.00 SPT N=24 6.00-6.45 WET 2,1/3,5,6,10 Medium dense to dense brown clayey sandy fine to 6.00 6.00-6.63 coarse GRAVEL WS 1.00 6.63 6.63-7.00 WS 0.31 7.00 25/03/2014:5.12m (1.50)26/03/2014:4.57m 13,11/12,18,19,19 SPT N=68 7.00-7.45 5.05 7.00 7.00-7.50 WS 0.35 7.50 26/03/2014:2.23m Complete at 7.50m Scale (approx) Logged Inspection pit excavated on 21.03.14 from GL to 1.2m, dry & stable, backfilled before drilling Window sampling 1.2 - 7.50m Hole unable to be extended below 7.50m because of dense ground Slotted pipe installed, response zone 7.00-1.00mbgl 1:50 MEW Figure No. 1503.BH3

A۱	/P	LU	SI	Founda	ation & Ge Specialis		cal	<b>Site</b> 66-72 Esp	olanade,	St i felier					Borehole Number BH3
Installati Single In	ion Type nstallation		Dimens Intern	ions al Diameter of Tube [A] = 50 r	ຕກາ			Client Dandara	Jersey Et	d			***************************************		Job Number 1503
			Location	1	Ground	Level (m	(00)	Engineer							Sheet
			as pe	r site plan				Dandara							1/3
Legend	हिंह (A)	Level (mOD)	Depth (m)	Description				G	iroundw	ater Strik	es Durin	g Drilling	3		
ैं <u>दि</u> ष्टे इडक्क					Date	Time	Depth Struc	Casing Depth	Inflo	w Rate		Read		1	Depth Sealed (m)
				Cement/Bentonite Grout		······································	(m)	(m)	<u> </u>	<del> </del>	5 min	10 min	15 min	20 min	(m)
			0.70	Gravel Filter				1		•.••					
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			٠.		<u> </u>	Time	Depti Hole (m)	Casing Depth (m)	Water Depth (ni)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
		·			25/03/14 26/03/14	07.30		6.63	4,57		17.00 17.00	6.63	6.63 7.00	5.12 2.23	
					20.00(1)	71,65		1 3.00	1,07		17.00	1.04.	1.00	2.10	٠.
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o 1.2m	t hand excavated	113		ed to 2.28m sed to 9.21m	Ground	Level (mOD)	Client Dandara Jersey Ltd		Job Numb 150
raste PL Ri	9	Location	n		Dates	100,0044	Engineer		Sheet
		as	per site p	olan	02	/03/2014- //04/2014	Dandara		1/2
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
					1	(0.20) (0.20) (0.20)	MADE GROUND - Concrete	W. 1883	150
						(0.20)	MADE GROUND - Gravelly silt		
					1 5	(0.20)	Dark brown peaty SILT	4.1	
						(0.20)	Brown silty CLAY	1 325 200 200	
					1 3	E- 1	Dense light yellow brown to off white fine to medium silty SAND		200
00 4 05	ODT N-04			0.000.0.40.40		E	medium silty SAND		48
20-1.65 20-1.54	SPT N=34 X 0.34			2,2/6,8,10,10		E			
.54-1.71	X 0.20					(1.62)			
71-1,88 88-2.08	X 0.17 X 0.20					=		1000	133
08-2.28	X 0.20	2.26			3	E			
28-2.42	X 0.17	2.20				2.42		222	
42-2.65	X 0.00			28/03/2014:DRY			Dense off white grey brown slightly silty sandy GRAVEL	8.72	器
65-2.71 42-2.87	X 0.00 SPT N=45			01/04/2014:WET 5,11/11,12,12,10		(0.83)		1000	
71-2.85 85-3.25	X 0.43 X 0.40	2.68 3.25				E ' '			133
25-3.70	SPT N=7	3.25	GL	2,1/1,2,2,2		3.25	Firm brown sandy SILT with a little fine to medium	00000	
25-4.06	X 0.50	4.00	OL.	2,171,2,2,2			gravel	200	
				-		E		1888	器
				1		E		233	
06-4.56	X 0.50					=		X (1)	
								1833	
56-5.01	SPT N=9		3.25	0,1/2,2,2,3	1 4	(2.67)			
56-5.12	X 0.50	4.30				E	4.		
12-5.42	X 0.33	4.68				È		1800	
42-5.92	X 0.50	5.68				E		23.5	
			1 - 8			E		X9.0	
92-6.37	SPT N=28		GL	2,3/4,7,8,9		5.92	Medium dense brown clayey slightly sandy	70.00	
92-6.34	X 0.42	6.23				Ē I	GRAVEL	1	
34-6.53	X 0.19					E		75	100
53-6.92	X 0.39	6.68				E			
92-7.00	X 0.00		1			(1,68)		930	100
00-7.14 14-7.43	X 0.00 X 0.00								
		7.00				E			100
43-7.54 54-7.89	X 0.00 X 0.60	7.23				7.60		12.22	(0.9
		-				E	Stiff grey sandy clayey SILT with a little fine to medium gravel		100
89-8.34 89-8.27	SPT N=20 X 0.38	8.23	3.00	3.4/5,5.5,5	- 1	E	100000000000000000000000000000000000000	200	
27-8.58	X 0.31	100	4			E		4.6	
						(1.61)		Will the	
58-9.21	X 0.63		- 0			E			273
						E			
			9.00			9.21		200	200
21-9.66 21-9.49	SPT N=25 X 0.41	9.21	2.51	2,5/5,6,6,8		E	Stiff grey sandy CLAY with fine gravels		
49-9.79	X 0.27			01/04/2014:5.63m		F		1 200	1
79-9.96	X 0.20			02/04/2014:5.47m		7.60 (1.61) 9.21 (1.01)		27-33 32-33	1009
emarks									1 854
	excavated by hand, 10.62m	backfilled	before d	Irilling				Scale (approx)	Logge By
tary Drilling		one 11.60	- 6.00mh	eal				1:50	MEW
and below									
								Figure N	

C.22-10.49 C.49-10.62 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF p*/76 SPF	Haring Mad	hod	Cacina	Diamete	<u> </u>	Graves	t	d (mon)	Client		-	E
Depth   Sample   Tests   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Dep			113 0.9	3mm case )8mm cas			Leve	ei (mou)	Dandara Jersey Ltd		. N	ŧŧ
10.22   X 0.30   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.27   X 0.20   X 0.20   X 0.27   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X 0.20   X					alan	21. 02	/03/2 /04/2	2014- 2014	_		5	) E
2.22-10.49  X 9.27  C 9.49-10.62  SFT 6775  4.21  6.025,0,0,6  1.0-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10-62  C 10	Depth (iii)	Sample / Tosts	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	{ <b>Th</b> i	Depth (m) ickness)	Description	Legen	Water	
0.22-10.42	9.96-10.22	X 0.30						10.22	i de la companya de la companya de la companya de la companya de la companya de la companya de la companya de			T A A A
0.43-1.02 27.7 0 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.00 0 0.02-0.17.2 0.02-0.02-0.17.2 0.02-0.17.2 0.02-0.17.2 0.02-0.17.2 0.02-0.17.2 0.02-0.	10.22-10.49	X 0.27					-	$\{0.27\}$	Stift brown CLAY with title gravels			00000
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02/04/2014:2.05m	11.10-11.00	0.30	<u> </u>									74000
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Prop. Invert Ex. Invert Chainage.(m) Levels Levels 13 124 13 017 13 082 13 237 12-900 13-028 50.000 13-073 13-136 Patriotic Place BH.4 13 - 212 110-000 13 - 165 120.000 Newgate Street Firm to stiff morange brown with traces of 130.000 13-066 The dimensions i

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e information 0 13 029 140-000  $\Box$ 150.000 BH.3 [11] 170-000 PLAN B.H. 2 LONGITUDINAL S 180-000 13-198 190-000 13-281 m 200-000 ъ 500  $\mathcal{R}$ Asphait crushed Ex. Culvert SECTION 10 - 995 13-642 210-000 surfacing rock fill 11 - 275 | 13 - 768 220-000 230.000 13-982 240.000 7.679 14-172 S  $\leq \Xi$ 250-000 14-366 <u>BH.2</u> ਰ ਰ 14-567 260-000 ឧឧ 270.000 14-700 Parade Place 15-082 300-000 12-098 15-257 Tangent Point No. 2 303 - 378 525 6 Foul Sewer 310-000 15-523 330-000 15 528 Tangent Point No. 1 340-000 15-617 350-000 15.732 15-822 365·000 8·500 367·000 12·800 15-915 380-000 390 000 12 973 450 mm. dia G.V.C. pipe at 1 in 4.772 Contract N° 120.

DRAWN BY: M.R.

CHECKED BY: 88.

SCALE: 1 to 50/500.

REG. DRG. N° T.S. 693. STATES RESOURCES RE Plan & Section of Turnel and Sewer.

701 Beach Outfall, Plan & Section.

702 Details of M.H.No.J - Drop M.H.

703 Details of M.H.No.Z - Tide Flap/Access M.H.

704 Location Plan

1 ypical Details. Gloucester Street
Surface Water Outfall BARTLEY, B.Sc.(Eng.); C.Eng; M.I.C.E; F.I.Mun.E; M.I.W.E.S. Plan 81 B.B. CURVES INCREASED TO 200m RADIUS
2 B.B. WORKING AREA IN PARK AMENDED.
2 B.B. Level of Connel at MH2 altered
and gradient MH2 to Ch.240.009
existing sewer details added.

BETAILS

BETAILS Tunnel 8 % 1A & 1B have recently been sunk piezometers installed. And NOTES RECOVERY BO. related DIRECTOR L.B.38 S.O. And Sewer TRACED BY: M.R. Section Of F.B. **BOARD** 1981. |**X**|**X**|**C** 0 ○ JEPST

## **Appendix F-3**

On-going Phase I Ground Investigation – Draft Data

AM	IPLU:	SL	_T[	Foundation	on & Geo Specialist		nical	Site  Jersey Future Hospital		N	oreh lumb BH1	ber
Boring Meth	nod	Casing	Diamete	r	Ground	Level (	AMSL)	Client		J	ob	
Fraste PL Ri	1 x 1kg plastic	11	3mm cas	ed to 12.65m		8.37		States of Jersey		N	188	
600g glass v	g glass jar & 2 x rial er initially 101mm		n (Obser	ved measurements) blan		3/01/20 5/01/20		<b>Engineer</b> Arup		s	Sheet 1/3	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	Do (Thic	epth (m) kness)	Description	Legend	Water	In	str
					8.31 8.23		0.06 0.14	MADE GROUND - Tarmac	** `.a``.			<b>XX</b>
0.30 0.30	S1 S1			Water flush started	8.12	E	0.25	MADE GROUND - Hoggin				
0.60	S2			Coring trhrough Concrete		E	(0.65)	MADE GROUND - Concrete  MADE GROUND - Sandy gravelly clay with				۵.
				Starter pit excavated by hand to 1.20mbgl	1.31		0.90 1.00	hardcore and boulders				a
1.20	J4		0.90	Coring trhrough Concrete	7.27		1.10	MADE GROUND - Concrete	<u>                                      </u>			
1.20-1.65 1.20	SPT N=15 S3		0.90	7,7/5,4,3,3				MADE GROUND - Stones Stiff brown sandy cobbly CLAY	- 0 · 0 · 0 ·			
1.20-1.25 1.20-1.92	NR B5 0.51					E	(4 ==)	Our brown sainty cobbiy OLAT	· <u>\$ .</u> \$.\$			
1.92-2.27	S6 0.40	1.55					(1.55)		· <u>0 · 0 · 0</u>			
2.27-2.72	SPT N=2		DRY	1,1/,1,,1		Ē			· · · · · · · · · · · · · · · · · · ·			1
2.27 2.27-2.73	J7 B8 0.46	2.55	DRY	,,,,,,,		E			\$ <u>\$ \$ \$ \$</u>			
2.73-3.09	S9 0.36	3.08		23/01/2018:DRY	5.72 5.64	E	2.65 2.73	Very loose brown SAND				
2.70 0.00	00 0.00	0.00		24/01/2018:1.69m				Loose becoming medium dense brown SAND			<b>.</b>	-   
3.09-3.54 3.09	SPT N=20 J10		GL GL	2,4/3,5,6,6		Ē	(0.85)					
3.09-3.58	B11 0.49	3.58			4.79		3.58					
3.58-4.09	X12 0.10				4.75	E	(0.51)	Small granitic Cobbles	000			
					4.28		4.09		000			
4.09-4.54 4.09	SPT N=16 J13	4.09	2.48 2.48	3,3/5,3,4,4	4.20		(0.45)	Stiff green brown sandy SILT				
4.09-4.61	B14 0.56				3.83	E	4.54	Medium dense brown grey SAND with cobbles	* * * * * * * * * * *			
4.61-5.22	NR					E	<i>(</i> )	Mediam dense blown grey SAND with cobbles	ο			
							(0.72)		0.			
5.22-5.26	S15 0.65	5.09			3.11	Ē	5.26	Firm green grey sandy SILT	0.8-0.8-0			
5.26-5.71 5.26	SPT N=12 J16		0.12 0.12	5,3/3,3,3,3		E	(0.75)	l l l l l l l l l l l l l l l l l l l	× × × × × ×			11111
5.26-6.01	NR						(0.75)		* * * * * * * * * * * *			
6.01-6.05	B17 0.50	6.05			2.36		6.01	Firm brown SILT	* * * * *			
6.05-6.61	X18 0.56				2.07	Ē	(0.29) 6.30	Firm grey CLAY	× × × ×			
					1.76		(0.31) 6.61					
6.61-7.06 6.61	SPT N=17 J19		4.09 4.09	4,1/3,4,4,6	1.70		(0.47)	Firm grey CLAY	+=+			
6.61-7.08	B20 0.47				1.29		7.08	Firm fine gravelly SILT				
7.08-7.53	U21/70 0.40	7.05	6.30			Ē		Firm line gravelly SILI				
7.53-7.87	X22 0.40						(0.92)		* * * * * * * * * * * * * * * * * * *			
						Ē			× × × × × × × × × × × × × × × × × × ×			
7.87-8.40	X23 0.53	8.09			0.37		8.00	Firm to stiff grey CLAY	*******			
	Va. 1 a 1 a					Ē	(0.56)					
8.40-8.56 8.56	X24 0.16 J25	0.55	3.72	24/01/2018:3.67m	-0.19		8.56	Very dense grey silty SAND	X/27/27			
8.56-9.18	B26 0.62	8.55	2.63	25/01/2018:2.63m	•	Ē	(0.62)	very defined grey daily 67 ave				
8.56-9.00	SPT 53/285		3.72	2,4/7,9,12,25	0.04		, ,		X		Z 2	
9.18-9.38	X27 0.20	0.45			-0.81 -1.01	Ē	9.18 (0.20) 9.38	Dense green grey fine GRAVEL with coarse sand				
9.38-9.70	X28 0.32	9.15					(0.32)	Stiff grey SILT	× × × × × ×			
9.70-10.32	X29 0.50	9.65			-1.33		9.70	Stiff grey SILT			5000 K	
Remarks Concrete con	lring 0.14-0.25l & 0.9	0-1.00 mh	oal	I	1			Driller: MM	Scale (approx)	Ļ	ogge	ed
Starter pit ex Dry drilling fr	cavated by hand to om GL - 11.10 mbgl	0.25-1.20r	mbgl						(approx)		•	
Ins A: Perfor	g from 11.10 mbgl to ated Pipe with Geos	ock grave	l respons	e zone mbgl					1:50		MFV	V
Ins B: Perfor	ated Pipe with Geos	sock grave	l respons	e zone mbgl					Figure N 1887		1101	

AM	PL	US	S L	T	Foundation	on & Geo		inical	Site  Jersey Future Hospital		N	Sorehole lumber BH101
Boring Meth Fraste PL Ri Sample S =	g 1 x 1kg pla	stic	_	Diamete 3mm cas	r ed to 12.65m	Ground	<b>Level</b> 8.37	. ,	Client States of Jersey			ob lumber 1887
tub, 1 x 250g 600g glass v Hole diamete	ial			n (Obser	ved measurements) blan		3/01/2 5/01/2		Engineer Arup		S	Sheet 2/3
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	(Thi	Depth (m) ickness)	Description	Legen	Water	Instr
10.32 10.32-10.77 10.32-10.98	J30 SPT N= B31 0.5		10.65	5.88 5.88	4,5/9,11,13,13	-1.95		(0.62) 10.32 (0.66)	Stiff grey SILT  Dense grey fine SAND			
10.98-11.10 11.10-11.28	TCR	SCR	RQD	FI	3,21/25 X32 0.18 SPT(C) 25/25	-2.61 -2.73		10.98 11.10	Grey fine SAND with fragments of rock			
11.10	100	0	0	_	X33 ( )	2.70		11.10	Week grey slightly weathered Mudstone (Jerey Shale Formation) closely bedded			
11.57	100	20	0	_	X34		E					
12.19	100	40	20	10	X35			(2.68)				
12.82					X36							
	100	85	50	8	25/01/2018:1.94m		E					
13.78	100	0	0	_	X37 26/01/2018:1.85m	-5.41		13.78	Strong grey fresh to slightly weathered Mudstone (Jerey Shale Formation) medium spaced bedding			
14.32	100	60	0	_	X38							
15.06					X39							
	100	95	85	3			<b>-</b>					
16.18					X40							
	100	90	75	5								
17.59	100	15	0	10+	X41			(7.84)				
18.27					X42							
	100	90	70	5								
19.40					X43							
Remarks Concrete cor	ring 0.14-0	.25l & 0.9l	0-1.00 mb	ıgl	I	1	_		Driller: MM	Scale (approx)	L	ogged By
Starter pit ex Dry drilling fr Rotary coring	a from 11.1	0 mbal to	depth		e zone mbgl					1:50		MFW
Ins B: Perfor	ated Pipe	with Geos	ock grave	l respons	e zone mbgl					Figure 188	<b>No.</b> 7.BH	i101

AV	1PL	U	SL	T	Foundati	on & Geo Specialist	otechnical	Site  Jersey Future Hospital		N	orehole lumber BH101
Machine : F	v			Diamete 3mm ca	er sed to 12.65m	Ground	Level (AMSL) 8.37	Client States of Jersey		N	ob lumber 1887
Core Dia: 1		ssion		n (Obse	erved measurements) plan		3/01/2018- 6/01/2018	<b>Engineer</b> Arup		S	heet 3/3
Depth (m)	TCR	SCR	RQD	FI	Field Records	Level (AMSL)	Depth (m) (Thickness)	Description	Legend	Water	Instr
	100	90	85	3							
20.89	100	100	100	5	X44						
21.39 21.62	100	50	50	5	X45 26/01/2018:1.86m	-13.25		Complete at 21.62m			
Remarks Concrete co	pring 0.14-0	.251 & 0.9	0-1.00 mb	ogl			21.62	Driller: MM	Scale	LIB	ogged
Concrete co Starter pit e Dry drilling f	xcavated by from GL - 11	hand to 1.10 mbgl	0.25-1.20	ogl mbgl				Driller: MM	(approx)		ogged y
Rotary corin Ins A: Perfo Ins B: Perfo No return of	rated Pipe varated Pipe v	with Geos with Geos	ock grave ock grave	l respon	se zone mbgl se zone mbgl				1:50 <b>Figure N</b>	No.	MFW 1101

Boring Meth	od	Casing	Diamete	r	Ground L	_evel (	(AMSL)	Client		Jo	H103
raste PL Rig		_		ed to 12.65m		8.10		States of Jersey			u <b>mber</b> 1887
tub, 1 x 250g 600g glass vi	glass jar & 2 x		n (Obser	ved measurements)		/01/20 /01/20		Engineer Arup DRAF	7	Sh	<b>1/3</b>
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	Do (Thic	epth (m) ckness)	Description	Legen	Water	Instr
							(0.25)	MADE GROUND - Reinforced Concrete		}	
0.30	S1			Starter pit excavated by hand to 1.20mbgl	7.85	E	0.25 (0.35)	MADE GROUND - Sub-base - cruched gr	anite and		
0.60	S2				7.50	Ē	0.60	SAND			<u>:</u>
0.90	S3						(0.60)				
1.20-1.65	SPT N=6		DRY	0,1/2,1,2,1	6.90	Ē	1.20	Loose yellow brown SAND		2000 0 To 1000	
1.20 1.20-1.55 1.55-1.92	S4 NR NR					Ē	(0.93)			C Smcan a	
1.92-2.09	B5 0.17									2000 10000000	
2.09-2.54 2.09-2.13	SPT N=9 NR		DRY	1,1/2,3,1,3 12/01/2018:DRY	5.97	Ē	2.13	Loose brown SAND		5,000000000	
2.13-2.52 2.52-3.10	NR S6 0.50			15/01/2018:1.60m		Ē	(0.97)			200000	
						Ē	(5.5.)				
3.10-3.55	SPT N=14		1.88	2,3/3,3,4,4	5.00		3.10	Firm to stiff brown SILT	* * * * *		
3.10 3.10-3.82	J7 X8			, , , ,					* * * * * * * * * * * * * * * * * * *		
						Ē			* * * * * * * * * *		
3.82-4.48	S9 0.66	3.65		Water flush started			(1.90)		* * * * * * * * * * * *		
									* * * * * * * * * * * *		
4.48-4.93 4.48-5.00	SPT N=25 X11 0.52	5.00	2.88	3,4/5,7,6,7					× × × × × × × × × × × × × × ×		
5.00-5.24	S12 0.24				3.10	E	5.00	Stiff grey SILT	* * * * * * * *		
5.24-5.69	SPT N=25		2.89	4,5/6,6,6,7		Ē		Still grey SILI	*		
5.24 5.24-6.11	J13 X14 0.52	6.00							* * * * * * * * * * * * *		
						Ē	(1.94)		* * * * * * * * * *		
6.11-6.49	X15 0.35						(1.01)		× × × × × × × × ×		
6.49-6.94	U70/16 0.45		3.35	43 blows		E			* ^ * ^ * * * * * * * * *		
					1.16	Ē	0.04		× × × × × × × × × × × × × × ×		
6.94-7.39 6.94	SPT N=44 J17		3.59	11,9/9,9,12,14	1.16		6.94 7.00 (0.40)	Dense COBBLES	× × × × ×		
5.94-7.40 7.40-7.74	X18 0.43 X19 0.34	7.15			0.70	Ē	7.40	Stiff grey SILT  Dense brown fine GRAVEL with coarse sa	and Professional		
7.74-8.05	NR					Ē	(0.00)				
3.05-8.16	NR						(0.93)				
3.16-8.32 3.32-8.33	NR X20	8.15		15/01/2018:3.39m	-0.23	Ē	8.33	Very dense pink grey fine GRAVEL with s	mall (100,000)		
8.33-9.32	NR	0.10		16/01/2018:2.02m				cobbles	0.0		
8.33-8.62	SPT(C) 33/135		2.38	8,10/8,25,0,0			(1.00)		, , , , , , , , , , , , , , , , , , ,		
					-1.23		9.33	0.00	, , , , ,		
9.32-9.33 9.33-9.66	X21 X22 X23	9.15					(0.33) 9.66	Stiff grey CLAY			
9.66-10.21	۸۷۵				-1.30	Ē	J.00	Stiff grey coarse sandy SILT	× × × × × × × × × × × × × × × × × × ×		
Remarks Concrete cor	ing GL-0.25mbgl	0.05.1.55		I.				Driller: MM	Scale (approx)	Lo B\	ogged /
Starter nit ev	cavated by hand to om GL - 12.80 mbgl from 12.80 mbgl to	0.25-1.20n depth	nbgl						1:50		лFW
ns A: Perfora	ated Pipe with Geos ated Pipe with Geos	ock gravel	respons	e zone 11.50-10.00 m	bgl				1.00	No.	

## AMPLUS LTI Borehole Number Site Foundation & Geotechnical Specialists Jersey Future Hospital **BH103** Ground Level (AMSL) **Boring Method Casing Diameter** Client Job DRAFT Number Fraste PL Rig Sample S = 1 x 1kg plastic tub, 1 x 250g glass jar & 2 x 600g glass vial Hole diameter initially 101mm 113mm cased to 12.65m 8.10 States of Jersey 1887 Location (Observed measurements) Engineer Sheet 12/01/2018as per site plan 18/01/2018 Arup 2/3 Water Depth (m) Depth (m) (Thickness) Depth (m) Level (AMSL) Sample / Tests Field Records Description Legend Instr (0.55) Stiff grey coarse sandy SILT 10.21 10.21-10.66 10.21-10.62 J24 SPT N=26 -2.11 10.21 Medium dense brown coarse silty fine SAND 2.43 1.2/4.6.8.8 X25 10.15 X26 10.62-11.21 11.15 (1.00)11.21-11.85 -3.11 11.21 Very dense brown coarse SAND SPT(C) 25*/60 11.21-11.27 0.88 25/ (0.79)11.85-12.19 NR -3.90 12.00 Very dense brown coarse silty SAND (0.28)-4.18 12.28 12.19-12.25 12.28-12.55 X27 12.15 Very stiff grey brown SILT with fragments of rock 25/ SPT(C) 25*/35 16/01/2018:2.21m (0.52)12.55-12.80 ÑR 12.65 SCR RQD TCR FI -4.70 12.80 12.80 X30 Weak to medium strong blue grey slightly to moderately weathered Mudstone (Jersey Shale 100 0 0 12.80-12.84 17/01/2018:1.87m Formation) iron stained bedding closely spaced 13.04 X31 100 0 0 14.12 X32 100 20 0 15.21 15.29 100 0 0 X33 (5.20)100 50 20 10 15.90 16.04 0 0 NR 0 X35 100 0 50 Falling / Rising Head Test from 16.27-16.93mbgl 16.27 X36 100 30 15 10 17/01/2018:2.07m 17.24 18/01/2018:1.69m 75 50 8 100 -9.90 18.00 Medium strong to strong blue grey slightly weathered Mudstone (Jersey Shale Formation) 18.13 X38 smooth planar bedding closeto medium spaced 100 90 80 6 19.26 X39 (2.68)100 95 50 6 Logged By Remarks Scale (approx) Concrete coring GL-0.25mbgl Starter pit excavated by hand to 0.25-1.20mbgl Dry drilling from GL - 12.80 mbgl Rotary coring from 12.80 mbgl to depth Ins A: Perforated Pipe with Geosock gravel response zone 11.50-10.00 mbgl Ins B: Perforated Pipe with Geosock gravel response zone 2.60-1.10 mbgl Driller: MM 1:50 MFW Figure No. 1887.BH103

AN	1PL	U	SL	TI	Foundati	on & Geo Specialist		nical	Site  Jersey Future Hospita	1		N	Borehole lumber BH103
Machine : F	N		_	Diamete 3mm cas	er sed to 12.65m	Ground	<b>Level</b> 8.10	-	Client States of Jersey	DRAFT			ob lumber 1887
Core Dia: 1		ıssion		n (Obse	rved measurements) plan	Dates 12 18	2/01/2 3/01/2	018- 018	<b>Engineer</b> Arup			S	Sheet 3/3
Depth (m)	TCR	SCR	RQD	FI	Field Records	Level (AMSL)	(Thi	epth (m) ckness)	D	escription	Legen	Water	Instr
20.68	100	10	0	-	X40	-12.58 -13.09		20.68 (0.51) 21.19	Medium strong to stron weathered Mudstone smooth planar beddin	ng blue grey slightly to I Mudstone (Jersey Shale d bedding closely spaced ng blue grey slightly (Jersey Shale Formation) g closeto medium spaced			
22.07	100	15 80	70	7	18/01/2018:1.88m X42 19/01/2018:1.58m			(2.00)	with iron stained surfa	ces			
23.19					19/01/2018:1.55m	-15.09		23.19	Complete at 23.19m				
Remarks Concrete co Starter pit e Dry drilling	xcavated by from GL - 12	hand to 2.80 mbgl		mbgl						Driller: MM	Scale (approx)	) в	ogged By
Rotary corir Ins A: Perfo Ins B: Perfo	rated Pipe	with Geos	ock grave	l respon	se zone 11.50-10.00 m se zone 2.60-1.10 mb	nbgl gl					1:50 Figure		MFW 1103

AM	PLU:	S L	_T[	Foundation	on & Geo		Site  Jersey Future Hospital		N	Boreholumbe	er
Boring Meth Fraste PL Ri Sample S =	g 1 x 1kg plastic	_	Diamete 3mm cas	r ed to 11.05m	Ground L	<b>Level (AMSL)</b> 9.50	Client States of Jersey			ob lumbe	
600g glass v	g glass jar & 2 x ial er initially 101mm		n (Obser	ved measurements)		/02/2018- /02/2018	Engineer Arup		S	Sheet 1/3	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	Depth (m) (Thickness)	Description	Legend	Water	Ins	str
0.30	SWAC/1			02/02/2018:DRY 05/02/2018:DRY	9.45 9.37 8.90	0.05 0.13 (0.47)	MADE GROUND - Tarmac  MADE GROUND - Tarmac - 2nd layer  MADE GROUND - Sand with cobbles				
0.60	SWAC/2 SWAC/3			Starter pit excavated by hand to 1.50mbgl	8.90	(0.90)	MADE GROUND - Yellow sand			VIII	
1.20 1.20-1.50 1.50-1.95 1.50-1.98	SWAC/4 - NR SPT N=10 B5 0.48		DRY	1,2/2,2,3,3	8.00	1.50	Loose to medium dense brown SAND				
1.98-2.25 2.25-2.70 2.25-2.79	S6 0.30 SPT N=7 B7 0.55	2.15	DRY	1,2/2,1,2,2		(2.90)				1	
2.79-3.08	S8 0.29	2.65				(2.90)					
3.08-3.53 3.08 3.08-3.58	SPT N=14 J9 B10 0.50	2.00	2.35	1,2/3,3,4,4							179 C 188 C 188 C 188
3.58-4.00 4.00-4.45 4.00-4.45	S11 0.42 SPT N=10 J12	4.00	GL	Water flush started 2,2/2,2,3,3		= - - - - - - -					
4.00-4.56 4.56-5.03	B13 0.45 S14 0.47	5.01			5.10	4.40 (0.63)	Firm brown clayey SILT	* * * * * * * * * * * * * * * * * * *			
5.03-5.48 5.03 5.03-5.76	SPT N=11 J15 B16 0.65		1.05	1,1/2,2,3,4	4.47	5.03	Firm grey SILT	X X X X X X X X X X X X X X X X X X X			
5.76-6.21	100 0 U17/70 0.45	0	3.96	32 blows		(1.18)		x x x x x x x x x x x x x x x x x x x			
6.21-6.64 6.64-7.09	X18 0.45 SPT N=19	6.05	3.68	05/02/2018:4.23m 06/02/2018:3.14m 2,3/3,4,6,6	3.29	6.21	Firm to stiff grey SILT	X X X X X X X X X X X X X X X X X X X			
6.64 6.64-7.90	J19 B20 0.74	7.55				(2.14)		x x x x x x x x x x x x x x x x x x x		300 300 300 300 300 300 300 300 300 300	
7.90-8.35	X21 0.45				1 15	8.35		x x x x x x x x x x x x x x x x x x x			
8.35-8.80 8.35 8.35-8.93 8.93-9.75	SPT N=35 J22 B23 0.58 X24 0.30	8.10 8.60	3.53	5,6/4,6,12,13	0.57	(0.58)	Stiff brown fine gravelly SILT	* * * * * * * * * * * * * * * * * * *			
0.50-5.10	727 U.JU				0.57		Firm to stiff grey clayey SILT	X X X X X X X X X X X X X X X X X X X			
9.75-10.20 9.75 <b>Remarks</b>	SPT N=13 J25		2.52	1,2/3,3,3,4		(1.41)		× × × × × × × × × × × × × × × × × × ×	<u> </u>		
Starter pit ex Dry drilling fr Rotary coring Ins A: Perfor		depth ock grave	l respons	e zone 4.00-2.00 mbg e zone 7.00-6.00 mbg			Driller: MM	Scale (approx)  1:50  Figure N		ogge By MFW	
								1887		1104	

AM	PL	.US	S L	_T[	Foundation	on & Geo		ical	Site  Jersey Future Hospital		ı	Borehole Number 3H104
Boring Meth Fraste PL Rig Sample S = 1 tub, 1 x 250g	) I x 1kg pla	stic	_	<b>Diamete</b> 3mm cas	r ed to 11.05m	Ground	<b>Level (A</b> 9.50	MSL)	Client States of Jersey			Job Number 1887
600g glass vi Hole diamete	al			n (Obser per site p	ved measurements) blan		2/02/201 9/02/201		<b>Engineer</b> Arup			Sheet 2/3
Depth (m)	Sample	/ Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	De (r (Thick	pth n) kness)	Description	Legen	Water	Instr
9.75-10.34	B26 0.5	9	9.55						Firm to stiff grey clayey SILT	× × × × × × × × × × × × × × × × × × ×		
10.34-10.63	X27 0.2		10.55			-0.84 -1.13		10.34 (0.29) 10.63	Medium dense brown silty cobbly SAND	×		
10.63-10.83 10.83-11.07	X28 0.2 X29 0.2 TCR		RQD	FI	25/			(0.44)	Very dense weathered ANDESITE recovered as fragments	++++++		
11.07-11.12 11.07	100	0	0		SPT(C) 25*/50 X30	-1.57		11.07	Grey fractured ANDESITE			
11.52				_	X31					++++++		
	100	0	0	_						++++++		
								(0.70)		*******		
12.46					X32			(2.70)		*******		
	100	0	0							*******		
	100	O		_						*******		
					06/02/2018:2.91m	4.07		40.77		*******		
13.77	100	0	0	_	X33 07/02/2018:2.75m	-4.27		13.77	Grey fractured ANDESITE	*******		
14.15					X34		E			**********		
	100	0	0	_						*******		
										++++++		
15.07	100	30	0	_	X35					++++++		
15.63					X36			(3.61)		*******		
	100	10	0	_								
16.10					X37					********		
	100	20	20	10						*******		
										********		
						-7.88		17.38		*******		
17.38					X38	-7.00		17.50	Strong grey slightly weathered to fresh ANDESITE	********		
	100	90	85	5						*******		
	100	90	05	3						++++++		
18.60					X39					*******		
										*******		
	100	95	90	4						+++++++		
										++++++	•	
20.00										*******		
Remarks Starter pit ex	cavated by	hand to	GL-1.50m	bgl					Driller: MM	Scale (approx	) I	Logged By
Dry drilling fro Rotary coring Ins A: Perfora	g from 11.0 ated Pipe v	7mbgl to with Geos	ock gravel	l respons	e zone 4.00-2.00 mbg	ıl				1:50		MFW
Ins B: Perfora	ated Pipe v	with Geos	ock grave	l respons	e zone 7.00-6.00 mbg	jl				Figure		H104

AIV	1PL	.U	SL	_	Foundation	on & Geo Specialist	otechnical s		Site  Jersey Future Hospital			Nu	orehole imber H104
Flush : \	N		Casing		er sed to 11.05m	Ground	Level (AMSL 9.50	)	Client States of Jersey				b imber 1887
	Depth   TCR   SC			n (Obse	erved measurements)		2/02/2018- 9/02/2018		<b>Engineer</b> Arup			Sh	3/3
Depth (m)	TCR	SCR	RQD	FI	Field Records	Level (AMSL)	Depth (m) (Thickness	s)	Description	Lege	end	Water	Instr
	100	90	80	5	07/02/2018:3.50m				Strong grey slightly weathered to fresh ANDESITE	**************************************	*** ** ** ** ** ** ** ** ** **		
20.78	100	95	90	4	09/02/2018:2.53m						+ + + + + + + + + + + + + + + + + + +		
22.12	100	100	100	2			(10.0	(3)			** ** ** ** ** ** ** ** ** ** ** ** **		
22.84	100	100	100	2							***  * * * * * * * * * * * * * * * * *		
24.16	100	90	90	3									
25.47	100	95	90	2							+ + + + + + + + + + + + + + + + + + +		
26.77	100	100	95	2	09/02/2018:3.23m	-17.91	27.4	.1		+ + + + + + + + + + + + + + + + + + +	* * * * * * * * * * * * * * * * * * * *		
21.41									Complete at 27.41m				
Remarks Starter pit e Dry drilling Rotary corir	excavated by from GL - 11 ng from 11.0	/ hand to l l.07mbgl l7mbgl to	GL-1.50m depth	bgl	se zone 4.00-2.00 mbg	1			Driller: MM	Scal (appro	x)		gged
Ins A: Perfo	orated Pipe orated Pipe or	with Ğeos with Geos	ock grave ock grave	l respon I respon	se zone 4.00-2.00 mbg se zone 7.00-6.00 mbg	ji J				1:50 Figur		<b>.</b>	1FW

AM	PLU	S L	_T[	Foundation	on & Geo	otechnical s		Site  Jersey Future Hospital		N	orehoumbe umbe	er
	g 1 x 1kg plastic	_	<b>Diamete</b> 3mm cas	r ed to 13.56m		<b>Level (AMSI</b> 10.40	_)	Client States of Jersey			ob umbe 1887	
600g glass v	gglass jar & 2 x ial er initially 101mm		n (Obser	ved measurements) blan		1/02/2018- 0/02/2018		Engineer Arup		S	<b>heet</b> 1/3	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	Depth (m) (Thicknes	ss)	Description	Legend	Water	Ins	str
0.30 0.60 0.90	SWACX1 SWAC2 SWAC3			Starter pit excavated by hand	10.33 10.26 10.20	0.0	4 0 0)	MADE GROUND - Tarmac  MADE GROUND - Tarmac  MADE GROUND - Hoggin  MADE GROUND - Sandy matrix with stones and fragments of hardcore				3
1.20-1.65 1.20 1.20 1.20-1.73 1.73-2.03 2.03-2.48 2.03	SPT N=9 J5 SWAC4 B6 0.53 S7 0.30 SPT N=12 J8		DRY	to 1.50mbgl 2,2/2,3,2,2 1,1/3,2,3,4		(2.0)		Loose becoming medium dense yellow brown SAND				\$ 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.5 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 / 12.6 /
2.50-2.60 2.60	B9 0.40 S10	2.15			7.00		4					10.128.00.138.00.00.00.00.00.00.00.00.00.00.00.00.00
3.01-3.50 3.01-3.46 3.50	B11 0.49 SPT N=7 S12	3.50	2.27	Water flush started 14/02/2018:GL 15/02/2018:2.27m 2,2/2,1,2,2	7.39	3.0		Loose becoming medium dense brown SAND				200 0 200 0 200 0 0 0 0 0 0 0 0 0 0 0 0
4.08-4.53 4.08 4.08-4.60 4.60	SPT N=15 J13 B14 0.38 S15 0.38	4.55	GL	2,3/5,3,3,4	5.90	4.5	0	Medium dense occasionally loose brown fine silty SAND			WIIII	
5.06-5.51 5.06 5.06-5.60	SPT N=8 J16 B17 0.45		1.84	1,1/1,2,2,3		= = = = = = = = = = = = = = = = = = =			X X X X X X X X X X X X X X X X X X X			
5.60-6.05 6.05-6.48	U18 0.45 X19 0.43	5.60	2.28	33 blows		(2.7)	3)					
6.48-6.93 6.48 6.48-6.86 6.86-7.28	SPT N=30 J20 B21 0.30 X22 0.49	6.61 7.05	2.13	3,6/6,8,8,8		= = = = = = = = = = = = =						
7.28-8.09	X23 0.60	8.07			3.12	7.2		Stiff grey brown CLAY				
8.09-8.54 8.09 8.09-8.47	SPT N=24 J24 B25 0.38	8.50	0.57	2,4/4,4,8,8	1.93	(0.3	4)	Medium dense brown and grey cobbly GRAVEL				
8.69-8.81 8.81-8.95 9.21-10.15	X26 0.10 X27 0.15 X28 0.85	10.10		15/02/2018:1.95m 16/02/2018:2.33m	1.59 1.45	(8.8) - (8.9) - (8.9) - (8.9) - (8.9)		Medium dense brown and grey coarse SAND and fine GRAVEL  Medium dense grey SAND becoming clayey SAND				
Dry drilling fr	cavated by hand to om GL - 13.02mbgl g from 13.02mbgl to		bgl			<u>-</u>		Driller: MM	Scale (approx)	L ₀	ogge y	ed :
Ins A: Perfor	ated Pipe with Geos	ock grave		e zone 3.50-1.50mbg e zone 15.50-14.00ml					1:50 <b>Figure N</b>	lo.	MFW 105	! ——

AM	PL	U	S L	_T[	Foundation	on & Geo		nical	Site  Jersey Future Hospital		N	Borehole lumber BH105
Boring Meth Fraste PL Rig Sample S =	g 1 x 1kg pla	estic	-	Diamete 3mm cas	r ed to 13.56m	Ground I	<b>Level</b> 10.40	` '	Client States of Jersey			lob lumber 1887
tub, 1 x 250g 600g glass vi Hole diamete	ial			n (Obser	ved measurements)		1/02/2 0/02/2		Engineer Arup		S	Sheet 2/3
Depth (m)	Sample	e / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (AMSL)	(Thi	epth (m) ckness)	Description	Legen	Water	Instr
10.15-10.48	X29 0.3	33				0.25		10.15 (0.33)	Medium dense brown and grey coarse SAND and fine GRAVEL Stiff light grey CLAY	######################################		
10.48-11.25	X30 0.6	65				-0.08		10.48	Stiff dark grey sandy CLAY			
11.25 11.25-11.70 11.25-11.91	J31 SPT N= B32 0.3		11.65	7.78	2,4/4,6,6,8			(1.85)				
11.91-12.33	X33 0.7	0						40.00				
12.33-12.70 12.83-13.02	X34 0.3 X36 0.1		12.60 13.10		2,8/25	-1.93 -2.30		12.33 (0.37) 12.70	Stiff green grey sandy CLAY			
12.70-12.83 13.02-13.21 13.02	X35 0.1		RQD	FI	SPT(C) 25/35 X37	-2.62		(0.32) 13.02 (0.18) 13.20	Stiff yellow brown SILT with fragments of weathered rock weathered ANDESITE	× × × × × × × × × × × × × × × × × × ×		
						-2.80		13.20	Medium strong grey slightly weathered ANDESITE iron stained planar joints	*******		
13.87					X38					******* ******* ****** ****** ******		
14.76					16/02/2018:3.60m X39			(3.57)		******* ******* ******* *******		
					19/02/2018:3.22m			(0.07)				
16.18					X40							
16.77					Falling Head Test X41	-6.37		16.77	Weak grey brown slightly to mederately weathered ANDESITE, closely spaced joints	******** ******* ******* ****** ****** ****		
17.85					X42	-7.45		(1.08) 17.85	Medium strong grey slightly weathered ANDESITE	**************************************		
								(1.15)	iron stained planar joints			
19.00					X43	-8.60		19.00	Weak grey brown slightly to mederately weathered ANDESITE, closely spaced joints	*******		
19.52					X44	-9.42		(0.82) 19.82	Weak grey brown slightly to mederately weathered	*******		
Remarks Starter pit ex	cavated by	y hand to	 GL-1.20m	bgl			F-		Driller: MM	Scale (approx	L	ogged
	g from 13.0 ated Pipe v ated Pipe v	02mbgl to with Geoswith Geos	ock grave ock grave	l respons	e zone 3.50-1.50mbg e zone 15.50-14.00m				Driller: MM	1:50	No.	MFW 1105

AN	1PL	U	SL	_T[	Foundation	on & Geo Specialist		nical	Site  Jersey Future Hospital		N	Borehole Number 3H105
	water		_	Diamete 3mm cas	ed to 13.56m	Ground I	<b>Level</b> (	-	Client States of Jersey			Job Number 1887
Core Dia:		ussion		n (Obse	rved measurements)		1/02/20 0/02/20		Engineer Arup		5	Sheet 3/3
Depth (m)	TCR	SCR	RQD	FI	Field Records	Level (AMSL)	D (Thic	epth (m) ckness)	Description	Legen	Mater Mater	Instr
						-9.63		(0.21) 20.03	ANDESITE, closely spaced joints Weak grey brown slightly to mederately weathered ANDESITE, closely spaced joints	*******		
20.63					X45			(1.76)	Medium strong grey slightly weathered ANDESITE iron stained planar joints			
21.79					19/02/2018:3.65m X46 20/02/2018:3.14m	-11.39		21.79 (0.72)	Medium strong grey slightly weathered ANDESITE iron stained planar joints	***************************************		
22.51					X47	-12.11		22.51	Weak grey brown slightly to mederately weathered ANDESITE, closely spaced joints			
23.63					X47					*******		
24.10						-13.70		24.10	Complete at 24.10m	Conta		
Dry drilling Rotary corir Ins A: Perfo	ng from 13.0 rated Pipe	02mbgl to with Geos	ock grave		se zone 3.50-1.50mbg se zone 15.50-14.00m					Scale (approx	)   E	Logged By MFW
	•		<b>.</b>			-				Figure		

Α	V	ΙΡΙ	_U	S LTD Foundation & Geotechnical Specialists					Site  Jersey Future Hospital							Borehole Number BH102		
Installation Type Double Installation				Dimensions Internal Diameter of Tube [A] = 20 mm Internal Diameter of Tube [B] = 50 mm					Client States of Jersey							Job Number 1887		
				Location as per site plan		Ground Level (AMSL) 8.80			Engineer Arup							Sheet 1/1		
Legend	<b>p</b> Water	Instr (A) (B)	Level (AMSL)	Depth (m)	Description		Groundwater Strikes During Drilling											
	90112 >		8.30	0.50	Concrete Bentonite Seal  Cement/Bentonite Grout			Depth	Casing			Readings				Depth		
* * * * * * *			7.80	1.00		Date	Time S	Depth Struck (m)	Casing Depth (m)	Inflow Rate		5 min	10 min   15 mi		20 min	Depth Sealed (m)		
∇	<b>∑</b> 1					27/11/17		2.97	2.65									
*.*.*.*									Gr	oundwa	ter Obse	rvations During Drilling						
			2.30						Start of S	 Shift		i i		End of Shift				
× × × × × × × × × × × × × × × × × × ×			1.30	7.50	Bentonite Seal	Date	Time	Depti Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (AMSL)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (AMSL)		
× × × × × × × × × × × × × × × × × × ×					Slotted Standpipe	24/11/17 27/11/17	08.00		1.53	DRY	(AIVISE)	17.00 17.00	2.15 9.20	1.53 9.15	DRY GL	(AIVISL		
* * * * * * * * * * * * * * * * * * *			-0.20	9.00		28/11/17 29/11/17	08.00 08.00	9.20	9.15 9.65	GL 2.53	6.27	17.00 17.00	16.48 25.20	9.65 9.65	2.38 2.59	6.42 6.21		
*******					Bentonite Seal													
			-2.20	11.00														
					Slotted Standpipe													
			-3.70	12.50	Bentonite Seal		Instrument Groundwater Observations											
			-4.70	13.50		Inst.	Inst. [A] Type: Slotted Standpipe						Inst. [B] Type: Slotted Standpipe					
						Date	Instrumen		t [A]	Instrument [		[B]						
							Time	Depti (m)	h Level (AMSL)	Time	Depth (m)	Level (AMSL)		arks				
					Cement/Bentonite Grout	30/11/17 01/12/17 01/12/17 14/12/17	17:00 08:00 17:00 11:30	2.5 2.5 2.5 2.4	1 6.29 4 6.26	17:00 08:00 17:00 11:30	2.48 2.45 2.48 2.34	6.32 6.35 6.32 6.46						
			-16.40	25.20														

Remarks
Ins A: Perforated Pipe with Geosock gravel response zone 12.50 - 11.00mbgl
Ins B: Perforated Pipe with Geosock gravel response zone 9.00 - 7.50mbgl

AMPLUS LTD Founda						otechnio ts	cal	Site  Jersey Future Hospital							Borehole Number BH107	
Installation Type Double Installation			Dimensions Internal Diameter of Tube [A] = 20 mm Internal Diameter of Tube [B] = 50 mm					Client States of Jersey							Job Number 1887	
			Location	Ground	round Level (AMSL) Engineer											
			as per site plan		11.70			Arup							1/1	
.egend ≷	Instr (A) (B)	Level (AMSL)	Depth (m)	Description		Groundwater Strikes During Drilling										
				Concrete  Bentonite Seal			Depth	Casing			Readings				Depth	
	10.7	10.70	1.00		Date	Time	Depth Struck (m)	Casing Depth (m)	Inflo	w Rate	5 min	10 min	15 min	20 min	Depth Sealed (m)	
¥	1 21 555 15	9.70	2.00		15/11/17		2.04	3.04			1.99	1.98			1.98	
				Slotted Standpipe												
		7.70	4.00	Bentonite Seal												
* × × ×		6.70	5.00	Bernorine Gedi												
× × × × × × × × × × × × × × × × × × ×				Groundwater Observations During Dr								rilling	rilling			
* * * * * * * * * * * * * * * * * * *								Start of Shift			 -					
* * * * * * * * * * * * * * * * * * *					Date	Time	Depti			Water	Time	Depth Hole	Casing Depth		Water	
× × × × × × × × × × × × × × × × × × ×				Cement/Bentonite Grout	15/11/17	Time	Depti Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (AMSL)	17.00	6.82	3.04	Water Depth (m) 3.15	Level (AMSL) 8.55	
· · · · · · · · · · · · · · · · · · ·					16/11/17 17/11/17	08.00 08.00	12.37	3.04 11.65	1.96 6.58	9.74 5.12	17.00 17.00	12.37 19.13	11.65 14.15	7.06 3.81	4.64 7.89	
* * * * * * * *					20/11/17 21/11/17	08.00 08.00	19.13 27.58	14.15 14.15	3.40 3.42	8.30 8.28	17.00 17.00	27.58 30.66	14.15 14.15	3.90 3.95	7.80 7.75	
× × × × × × × × × × × × × × × × × × ×																
× × × × × × × × × × × × × × × × × × ×		-2.30	14.00	Bentonite Seal												
**************************************	& 189 min	-3.30	15.00			Instrument Groundwater Observations										
**************************************		-4.30	16.00	Slotted Standpipe Bentonite Seal	In at IA1 Town				е	Ins	t. [B] Typ	Type: Slotted Standpipe				
******	-5.3		17.00			Instrumer		nt [A] In		Instrument [B]						
******					Date	Time	Depti (m)	Level (AMSL)	Time	Depth (m)	Level (AMSL)	Remarks				
**************************************					22/11/17	17:00	3.4	-	17:00	1.98	9.72					
,,,,,,,,					23/11/17 14/12/17	08:00 11:20	3.58 3.03	8 8.12	08:00 11:20	1.98 1.63	9.72					
**************************************																
//////// /////////////////////////////																
<del>//////</del>				Cement/Bentonite Grout												
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,																
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v'v'v'v'v'		-18.96	30.66													

Remarks
Ins A: Perforated Pipe with Geosock gravel response zone 16.00 - 15.00mbgl
Ins B: Perforated Pipe with Geosock gravel response zone 4.00 - 2.00mbgl